Chapter 8

BMP OVERVIEW AND SELECTION CRITERIA

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8.0. INTRODUCTION

The application of Best Management Practices (BMPs) to stormwater management has broadened in the past ten years. With EPA's implementation of various kinds of federal stormwater permits for localities with Municipal Separate Storm Sewer Systems (MS4s) and for building construction-related stormwater runoff control (both administered in Virginia through delegation to the DEQ), a broad array of practices has been identified as appropriate for managing stormwater. It is important for stormwater managers to understand the full context of these programs and related stormwater impacts, to see how they fit together and, thus, to understand what kinds of practices to employ for the various purposes. This chapter provides an overview of the various kinds of BMPs that must be employed, but it focuses especially on the "post-construction" practices that must be built during site development with the intent of managing site runoff perpetually after construction is completed. Then the chapter provides useful guidance regarding how to make the best selection of BMPs for a development project.

Flow-Related Issues

Section 4.1.6 of Chapter 4 of this Handbook discusses the hydrologic changes that occur in response to land development and added impervious cover. Maintaining or at least mimicking the pre-development hydrologic conditions is recommended in all cases, but especially for receiving water bodies that are highly or moderately susceptible to stormwater impacts. The relationship between any storm event, no matter how small or how large, and runoff volumes must be thoroughly understood. BMPs that address the full range of hydrologic conditions should be employed to minimize impacts.

In parts of Virginia with particularly cold winter climates, snow melt events pose a significant problem. A large volume of water occurs at the end of the winter when many impediments, such as frozen ground for infiltration basins or frozen permanent pools and clogged outlets for pond systems, may be at their worst. Thus the effectiveness of these BMPs is often compromised during such critical runoff events (CWP, 1997).

Pollutants of Concern

Section 4.5.4 of Chapter 4 of this Handbook discusses the water quality impacts that are common on urban and suburban (or developing) land. That section identifies the most prominent pollutants (see **Table 4.7**), indicates where on the land surface they are most likely to be generated (see **Figure 4.35**), and identifies the treatment mechanisms that are likely to be successful in removing or reducing each type of pollutant.

With careful site planning, developers and municipalities can reduce the amount of impervious area created by pavement and roofs, thus reducing the volume of stormwater runoff and associated pollutants requiring control. By employing BMPs that further reduce runoff volume, site designers can further reduce the negative impacts of development and perhaps avoid the need for some of the traditional stormwater management infrastructure resulting from the use of more traditional BMPs.

8.1. CATEGORIES OF BMPs AND THE MOST EFFECTIVE ORDER OF IMPLEMENTING THEM

Remember that the goal of pollution prevention is to prevent contact of rainfall or stormwater runoff with pollutants, thus reducing pollutant loads to water bodies while maintaining as much of the watershed's natural (predevelopment) hydrology as possible. Thus, stormwater control measures (BMPs) are most effective from the perspective of both efficiency and cost when stormwater management is considered and incorporated in the early planning stages of a community, watershed or development project.

As noted in **Chapter 5**, many, if not most, development sites will need to employ multiple practices in order to satisfy the nutrient reduction requirements in the Regulations and adequately manage the stormwater runoff. Under the treatment train approach, stormwater management begins at the site level with simple methods that minimize the amount of runoff that occurs from a site and methods that prevent pollution from accumulating on the land surface and becoming available for transport in runoff from the site ("source controls" or non-structural BMPs or Better/Environmental Site Design).

The following is a brief description of each of the categories of practices listed in **Table 5.1** (in **Chapter 5**), which reflect the correct order of BMP implementation. Following these descriptions, there will be more specific descriptions of the post-construction BMPs that are more the focus of this Handbook.

8.1.1. Product Substitution

Product substitution refers to one of the classic pollution prevention approaches of reducing the availability of pollutants for future wash-off into stormwater runoff. The most notable example is the introduction of unleaded gasoline, which resulted in an order-of-magnitude reduction of lead levels in stormwater runoff in a decade (Pitt et al., 2004a, b). Similar reductions are expected with the phase-out of methyl tert-butyl ether (MTBE) additives in gasoline. Other examples of product substitution are the ban on coal-tar sealants during parking lot renovation that has reduced PAH runoff (Van Metre et al., 2006), phosphorus-free fertilizers that have measurably reduced phosphorus runoff (Barten and Johnson, 2007), the painting of galvanized metal surfaces, and alternative rooftop surfaces (Clark et al., 2005). Given the importance of coal power plant emissions in the atmospheric deposition of nitrogen and mercury, it is possible that future emissions reductions for such plants may result in lower stormwater runoff concentrations for these two pollutants.

8.1.2. Watershed Land-Use Planning

Communities can address stormwater problems by making land-use decisions that change the location or quantity of impervious cover created by new development. This can be accomplished through zoning, watershed plans, comprehensive land-use plans, or Smart Growth incentives.

The unit process that is managed is the amount of impervious cover, which is strongly related to various residential and commercial zoning categories (Capiella and Brown, 2000). Numerous

techniques exist to forecast future watershed impervious cover and its probable impact on the quality of aquatic resources (see discussion of the Impervious Cover Model in **Appendix 5-A** (**Chapter 5**); (CWP, 1998a; MD DNR, 2005). Using these techniques and simple or complex simulation models, planners can estimate stormwater flows and pollutant loads through the watershed planning process and alter the location or intensity of development to reduce them.

The level of control that can be achieved by watershed and land-use planning is theoretically high, but relatively few communities have aggressively exercised it. The most common application of down-zoning has been applied to watersheds that drain to drinking water reservoirs (Kitchell, 2002). The strength of this practice is that it has the potential to directly address the underlying causes of the stormwater problem rather than just treating its numerous symptoms. The weakness is that local decisions on zoning and Smart Growth are reversible and often driven by other community concerns and priorities, such as economic development, adequate infrastructure, and transportation. In addition, powerful consumer and market forces often have promoted low-density sprawl development. Communities that use watershed-based zoning often require a compelling local environmental goal, since state and federal regulatory authorities have traditionally been extremely reluctant to interfere with the local land-use and zoning powers.

8.1.3. Conservation of Natural Areas

Natural area conservation protects natural features and environmental resources that help maintain the predevelopment hydrology of a site by reducing runoff, promoting infiltration, and preventing soil erosion. Natural areas can be legally protected by a permanent conservation easement prescribing allowable uses and activities on the parcel and preventing future development. Examples include any areas of undisturbed vegetation preserved at the development site, including forests, wetlands, native grasslands, floodplains and riparian areas, zero-order stream channels, springs and seeps, ridge tops or steep slopes, and stream, wetland, or shoreline buffers. In general, conservation should maximize contiguous area and avoid habitat fragmentation.

While natural areas are conserved at many development sites, most of these requirements are prompted by other local, state, and federal habitat protections, and are not explicitly designed or intended to provide runoff reduction and stormwater treatment. To date, there are virtually no data to quantify the runoff reduction and/or pollutant removal capability of specific types of natural area conservation, or the ability to explicitly link them to site design.

8.1.4. Impervious Cover Reduction

A variety of practices, some of which fall under the broader term "better site design (BSD)" or "environmental site design (ESD)," can be used to minimize the creation of new impervious cover and disconnect or make more permeable the hard surfaces that are needed (Nichols et al., 1997; Richman, 1997; CWP, 1998a). The following is a list of some common impervious cover reduction practices for both residential and commercial areas:

Elements of Environmental Site Design: Single-Family Residential Sites

- Reducing the residential street width
- Reducing the street right-of-way (ROW) width
- Using swales and other BMPs that can be located within the ROW
- Reducing the cul-de-sac radius
- Installing vegetation and, ideally, a bioretention BMP on the island in the center of the cul-desac
- Alternative turn-around options, such as hammerheads, are acceptable if they reduce impervious cover
- Narrow sidewalks on one side of the street only (or move pedestrian pathways away from the street entirely)
- Disconnect rooftops from the storm-drain systems
- Minimize driveway length and width or share driveways, and use permeable surfaces
- Allow for cluster or open-space designs (e.g., zero lot line) that reduce lot size or setbacks in exchange for conservation of natural areas
- Permeable pavement in parking areas, driveways, sidewalks, walkways, and patios

Elements of Environmental Site Design: Multi-Family Residential and Commercial Sites

- Design buildings and parking to have multiple levels
- Store rooftop runoff in green roofs, foundation planters, bioretention areas, or cisterns
- Reduce parking lot size by reducing parking demand ratios and stall dimensions
- Use landscaping areas, tree pits, and planters for stormwater treatment
- Use permeable pavement for parking areas, plazas, and courtyards

CWP (1998a) recommends minimum or maximum geometric dimensions for subdivisions, individual lots, streets, sidewalks, cul-de-sacs, and parking lots that minimize the generation of needless impervious cover, based on a national roundtable of fire safety, planning, transportation and zoning experts. Specific changes in local development codes can be made using these criteria, but it is often important to engage as many municipal agencies that are involved in development as possible in order to gain consensus on code changes.

At the present time there is little research available to define the runoff reduction benefits of these practices. However, modeling studies consistently show a 10-45 percent reduction in runoff compared to conventional development (CWP, 1998b, c, 2002). Several monitoring studies have documented a major reduction in stormwater runoff from development sites that employ various forms of impervious cover reduction and LID in the United States and Australia (Coombes et al., 2000; Philips et al., 2003; Cheng et al., 2005) compared to those that do not.

Unfortunately, environmental site design has been slowly adopted by local planners, developers, designers, and public works officials. For example, although the Seattle Green Street project pictured in **Figure 5.2** (**Chapter 5**) has been very successful in terms of controlling stormwater, the environmental site design principles used have not been widely adopted in the Seattle area. Existing local development codes may discourage or even prohibit the application of

environmental site design practices, and many engineers and plan reviewers are hesitant to embrace them. Impervious cover reduction must be incorporated at the earliest stage of site layout and design to be effective, but outdated development codes in many communities can greatly restrict the scope of impervious cover reduction. Finally, the performance and longevity of impervious cover reduction is dependent on the infiltration capability of local soils, the intensity of development, and the future management actions of landowners.

8.1.5. Earthwork Minimization

This source control measure seeks to limit the degree of clearing and grading on a development site in order to prevent soil compaction, conserve soil structure, prevent erosion from steep slopes, and protect zero-order streams. This concept can be applied in two ways by (1) minimizing the total site area that must be cleared and graded to complete the project; and (2) minimizing the site area that must be cleared and graded at any one time by completing large projects in phases, stabilizing one phase as the next phase is being cleared. This is accomplished by (1) identifying key soils, drainage features, and slopes to protect, and then (2) establishing limits of disturbance beyond which construction equipment is excluded. This element is an important but often under-utilized component of local erosion and sediment control plans.

Numerous researchers have documented the impact of mass grading, clearing, and the passage of construction equipment on the compaction of soils, as measured by increases in bulk density, declines in soil permeability, and increases in the runoff coefficient (Lichter and Lindsey, 1994; Legg et al., 1996; Schueler, 2001a, b; Gregory et al., 2006). Another goal of earthwork minimization is to protect zero-order streams, which are channels with defined banks that emanate from a hollow or ravine with convergent contour lines (Gomi et al., 2002). They represent the uppermost definable channels that possess temporary or intermittent flow. Functioning zero-order channels provide major watershed functions, including groundwater recharge and discharge (Schollen et al., 2006; Winter, 2007), important nutrient storage and transformation functions (Bernot and Dodds, 2005; Groffman et al., 2005), storage and retention of eroded hill slope sediments (Meyers, 2003), and delivery of leaf inputs and large woody debris. Compared to high-order network streams, zero-order streams are disproportionately disturbed by mass grading, enclosure, or channelization (Gomi et al., 2002; Meyers, 2003).

The practice of earthwork minimization is not widely applied across Virginia. This is partly due to the limited performance data available to quantify its benefits, and the absence of local or national design guidance or performance benchmarks for the practice.

8.1.6. Erosion and Sediment Control

Erosion and sediment control are critical to every construction project. Erosion and sediment control predates all other state and federal stormwater management efforts in Virginia. Methods to prevent the export of sediments should be planned during the site design process. These consist of the temporary installation and operation of a series of structural and nonstructural practices (see Figures 8.1 and 8.2) throughout the entire construction process to minimize soil erosion and prevent off-site delivery of sediment. Because construction is expected to last for a finite and short period of time, the design standards are usually smaller and thus riskier (25-year versus the 100-

year storm). By phasing construction, thereby limiting the exposure of bare earth at any one time, the risk to the environment is reduced significantly.

The basic practices include clearing limits, dikes, berms, temporary buffers, protection of drainage ways, soil stabilization through hydroseeding or mulching, perimeter controls, and various types of sediment traps and basins. All plans have some component that requires filtration of runoff crossing construction areas to prevent sediment from leaving the site. This usually requires a sediment collection system including, but not limited to, conventional settling ponds and advanced sediment collection devices such as polymer-assisted sedimentation and advanced sand filtration. Silt fences are commonly specified to filter distributed flows, and they require maintenance and replacement after storms. Filter systems are added to inlets until the streets are paved and the surrounding area has a cover of vegetation. Sediment basins are constructed to filter out sediments through rock filters, or are equipped with floating skimmers or chemical treatment to settle out pollutants. Other common erosion and sediment control measures include temporary seeding and rock or ribbed entrances to construction sites to remove dirt from vehicle tires.

Control of runoff's erosive potential is critical. Most erosion and sediment control manuals provide design guidance on the capacity and ability of swales to handle runoff without eroding, on the design of flow paths to transport runoff at non-erosive velocities, and on the dissipation of energy at pipe outlets. Examples include rock energy dissipators, level spreaders, and other such devices. Although erosion and sediment control practices are temporary, they require constant operation and maintenance during the complicated sequence of construction and after major storm events. It is exceptionally important to ensure that practices are frequently inspected and repaired and that sediments are cleaned out.

In Virginia, Erosion and Sediment Control is the subject of a completely separate regulatory program (§ 62.1-44.15:51 <u>et seq.</u>, Code of Virginia; 9 VAC 25-840 <u>et seq.</u>; *Virginia Erosion and Sediment Control Handbook, Third Edition*, 1992) and is not addressed further in this Handbook.



Figure 8.1. Temporary Silt Fence



Figure 8.2. Temporary Sediment Basin

8.1.7. Reforestation and Soil Compost Amendments

This set of practices seeks to improve the quality of native vegetation and soils present at the site. Depending on the ecoregion, this may involve forest or meadow plantings, tilling, and amending compacted soils to improve their hydrologic properties.

The goal is to maintain as much predevelopment hydrologic function at a development site as possible by retaining canopy interception, duff/soil layer interception, evapotranspiration, and surface infiltration. The basic methods to implement this practice are described in Cappiella et al. (2006), Pitt et al (2005), Chollak and Rosenfeld (1998), and Balusek (2003).

At this time, there are few monitoring data to assess the degree to which land reforestation or soil amendments can improve the quality of stormwater runoff at a particular development site, apart from the presumptive watershed research that has shown that forests with undisturbed soils have very low rates of surface runoff and extremely low levels of pollutants in runoff (Singer and Rust, 1975; Johnson et al., 2000; Chang, 2006). More data are needed on the hydrologic properties of urban forests and soils whose ecological functions are stressed or degraded by the urbanization process (Pouyat et al., 1995, 2007).

8.1.8. Pollution Prevention BMPs

By far the most effective control of NPS pollution is to *prevent its release*. This is especially true for stormwater hotspots. There are three families of runoff pollution prevention:

- Impervious surface reductions: reducing the amount of hard surfaces;
- Housekeeping techniques: basic clean-up and management practices;
- Construction practices (see E&S control above): techniques to prevent exposed soils from eroding, methods to reduce opportunities for sediment release into stormwater, and methods to catch sediment already suspended in stormwater

The stormwater-related problems associated with hotspots were described in **Chapter 6**. The keys to managing and treating runoff at hotspot sites are as follows:

- **Prevention**. The goal of pollution prevention is to prevent contact of rainfall or stormwater runoff with pollutants, and it is an important element of the post-construction stormwater plan. It is most important to design manage and store toxic materials on the site in a way that prevents opportunities for the pollutants to be exposed to rain and be washed into runoff.
- **Provide pre-treatment** devices between the source material and any stormwater control measures used to control general runoff from the site, especially if they involve infiltration. **Table 8.3** provides a matrix that indicates which control measures are appropriate for use at hotspot locations.

- **Inspect and correctly maintain** all pollution prevention or treatment elements at the site on a routine basis. Because of the extremely toxic nature of hotspot pollutants, it is extremely important that the stormwater control measures at hotspot sites be kept in good working order.
- **Train personnel** at the affected area to ensure that industrial and municipal managers and employees understand and implement the correct stormwater pollution prevention practices needed for their site or operation.

8.1.9. Runoff Volume Reduction – Rainwater Harvesting

A primary goal of stormwater management is to reduce the volume of runoff from impervious surfaces. There are several classes of BMPs that can achieve this goal, including rainwater harvesting systems, vegetated BMPs that evaporate and transpire part of the volume, and infiltration BMPs. For all of these measures, the amount of runoff volume to be captured depends on watershed goals, site conditions including climate, upstream nonstructural practices employed, and whether the chosen BMP is the sole management measure or part of a treatment train. Generally, runoff volume reduction BMPs are designed to handle at least the Treatment Volume from impervious surfaces (first 1-inch of rainfall). In Virginia, control of the 1-year 24-hour storm volume is considered the standard necessary to protect stream channel geomorphology, while base flow recharge can be addressed by capturing a much smaller volume (see **Chapter 10**).

Some designers have reported that in areas with medium to lower percentage of impervious surfaces, they are able to control up to the 100-year storm by enlarging runoff volume reduction BMPs and applying them to the entire site. In retrofit situations, capture amounts as small as 1 cm are a distinct improvement. It should be noted that there are important, although indirect, water quality benefits of all runoff volume reduction BMPs: (1) the reduction in runoff will reduce streambank erosion downstream and the concomitant increases in sediment load, and (2) volume reductions lead to pollutant mass load reductions, even if pollutant concentrations in stormwater are not decreased.

Rainwater harvesting systems refer to the use of captured runoff from roof tops in rain barrels, rain tanks, or cisterns (**Figures 8.3 and 8.4** below). This BMP treats runoff as a resource and is one of the few BMPs that can provide a tangible economic benefit through the reduction of treated water usage. Rainwater harvesting systems have substantial potential as retrofits via the use of rain barrels or cisterns that can replace lawn or garden sprinkling systems. Use of this BMP to provide gray water within buildings (e.g., for toilet flushing) is considerably more complicated due to the need to construct new plumbing and obtain the necessary permits.

The greatest challenge with these systems is the need to use the stored water and avoid having full tanks when the next storm occurs. That is, these BMPs are effective only if the captured runoff can be regularly used for some gray water usage, like car washing, toilet flushing, or irrigation (e.g., golf courses, landscaping, nurseries). In some areas it might be possible to use the water for drinking, showering, or washing, but treatment to potable water quality would be required. Sizing of the required storage is dependent on the climate patterns, the amount of impervious cover, and the frequency of water use. Areas with frequent rainfall events require less storage as long as the

water is used regularly, while areas with cold weather will not be able to utilize the systems for irrigation in the winter, and thus require larger storage.

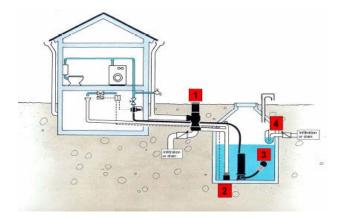




Figure 8.3. Rainwater Harvesting Schematic

Figure 8.4 Above-Ground Rain Tanks

One substantial advantage of these systems is their ability to reduce water costs for the user and the ability to share needs. An example of this interaction is the Pelican Hill development in Irvine, California, where excess runoff from the streets and houses is collected in enormous cisterns and used for watering of a nearby golf course. Furthermore, compared to other BMPs, the construction of rainwater harvesting facilities provides a long term benefit with minimal maintenance cost, although they do require an up-front investment for piping and storage tanks.

Coombes et al. (2000) found that rainwater harvesting achieved a 60-90 percent reduction in runoff volume. However, in general, few studies have been conducted to determine the performance of these BMPs. It should be noted that rainwater harvesting systems do collect airborne deposition and acid rain.

8.1.10. Runoff Volume Reduction

Runoff Volume Reduction – Vegetated

A large and very promising class of BMPMs includes those that use infiltration and evapotranspiration via vegetation to reduce the volume of runoff. These BMPs also directly address water quality of both surface water and groundwater by reducing streambank erosion, capturing suspended solids, and removing other pollutants from stormwater during filtration through the soil (although the extent to which pollutants are removed depends on the specific pollutant and the local soil chemistry). Depending on their design, these BMPs can also reduce peak flows and recharge groundwater (if they infiltrate). These BMPs can often be added as retrofits to developed areas by installing them into existing lawns, rights-of-way, or traffic islands. They can add also beauty and property value.

Flow volume is addressed by this BMP group by first capturing runoff, creating a temporary holding area, and then removing the stored volume through infiltration and evapotranspiration. Swales refer to grassy areas on the side of the road that convey drainage (**Figure 8.5** below). These were first designed to move runoff away from paved areas, but they can now be designed to achieve

a certain contact time with runoff, so as to promote infiltration and pollutant removal. Bioretention generally refers to a constructed depression or swale that encloses a filter media mix (often sand and organic material), with vegetation growing on top, to which stormwater runoff from impervious surfaces is directed (**Figure 8.6**). The original rain garden or bioretention facilities were constructed with an impermeable liner at the bottom of the prepared soil to prevent infiltration and instead had a low-level outflow at the bottom. Green roofs are very similar to bioretention BMPs (**Figure 8.7**). They tend to be populated with a light expanded shale-type soil and succulent plants chosen to survive wet and dry periods. Finally, bioinfiltration is similar to bioretention, but it is better engineered to achieve greater infiltration (**Figure 8.8**). All of these devices are usually at the upper end of a treatment train and designed for smaller storms, which minimizes their footprint and allows for incorporation within existing infrastructure (such as traffic control devices and median strips). This allows for distributed treatment of the smaller volumes and distributed volume reduction.



Figure 8.5. Vegetated Wet Swale



Figure 8.6. Parking Area Bioretention



Figure 8.7. Vegetated Roof



Figure 8.8. Retrofit Bioinfiltration

These BMPs work by capturing water in a vegetated area, which then infiltrates into the soil below. They are primarily designed to use plant material and soil to evaporate and transpire the runoff over several days following the storm. A shallow depth of ponding is required, since the inflows may exceed the possible infiltration capacity of the native soil. This ponding is maintained above an engineered sandy soil mixture and is a surface-controlled process (Hillel, 1998). Early in the

storm, the soil moisture potential creates a suction process that helps draw water into the BMP. This then changes to a steady rate that is "practically equal to the saturated hydraulic conductivity" of the subsurface (Hillel, 1998). The hydrologic design goal should be to maximize the volume of water that can be held in the soil, which necessitates consideration of the soil hydraulic conductivity (which varies with temperature), climate, depth to groundwater, and time to drain. Usually these devices are designed to empty between 24-72 hours after a storm event. In some cases (usually bioretention), these BMPs have an underdrain.

The choice of vegetation is an important part of the design of these BMPs. Many sites where infiltration is desirable have highly sandy soils, and the vegetation has to be able to endure both wet and dry periods. Long root growth is desired to promote infiltration (Minnesota Council, 2001), and plants that attract birds can reduce the insect population. Bioretention cells may be wet for longer periods than bioinfiltration sites, requiring different plants. Denser plantings or "thorns" may be needed to avoid the destruction caused by humans and animals taking shortcuts through the beds.

The pollutant removal mechanism operating for volume reduction BMPs are different for each pollutant type, soil type, and volume reduction mechanism. For bioretention and BMPs using infiltration, the sedimentation and filtration of suspended solids in the top layers of the soil are extremely efficient. Several studies have shown that the upper layers of the soil capture metals, particulate nutrients, and carbon (Pitt, 1996; Deschesne et al., 2005; Davis et al., 2008).

The removal of dissolved nutrients from stormwater is not as straightforward. While ammonia is caught by the top organic layer, nitrate is mobile in the soil column. Some bioretention systems have been built to hold water in the soil for longer periods in order to create anaerobic conditions that would promote denitrification (Hunt and Lord, 2006). Phosphorus removal is related to the amount of phosphorus in the original soil. Some studies have shown that bioretention cells built with agricultural soils actually *increased* the amount of phosphorus released. Chlorides pass through the system unchecked (Ermilio and Traver, 2006), while oils and greases are easily removed by the organic layer. Hunt et al. (2008) have reported in studies in North Carolina that the drying cycle appears to kill off bacteria. Temperature is not usually a concern, since most storms do not overflow these devices. Green roofs collect airborne deposition and acid rain and may export nutrients when they overflow. However, this must be tempered by the fact that in larger storms, most natural lands would produce nutrients.

A group of new research studies from North America and Australia have demonstrated the value of many of these runoff volume reduction practices to replicate predevelopment hydrology at the site. The results from 11 recent studies are given in **Table 8.1** below, which shows the runoff reduction capability of bioretention. As can be seen, the reduction in runoff volume achieved by these practices is impressive, ranging from 20-99 percent with a median reduction of about 75 percent. Bioswales installed during Seattle's natural drainage systems project also have demonstrated excellent results (see Horner et al., 2003; Jefferies, 2004; Stagge, 2006). Bioinfiltration has been less studied, but one field study concluded that close to 20 percent of the storm volume was removed by bioinfiltration (Sharkey, 2006). Capture of small storms through this kind of BMP appears to be extremely effective in areas where the majority of rain falls in smaller storms.

Table 8.1. Volumetric Runoff Reduction Achieved by Bioretention

Bioretention Design	Location	Runoff Reduction	Reference
	CT	99%	Dietz and Clausen (2006)
Infiltration	PA	86%	Ermiliao and Traver (2006)
militration	FL	98%	Rushton (2002)
	AUS	73%	Lloyd et al. (2002)
	ONT	40%	Van Seters et al. (2006)
	Model	30%	Perez-Perdini et al. (2005)
	NC	40-60%	Smith and Hunt (2007)
Underdrain	NC	20-29%	Sharkey (2006)
	NC	52-56%	Hunt et al. (2008)
	NC	20-50%	Passeport et al. (2008)
	MD	52-65%	Davis et al. (2008)

Source: NRC (2008)

The strengths of vegetated runoff volume reduction BMPs include the flexibility to use the drainage system as part of the treatment train. For example, bioswales can replace drainage pipes, green roofs can be installed on buildings, and bioretention can replace parking borders, thereby reducing the footprint of the stormwater system. Also, through the use of swales and reducing pipes and inlets, costs can be offset. Vegetated systems are more tolerant of the TSS collected, and their growth cycle maintains pathways for infiltration and prevents clogging. Freeze-thaw cycles also contribute to pathway maintenance. The aesthetic appeal of vegetated BMPs is also a significant strength.

Weaknesses include the dependence of these BMPs on native soil infiltration and the need to understand groundwater levels and karst geology, particularly for those BMPs designed to infiltrate. For bioinfiltration and bioretention, most failures occur early on and are caused by sedimentation and construction errors that reduce infiltration capacity, such as stripping off the topsoil and compacting the subsurface. Once a good grass cover is established in the contributing area, the danger of sedimentation is reduced. Nonetheless, the need to prevent sediment from overwhelming these structures is critical. The longevity of these BMPs and their vulnerability to toxic spills are a concern (Emerson and Traver, 2008), as is their failure to reduce chlorides. Finally, in areas where the land use is a hot spot, or where (the BMP could potentially contaminate the groundwater supply, bioretention, non-infiltrating bioswales, and green roofs may be more suitable than infiltration BMPs.

The role of infiltration BMPs in promoting groundwater recharge deserves additional consideration. Although this is a benefit of infiltration BMPs in regions where groundwater levels are dropping, it may be undesirable in a few limited scenarios. For example, in most urban areas, there is so much impervious cover that it would be difficult to "over-infiltrate." Nonetheless, the use of infiltration BMPs will change local subsurface hydrology, and the ramifications of this – good and bad – should be considered prior to their installation.

Maintenance of vegetated runoff reduction BMPs is relatively simple. A visit after a rainstorm to check for plant health, to check sediment buildup, and to see if the water is ponded can answer many questions. Maintenance includes trash pickup and seasonal removal of dead grasses and

weeds. Sediment removal from pretreatment devices is required. Depending on the pollutant concentrations in the influent, the upper layer of organic matter may need to be removed infrequently to maintain infiltration and to prevent metal and nutrient buildup.

At the site level, the chief factors that lead to uncertainty are the infiltration performance of the soil, particularly for the limiting subsoil layer, and how to predict the extent of pollutant removal. Traditional percolation tests are not effective to estimate the infiltration performance; rather, testing hydraulic conductivity is required. Furthermore, the infiltration rate varies depending on temperature and season (Emerson and Traver, 2008). Basing measurements on percent removal of pollutants is extremely misleading, since every site and storm generates different levels of pollutants. The extent of pollutant removal depends on land use, time between storms, seasons, and so forth. These factors should be part of the design philosophy for the site.

Finally, it should also be pointed out that climate is a factor determining the effectiveness of some of these BMPs. For example, green roofs are more likely to succeed in areas having smaller, more frequent storms, compared to areas subject to less frequent, more intense storms.

Runoff Volume Reduction - Subsurface

Infiltration is the primary runoff volume reduction mechanism for subsurface BMPs, such that much of the previous discussion is relevant here. Thus, like vegetated BMPs, these BMPs provide benefits for groundwater recharge, water quality, stream channel protection, peak flow reduction, capture of the suspended solids load, and filtration through the soil (Ferguson, 2002). Because these systems can be built in conjunction with paved surfaces (i.e., they are often buried under parking lots), the amount of water captured, and thus stream protection, may be higher than for vegetated systems. They also have lower land requirements than vegetated systems, which can be an enormous advantage when using these BMPs during retrofitting, as long as the soil is conducive to infiltration.

Similar to vegetated BMPs, this BMP group works primarily by first capturing runoff and then removing the stored volume through infiltration. The temporary holding area is made either of stone or using manufactured vaults. Examples include infiltration trenches, seepage pits (dry wells), and permeable pavement (see **Figures 8.9**, **8.10**, **8.11**, and **8.12** below). As with vegetated BMPs, a shallow depth of ponding is required, since the inflows may exceed the possible infiltration ability of the native soil. In this case, the ponding is maintained within a rock bed under a permeable pavement or in an infiltration trench. These devices are usually designed to empty between 24-72 hours after the storm event.

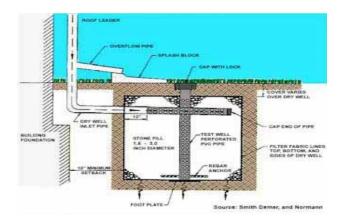


Figure 8.9. Seepage Pit (Dry Well) Schematic



Figure 8.10. Infiltration Trench



Figure 8.11. Porous Asphalt



Figure 8.12. interlocking Permeable Pavers

The infiltration processes operating for these subsurface BMPs are similar to those for the vegetated devices previously discussed. Thus, much like for vegetated systems, the level of control achieved depends on the infiltration ability of the native soils, the percent of impervious surface area in the contributing watershed, land use contributing to the pollutant loadings, and climate. A large number of recent studies have found that permeable pavement can reduce runoff volume by anywhere from 50 percent (Rushton, 2002; Jefferies, 2004; Bean et al., 2007) to as much as 95 percent or greater (van Seters et al., 2006; Kwiatkowski et al., 2007). Villanova University's Stormwater Research and Demonstration Park has successfully demonstrated a retrofit of standard asphalt with permeable pavement.

The strengths of subsurface runoff volume reduction BMPs are similar to those of their vegetated counterparts. Additional attributes include their ability to be installed under parking areas and to manage larger volumes of rainfall. These BMPs typically have few problems with safety or vector-borne diseases because of their subsurface location and storage capacity, and they can be very aesthetically pleasing. The potential of permeable pavement could be particularly far-reaching if one considers the amount of impervious surface in urban areas that is comprised of roads, driveways, and parking lots.

The weaknesses of these BMPs are also similar to those of vegetated systems, including their dependence on native soil infiltration and the need to understand groundwater levels and karst geology. Simply estimating the soil hydraulic conductivity can have an error rate of an order of magnitude. Specifically for subsurface systems that use geotextiles (not permeable pavement), there is a danger of TSS being compressed against the bottom of the geotextile, preventing infiltration. There are no freeze-thaw cycles or vegetated processes that can reopen pathways, so the control of TSS is even more critical to their life span. In most cases (permeable pavement is an exception), pretreatment is required, except for the cleanest of sources (like a slate roof). Typically, manufactured devices, sediment forebays, or grass filter strips are part of the design of subsurface BMPs to capture the larger sediment particles.

The maintenance of subsurface runoff volume reduction BMPs is relatively simple but critical. If inspection wells are installed, a visit after a rainstorm will check that the volume is captured, and later that it has infiltrated. Porous surfaces should undergo periodic vacuum street sweeping when a sediment source is present. Pretreatment devices require sediment removal. The difficulty with this class of BMPs is that, if a toxic spill occurs or maintenance is not proactive, there are no easy corrective measures other than replacement.

Low Impact Development (LID). LID refers primarily to the use of small, engineered, on-site stormwater practices to treat the quality and quantity of runoff at its source. It is discussed here because the BMPs that are thought of as LID – particularly vegetated swales, green roofs, permeable pavement, and rain gardens – are all runoff volume reduction BMPs. They are designed to capture the first portion of a rainfall event and to treat the runoff from a few hundred square meters of impervious cover.

As discussed earlier, several studies have measured the runoff volume reduction of individual LID practices. Fewer studies are available on whether multiple LID practices, when used together, have a cumulative benefit at the neighborhood or catchment scale. Several monitoring studies have clearly documented a major reduction in runoff from developments that employ LID and Environmental Site Design, compared to those that do not. In addition, six studies have documented the runoff reduction benefits of LID at the catchment or watershed scale, using a modeling approach (Alexander and Heaney, 2002; Stephens et al., 2002; Holman-Dodds et al., 2003; Coombes, 2004; Hardy et al., 2004; and Huber et al., 2006).

8.1.11. Peak Flow Reduction and Runoff Treatment

Peak Flow Reduction

After efforts are made to prevent the generation of pollutants and to reduce the volume of runoff that reaches stormwater systems, stormwater management focuses on the reduction of peak flows and associated treatment of polluted runoff. The main class of BMPs used to accomplish this is pond-type practices, versions of which have dominated stormwater management for decades. These include a wide variety of ponds and wetlands, including wet ponds (also known as retention basins), dry extended detention ponds (also known as detention basins), and constructed wetlands. By holding a volume of stormwater runoff for an extended period of time, pond-type BMPs can achieve both water quality improvement and reduced peak flows.

Generally the goal is to hold the flows for at least 24 hours to maximize the opportunity of settling, adsorption, and transformation of pollutants (based on past pollutant removal studies) (Rea and Traver, 2005). For smaller storm events (one-year storms), this added holding time also greatly reduces the outflows from the BMP to a level that the stream channel can handle. Most wet ponds and stormwater wetlands can hold a "treatment volume," such that the flows leaving in smaller storms have been held and "treated" for multiple days. Extended detention dry ponds also greatly reduce the outflow peaks to achieve the required residence times.

Usually pond-type devices are lower in the treatment train of BMPs, if not at the very end. This is both due to their function (they are designed for larger events) and because the required water sources and less permeable soils needed for these BMPs are more likely to be found at the lower areas of the site. Some opportunities exist to naturalize dry ponds or to retrofit wet ponds into stormwater wetlands, but it depends on their site configuration and hydrology. A wet pond is shown in **Figure 8.13**. A stormwater wetland and a dry extended basin are shown in **Figures 8.14** and **8.15**.



Figure 8.13. Wet Pond



Figure 8.14. Constructed Wetland



Figure 8.15. Dry Extended Detention Basin

Simple ponds are little more than a hole in the ground, in which stormwater is piped in and out. Dry ponds are meant to be dry between storms, whereas wet ponds have a permanent pool throughout the year. Detention basins reduce peak flows by restricting the outflows and creating a storage area. Depending on the detention time, outflows can be reduced to levels that do not accelerate erosion, that protect the receiving stream channel, and that reduce flooding.

The flow normally enters the structure through a sediment forebay (**Figure 8.16**), which is included to capture incoming sediment, remove the larger particles through settling, and allow for easier maintenance. Then a meandering path or cell structure is built to "extend" and slow down flows. The main basin is a large storage area (sometimes over the meandering flow paths). Finally, the runoff exits through an outflow control structure built to retard flow.



Figure 8.16. Sediment Forebay, with Wet Pond in the Background

Wet ponds, stormwater wetlands, and (to a lesser extent) dry extended detention basins provide treatment. The first step in the pond treatment process is the settling of larger particles in the sediment forebay. Next, for wet ponds a permanent pool of water is maintained so that, for smaller storms, the new flows push out a volume that has had a chance to interact with vegetation and be "treated." This volume is equivalent to an inch of rain over the impervious surfaces in the drainage area. Thus, what exits the BMP during smaller storm events is base flow contributions and runoff that entered during previous events. For dry extended detention ponds, there is no permanent pool and the outlet is instead greatly restricted. For all of these devices, vegetation is considered crucial to pollutant removal. Indeed, wet ponds are designed with an aquatic bench around the edges to promote contact with plants. The vegetation aids in reduction of flow velocities (through friction), provides growth surfaces for microbes, takes up pollutants such as nutrients, and provides filtering (Braskerud, 2001).

The ability of pond structures to achieve a certain level of control is size related – that is, the more peak flow reduction or pollutant removal required, the more volume and surface area are needed in the basin. Because it is not simply the peak flows that are important, but also the duration of the flows that cause damage to the receiving stream channels (McCuen, 1979; Loucks et al., 2005), some ponds are currently sized and installed in series with runoff volume reduction BMPs.

The strength of pond-type devices is the opportunity to create habitats or picturesque settings in conjunction with stormwater management. The weaknesses of these measures include large land requirements, chloride buildup, possible temperature effects (i.e., warming), and the risk of creating habitat for undesirable species in urban areas. There is a perception that these devices promote mosquitoes, but that has not been found to be a problem when a healthy biological habitat is created (Greenway et al., 2003). Another drawback of this class of BMPs is that they often have limited treatment capacity, in that they can reduce pollutants in stormwater only to a certain level. These so-called irreducible effluent concentrations have been documented mainly for ponds and stormwater wetlands, as well as for sand filters and grass channels (Schueler, 1998). Finally, it should be noted that either a larger watershed (10-25 acres: CWP, 2004) or a continuous water source is needed to sustain wet ponds and stormwater wetlands.

Maintenance requirements for ponds and wetlands include the removal of built-up sediment from the sediment forebay, harvesting of grasses to remove accumulated nutrients, and repair of berms and structures after damaging storm events. Inspection items relate to the maintenance of the dam and sediment forebay.

While the basic hydrologic function of extended detention devices is well known, their performance on a watershed basis is not. Because they do not significantly reduce runoff volume and are designed on a site-by-site basis using synthetic storm patterns, their exclusive use as a flood reduction strategy at the watershed scale is uncertain (McCuen, 1979; Traver and Chadderton, 1992). Much of this variability is reduced when they are coupled with volume reduction BMPs at the watershed level. Pollutant removal is effected by climate, short-circuiting of flows through the device, and by the schedule of sediment removal and plant harvesting. Extreme events can re-suspend captured sediments, thus reintroducing them into the environment. Although it is the subject of much debate, it seems likely that plants will need to be harvested to accomplish nutrient removal (Reed et al., 1998).

Runoff Treatment

As mentioned above, many BMPs associated with runoff volume reduction and extended detention provide a water quality benefit. There are also some BMPs that focus primarily on water quality with little peak flow or volume effect. Designed for smaller storms, these are usually based on filtration, hydrodynamic separation, or small-scale bioretention systems that drain to a subsequent receiving water or other device. Thus, often these BMPs are used in conjunction with other devices in a treatment train or as retrofits under parking lots. They can be very effective as pretreatment devices when used "higher up" in the watershed than infiltration structures. Finally, in some cases these BMPs are specifically designed to reduce peak flows in addition to providing water quality benefits by introducing elements that make them similar to detention basins. This is particularly the case for sand filters.

The sand filter is relied upon as a treatment technology in many regions, particularly those where stream geomorphology is less of a concern, and thus peak flow control and runoff volume reduction are not the primary goals. These devices can be effective at removing suspended sediments and can extend the longevity and performance of runoff volume reduction BMPs. They are also one of the few urban retrofit practices available, due to the ability to implement them within traditional culvert systems. **Figures 8.17 and 8.18** show designs for the Austin sand filter and Delaware sand filter.





Figure 8.17. Austin Sand Filter

Figure 8.18. Delaware Sand Filter

Filters use sand, peat, or compost to remove particulates, similar to the processes used in drinking water treatment plants. Sand filters primarily remove suspended solids and ammonia nitrogen. Biological material, such as peat or compost, provides adsorption of contaminants such as dissolved metals, hydrocarbons, and other organic chemicals.

Manufactured Treatment Devices (MTDs)

There are several types of manufactured stormwater treatment devices in the marketplace, and more are being designed all the time. Hydrodynamic devices use rotational forces to separate the solids from the flow, allowing the solids to settle out of the flow stream. There is a recent class of bioretention-like manufactured devices that combine inlets with planters. In these systems, small volumes are directed to a soil planter area, with larger flows bypassing and continuing down the storm sewer system. In any event, for manufactured treatment devices (MTDs) the user needs to look to the manufacturer's published and reviewed data to understand how the device should be applied.

The level of control that can be achieved with these BMPs depends entirely on sizing of the device based on the incoming flow and pollutant loads. Each unit has a certified removal rate depending on inflow to the BMP. Also, all units have a maximum volume or rate of flow they can treat, such that higher flows are bypassed with no treatment. Thus, the user has to determine what size unit is needed and the number to use, based on the area's hydrologic cycle and what criteria are to be met.

With the exception of some types of sand filters, the strengths of water quality treatment BMPs are that they can be placed within existing infrastructure or under parking lots, and thus do not take

up land that may be used for other purposes. They make excellent choices for retrofit situations. For filters, there is a wealth of experience from the water treatment community on their operations. There are several testing protocols, including the new Virginia Technology Assessment Protocol (VTAP), that have been established to validate the performance of MTDs (the sufficiency of the testing protocols is discussed below).

Weaknesses of these devices include their cost and maintenance requirements. Regular maintenance and inspection at a high level are required to remove captured pollutants, to replace mulch, or to rake and remove the surface layer to prevent clogging. In some cases, specialized equipment (vacuum trucks) is required to remove built-up sediment. Although the underground placement of these devices has many benefits, it makes it easy to neglect their maintenance because there are no signs of reduced performance on the surface. Because these devices are manufactured, the unit construction cost is usually higher than for other BMPs. Finally, the numerous testing protocols are confusing and inhibit more widespread applications.

The chief uncertainty with these BMPs is due to the lack of certification of some MTDs. There is also concern about which pollutants are removed by which class of device. For example, hydrodynamic devices and sand filters do not address dissolved nutrients, and in some cases convert suspended pollutants to their dissolved form. Both issues are related to the false perception that a single BMP must be found that will comprehensively treat stormwater. Such pressures often put vendors in a position of trying to certify that their devices can remove *all* pollutants. Most often, these devices can serve effectively as part of a treatment train, and they should be valued for their incremental contributions to water quality treatment. For example, a filter that removes sediment upstream of a bioinfiltration BMP can greatly prolong the life of the infiltration device.

Testing of MTDs

Manufacturers of proprietary BMPs offer a service that can save municipalities/developers time and money. Time is saved by the ability of the manufacturers to quickly select a model matching the needs of the site. A city can minimize the cost of buying the product by requiring the different manufacturers to submit bids for the site. All the benefits of the service will have no meaning, however, if the cities/developers cannot trust the performance claims of the different products. Because the United States does not have, at this time, a national program to verify the performance of MTDs, interested municipalities and developers face a high amount of uncertainty when they select a product. Money could be wasted on products that might have the lowest bid, but do not achieve the water quality goals of the municipality or state.

The U.S. EPA's Environmental Technology Verification (ETV) program was created to facilitate the deployment of innovative or improved environmental technologies through performance verification and dissemination of information. The Wet Weather Flow Technologies Pilot project was established as part of the ETV program to verify commercially available technologies used in the abatement and control of urban stormwater runoff, combined sewer overflows, and sanitary sewer overflows. Ten proprietary BMPs were tested under the ETV program, and the results of the monitoring are available on the National Sanitation Foundation website. Unfortunately, the funding for the ETV program was discontinued before all the stormwater products could be tested. Without a national testing program, some states have taken a more regional approach to verifying

the performance of proprietary practices, while most states do not have any type of verification or approval program.

The Washington Department of Ecology has supported a testing protocol called Technology Assessment protocol – Ecology (TAPE) that describes a process for evaluating and reporting on the performance and appropriate uses of emerging MTDs. California, Massachusetts, Maryland, New Jersey, Pennsylvania, and Virginia have sponsored a testing program called Technology Acceptance and Reciprocity Partnership (TARP), through which a number of products are being tested in the field. The state of Wisconsin has prepared a draft technical standard (2006) describing methods for predicting the site-specific reduction efficiency of proprietary sedimentation devices. To meet the criteria in the standard, the manufacturers can either use a model to predict the performance of the practice or complete a laboratory protocol designed to develop efficiency curves for each product. Although none of these state or federal verification efforts have produced enough information to sufficiently reduce the uncertainty in selection and sizing of MTDs, many proprietary practices are being installed around the country, because of the perceived advantage of the service being provided by the manufacturers and the sometimes overly optimistic performance claims.

All those involved in stormwater management, including the manufacturers, will have a much better chance of implementing a cost-effective stormwater program in their cities if the barriers to a national testing program for MTDs are eliminated. Two of the barriers to the ETV program were high cost and the transferability of the results. Also, the ETV testing did not produce results that could be used in developing efficiency curves for the product. There have been discussions about establishing a new national testing program that could reduce testing costs by using laboratory testing instead of field testing. However, many consider field testing to be very important to determine if laboratory test results are actually transferrable to the real world. The new VTAP is Virginia's method of building upon the other existing protocols to better evaluate how MTDs perform. The VTAP will be implemented through the DEQ's Virginia Stormwater BMP Clearinghouse.

8.1.12. Aquatic Buffers and Managed Floodplains

Establishing aquatic buffers, also called stream buffers or riparian buffers (**Figures 8.19 and 8.20** below), involves reserving a vegetated zone adjacent to streams, shorelines, or wetlands in response to development regulations or a local ordinance. In most regions of the country, including Virginia, forest vegetation is preferred. When properly designed, buffers can both reduce runoff volumes and provide water quality treatment of stormwater.

The performance of urban stream buffers cannot be predicted from studies of buffers installed to remove sediment and nutrients from agricultural areas (Lowrance and Sheridan, 2005). Agricultural buffers have been reported to have high sediment and nutrient removal because they intercept sheet flow or shallow groundwater flow in the riparian zone. By contrast, urban stream buffers often receive concentrated surface runoff or may even have a storm drain pipe that short-circuits the buffer and directly discharges into the stream. Consequently, the pollutant removal capability of urban stream buffers is limited, unless they are specifically designed to distribute and treat stormwater runoff (NRC, 2000). This involves the use of level spreaders, grass filters, and

berms to transform concentrated flows into sheet flow (Hathaway and Hunt, 2006). Such designed urban stream buffers have been applied widely in the Neuse River basin in North Carolina and in Henrico County in Virginia to reduce urban stormwater nutrient inputs to nutrient-sensitive water bodies.





Figure 8.19. Buffered Stream

Figure 8.20. Residential Riparian Buffer

The primary benefit of buffers is to help maintain aquatic biodiversity within the stream. Numerous researchers have evaluated the relative impact of riparian forest cover and impervious cover on stream geomorphology, aquatic insects, fish assemblages, and various indexes of biotic integrity. As a group, the studies suggest that indicator values for urban stream health increase when riparian forest cover is retained over at least 50 to 75 percent of the length of the upstream network (Goetz et al., 2003; Wang et al., 2003; McBride and Booth, 2005; Moore and Palmer, 2005). There is also general agreement that buffering headwater streams is more important than buffering higher order streams, since the headwaters provide the foundation for the aquatic food chain and ecologic health.

The width of the buffer is also important for enhancing its stream protection benefits. Recommended widths range from 25 to 200 feet depending on stream order, protection objectives, and community ordinances. Eastern Virginia communities subject to the Chesapeake Bay Preservation Act (CBPA) are required to designate lands near streams, rivers and open water as Resource Protection Areas, part of which is a 100-foot wide riparian buffer next to the water. Some other Virginia communities, as well, have added buffer requirements to their local codes to protect water quality, biodiversity, and general stream health. However, the beneficial impact of riparian forest cover may diminish as watershed impervious cover grows beyond 15 percent, when degradation by stormwater runoff can overwhelm the benefits of the riparian forest (Roy et al., 2005, 2006; Walsh et al., 2007).

Maintenance, inspection, and compliance for buffers can be a problem. In most communities, urban stream buffers are simply a line on a map and are not managed in any significant way after construction is over. As such, urban stream buffers are prone to residential encroachment and clearing, and to colonization by invasive plants.

Another important practice is to protect, preserve, or otherwise manage the ultimate 100-year floodplain so that vulnerable property and infrastructure are not damaged during extreme floods. Federal Emergency Management Agency (FEMA), state, and local requirements often restrict or control development on land within the floodway or floodplain. In larger streams, the floodway and aquatic buffer can be integrated together to achieve multiple social objectives.

8.1.13. Stream Rehabilitation

While not traditionally considered an BMP, certain stream rehabilitation practices or approaches can be effective at recreating stream physical habitat and ecosystem function lost during urbanization. When combined with effective BMPs in upland areas, stream rehabilitation practices can be an important component of a larger strategy to address stormwater. From the standpoint of mitigating stormwater impacts, four types of urban stream rehabilitation are common:

• Practices that stabilize streambanks and/or prevent channel erosion/enlargement can reduce downstream delivery of sediments and attached nutrients (Figures 8.21 and 8.22). Although the magnitude of sediment delivery from urban-induced stream channel enlargement is well documented, there are very few published data to quantify the potential reduction in sediment or nutrients from subsequent channel stabilization.







Figure 8.22. After Stream Restoration

Streams can be hydrologically reconnected to their floodplains by building up the profile of incised urban streams using grade controls so that the channel and floodplain interact to a greater degree. Urban stream reaches that have been so rehabilitated have increased nutrient uptake and processing rates and, in particular, increased denitrification rates, compared to degraded urban streams prior to treatment (Bukavecas, 2007; Kaushal et al., 2008). This suggests that urban stream rehabilitation may be one of many elements that can be considered to help decrease loads in nutrient-sensitive watersheds.

 Practices that enhance in-stream habitat for aquatic life can improve the expected level of stream biodiversity. However, Konrad (2003) notes that improvement of biological diversity of urban streams should still be considered an experiment, since it is not always clear what hydrologic, water quality, or habitat stressors are limiting. Larson et al. (2001) found that physical habitat improvements can result in no biological improvement at all. In addition, many of the biological processes in urban stream ecosystems remain poorly understood, such as carbon processing and nutrient uptake.

• Some stream rehabilitation practices can indirectly increase stream biodiversity (such as riparian reforestation, which could reduce stream temperatures, and the removal of barriers to fish migration).

It should be noted that the majority of urban stream rehabilitation projects undertaken in the United States are designed for purposes other than mitigating the impacts of stormwater or enhancing stream biodiversity or ecosystem function (Bernhardt et al., 2005). Most stream rehabilitation projects have a much narrower design focus, and are intended to protect threatened infrastructure, naturalize the stream corridor, achieve a stable channel, or maintain local streambank stability (Schueler and Brown, 2004). Improvements in either biological health or the quality of stormwater runoff have rarely been documented.

Unique design models and methods are required for urban streams, compared to their natural or rural counterparts, given the profound changes in hydrologic and sediment regime and stream-floodplain interaction that they experience (Konrad, 2003). While a great deal of design guidance on urban stream rehabilitation has been released in recent years (FISRWG, 2000; Doll and Jennings, 2003; Schueler and Brown, 2004), most of the available guidance has not yet been tailored to produce specific outcomes for stormwater mitigation, such as reduced sediment delivery, increased nutrient processing, or enhanced stream biodiversity. Indeed, several researchers have noted that many urban stream rehabilitation projects fail to achieve even their narrow design objectives for a wide range of reasons (Bernhardt and Palmer, 2007; Sudduth et al., 2007). This is not surprising given that urban stream rehabilitation is relatively new and rarely addresses the full range of in-stream alteration generated by watershed-scale changes. This shortfall suggests that much more research and testing are needed to ensure that urban stream rehabilitation can meet its promise as an emerging BMP.

8.1.14. Municipal Housekeeping

Phase II NPDES/VPDES stormwater permits specifically require municipal good housekeeping as one of the six minimum management measures for MS4s. Although the EPA has not presented definitive guidance on what constitutes "good housekeeping," CWP (2008a) outlines ten municipal operations where housekeeping actions can improve the quality of stormwater, including the following:

- Municipal hotspot facility management;
- Municipal construction project management;
- Road maintenance;
- Street sweeping;
- Storm drain maintenance;
- Stormwater hotline response;
- Landscape and park maintenance;
- BMP maintenance; and
- Employee training.

The overarching theme is that good housekeeping practices at municipal operations provide source treatment of pollutants before they enter the storm drain system. The most frequently applied practices are street sweeping (**Figure 8.23**) and sediment cleanouts of sumps and storm drain inlets (**Figure 8.24**). Most communities conduct both operations at some frequency for safety and aesthetic reasons, although not specifically for the sake of improving stormwater quality (Law et al., 2008).





Figure 8.23. Street Sweeping

Figure 8.24. Catch Basin Cleaning

Numerous performance monitoring studies have been conducted to evaluate the effect of street sweeping on the concentration of stormwater pollutants in downstream storm drain pipes (see Pitt, 1979; Bender and Terstriep, 1994; Brinkman and Tobin, 2001; Zarrielo et al., 2002; Chang et al., 2005; USGS, 2005; Law et al., 2008). The basic finding is that regular street sweeping has a low or limited impact on stormwater quality, depending on street conditions, sweeping frequency, sweeper technology, operator training, and on-street parking. Sweeping will always have a limited removal capability because rainfall events frequently wash off pollutants before the sweeper passes through, and only some surfaces are accessible to the sweeper, thus excluding sidewalk, driveways, and landscaped areas. However, frequent sweeping (i.e., weekly or monthly) has a moderate capability to remove sediment, trash and debris, coarse solids, and organic matter.

Fewer studies have been conducted on the pollutant removal capability of frequent sediment cleanout of storm drain inlets, most in regions with arid climates (Lager et al., 1977; Mineart and Singh, 1994; Morgan et al., 2005). These studies have shown some moderate pollutant removal if cleanouts are done on a monthly or quarterly basis. Most communities, however, report that they clean out storm drains on an annual basis or in response to problems or drainage complaints (Law, 2006).

Frequent sweeping and cleanouts conducted on the dirtiest streets and storm drains appear to be the most effective way to include these operations in the stormwater treatment train. However, given the uncertainty associated with the expected pollutant removal for these practices, street sweeping and storm drain cleanout cannot be relied on as the sole BMPs for an urban area.

8.1.15. Illicit Discharge Detection and Elimination

MS4 communities must develop a program to detect and eliminate illicit discharges to their storm drain system as a stormwater NPDES/VPDES permit condition. Illicit discharges can involve illegal cross-connections of sewage or washwater into the storm drain system or various intermittent or transitory discharges due to spills, leaks, dumping, or other activities that introduce pollutants into the storm drain system during dry weather. National guidance on the methods to find and fix illicit discharges was developed by Brown et al. (2004). Local illicit discharge detection and elimination (IDDE) programs represent an ongoing and perpetual effort to monitor the network of pipes and ditches to prevent pollution discharges.

The water quality significance of illicit discharges has been difficult to define since they occur episodically in different parts of a municipal storm drain system. Field experience in conducting outfall surveys does indicate that illicit discharges may be present at 2-5 percent of all outfalls at any given time. Given that pollutants are being introduced into the receiving water during dry weather, illicit discharges may have an amplified effect on water quality and biological diversity.

Many communities indicate that they employ a citizen hotline to report illicit discharges and other water quality problems (Brown et al., 2004), which sharply increases the number of illicit discharge problems observed.

8.1.16. Stormwater Management Education

Like IDDE, public information and education about stormwater is one of the six minimum management measures that MS4 communities must address in their stormwater NPDES/VPDES permits. Stormwater education involves municipal efforts to make sure individuals understand how their daily actions can positively or negatively influence water quality and work to change specific behaviors linked to specific pollutants of concern (Schueler, 2001c). Targeted behaviors include lawn fertilization and pesticide application, clipping and leaf disposal, littering, car fluid recycling, car washing, household hazardous waste management, septic system maintenance, and pet waste pickup.

Communities may use a wide variety of messages to make the public aware of the behavior and more desirable alternatives through internet websites, utility bill inserts, brochures and fact sheets, radio, television, newspaper ads, special events, workshops, or door-to-door outreach by volunteer educators. Communities can also coordinate programs to engage citizens in stormwater pollution prevention and watershed management activities, such as stream monitoring, stream clean-ups, adopt-a-stream programs, tree planting days, and storm drain stenciling.

Several communities have performed before-and-after surveys to assess both the penetration rate for these campaigns and their ability to induce changes in actual behaviors. Significant changes in behaviors have been recorded (see Schueler, 2002), although few studies are available to link specific stormwater quality improvements to the educational campaigns (but see Turner, 2005; CASQA, 2007).

8.1.17. Residential Stewardship

This BMP involves municipal programs to enhance residential stewardship to improve stormwater quality. Residents can undertake a wide range of activities and practices that can reduce the volume or quality of runoff produced on their property or in their neighborhood as a whole. This may include installing rain barrels or rain gardens, planting trees, xeriscaping, downspout disconnection, storm drain marking, household hazardous waste pickups, proper disposal of waste oil products (**Figure 8.25**), carefully managing application of de-icing products to sidewalks and driveways, and yard waste composting (CWP, 2005). This expands on stormwater education in that a municipality provides a convenient delivery service to enable residents to engage in positive watershed behavior.

The effectiveness of residential stewardship is enhanced when carrots are provided to encourage the desired behavior, such as subsidies, recognition, discounts, and technical assistance (CWP, 2005). Consequently, communities need to develop a targeted program to educate residents and help them engage in the desired behavior.



Figure 8.25. Don't Pour Waste Oil Products Down the Storm Drain!

8.2. OVERVIEW OF POST-CONSTRUCTION BMPs

This section generally describes the post-construction Stormwater Control Measures (BMPs) that may be used in Virginia to manage stormwater runoff. Given the large number and wide variety of MTDs in the marketplace and the pace at which new devices are being introduced, this Handbook will not provide any detail about such devices. However, additional information can be found at the Virginia Stormwater BMP Clearinghouse web site at http://www.vwrrc.vt.edu/swc/ and in Minton (2005). More specific information about ESD practices and techniques can be found in CWP (1998a). The various BMPs were selected based on their ability to achieve, at varying degrees, the following:

- 1. Can capture and treat the full Treatment Volume (T_v)
- 2. Can reduce the volume of stormwater runoff
- 3. Can remove total phosphorus (TP) from site runoff (regulatory compliance criteria)
- 4. Can remove total nitrogen (TN) from site runoff
- 5. Can remove total suspended solids (TSS) from runoff
- 6. Can remove other pollutants as well (e.g., hydrocarbons, bacteria, metals)
- 7. Can address stormwater quantity (channel protection criteria, and flood protection) criteria

8. Have acceptable longevity in the field, when maintained properly.

8.2.1. Pollutant Removal Mechanisms

Stormwater control measures remove pollutants from stormwater runoff through various physical, chemical, and biological processes. **Table 8.2** lists the major stormwater pollutant removal processes and the affected stormwater pollutants.

Table 8.2. Stormwater Pollutant Removal Processes

Process	Pollutants Affected		
	Solids, BOD, pathogens, particulate COD,		
Gravity settling of particulate pollutants	phosphorus, nitrogen, synthetic organics,		
	particulate metals		
Filtration and physical straining of pollutants	Solids, BOD, pathogens, particulate COD,		
through a filter media or vegetation	phosphorus, nitrogen, synthetic organics,		
tillough a filler media of vegetation	particulate metals		
	Solids, BOD, pathogens, particulate COD,		
Infiltration of particulate and dissolved pollutants	phosphorus, nitrogen, synthetic organics,		
	particulate metals		
Adsorption on particulates and sediments	Dissolved phosphorus, metals, synthetic organics		
Photodegradation	COD, petroleum hydrocarbons, synthetic		
Filotodegradation	organics, pathogens		
Gas exchange and volatilization	Volatile organics, synthetic organics		
Biological uptake and biodegradation	BOD, COD, petroleum hydrocarbons, synthetic		
Biological uptake and biodegradation	organics, phosphorus, nitrogen, metals		
Chemical precipitation	Dissolved phosphorus, metals		
Ion exchange	Dissolved metals		
Oxidation	COD, petroleum hydrocarbons, synthetic		
Oxidation	organics		
Nitrification and denitrification	Ammonia, nitrate, nitrite		
Density separation and removal of floatables	Petroleum hydrocarbons		

Source: NRC (2008)

Since many pollutants in urban stormwater runoff are attached to solid particles, treatment practices designed to remove suspended solids from runoff will remove other pollutants as well. Exceptions to this rule include nutrients, which are often in a dissolved form, soluble metals and organics, and extremely fine particulates (i.e., having a diameter smaller than 10 microns), which can only be removed by treatment practices other than traditional separation methods.

8.2.2. Approved Virginia Non-Proprietary Stormwater Control Measures

Virginia's approved BMPs can be organized into five groups, from rooftop to stream:

- Runoff volume reduction primary benefit is reducing the volume of runoff leaving the site
- Swales or open channels runoff conveyance practices that also provide various levels of pollution removal
- Filtering systems primary benefit is removing nutrients, sediment, heavy metals, grease and oil from runoff
- Infiltration practices these combine runoff volume reduction (runoff soaks into the soil) and pollution treatment (primarily from filtering)
- Basins –reduce the rate of runoff (detention), also improve pollution removal (wet ponds), and also add wildlife habitat (constructed wetlands)

8.2.2.1. Runoff Volume Reduction

1. Vegetated Roof (#5) (Figure 8.26). Vegetated roofs (also known as green roofs or eco roofs) are alternative roof surfaces that typically consist of waterproofing and drainage materials and an engineered growing media that is designed to support plant growth. Vegetated roofs capture and temporarily store stormwater runoff in the engineered growing media before it is conveyed into the storm drain system. A portion of the captured stormwater evaporates or is taken up by plants, which helps reduce runoff volumes, peak runoff rates, and associated pollutant loads. The water quality treatment processes exhibited by vegetated roofs are runoff volume reduction and plant uptake (biological transformation).







Figure 8.27. Downspout Disconnection

- 2. **Downspout Disconnection** (#1) (Figure 8.27. This strategy involves treating runoff close to its source by intercepting rooftop runoff and infiltrating, filtering, treating, or reusing it before it moves from the roof into the storm drain system. Two kinds of practices are allowed. The first is for simple rooftop disconnection, whereas the second involves disconnection combined with supplementary runoff treatment, including the following:
 - Compost amended soils in the filter path
 - Installation of dry wells or french drains

- Installation of rain gardens or front yard bioretention
- Storage and reuse in a rain tank or cistern
- Storage and release in a foundation planter

The water quality treatment processes exhibited by downspout disconnection vary, depending upon the supplementary treatment practices used. Simple disconnection and rainwater harvesting (rain tanks or cisterns) rely on the processes of runoff volume reduction, settling (sedimentation), and filtering (filtration). The various forms of supplemental infiltration add the processes of adherence (sorption) to the soil and plant uptake (biological transformation) or removal by bacteria.

3. Rainwater Harvesting (#6) (Figure 8.28). Rain tanks intercept, divert, store, and release rainfall for future use. The term Rainwater Harvesting is used as the title of this specification, but it is also known as a cistern or rain tank system. Rainwater that falls on a rooftop is collected and conveyed into an above- or below-ground storage tank where it can be used for landscape irrigation, non-potable water, and on-site stormwater disposal. Typically, pre-fabricated rain tanks range from 200 to 10,000 gallons in size. The capture and re-use of rainwater can significantly reduce stormwater runoff volumes and pollutant loads (through the water quality treatment processes of runoff volume reduction and sedimentation). By providing a reliable and renewable source of water to end users, rain tanks can also have environmental and economic benefits beyond stormwater management (increased water conservation, water supply during drought, decreased demand on municipal or groundwater supply, etc). Rain tanks can be combined with other on-site practices, such as rain gardens, to enhance their runoff reduction and nutrient removal capability. The water quality treatment processes exhibited by rainwater harvesting practices are runoff volume reduction, settling (sedimentation), and filtering (filtration).







Figure 8.29. Filter Strip with Level Spreader (gravel pad as pre-treatment)

4. Soil Compost Amendments (#4). Soil restoration is an ESD practice applied after construction to restore soil porosity by adding compost and tilling it deep into the soil profile. These soil amendments can reduce the generation of runoff from compacted urban lawns and may also be used to enhance the runoff reduction performance of downspout disconnections, grass

channels, filter strips, and tree clusters. The water quality treatment process exhibited by soil compost amendments are those of infiltration practices: runoff volume reduction, settling (sedimentation), filtering (filtration), adherence (sorption) to the soil, and plant uptake (biological transformation) or removal by bacteria.

5. Sheet Flow to Vegetated Filters or Conserved Open Space (#2) (Figure 8.29). Filter strips are vegetated areas that treat sheet flow delivered from adjacent impervious areas by slowing runoff velocities and allowing sediment and attached pollutants to settle out. The two design variants are (1) sheet flow into a conserved natural area, and (2) sheet flow to a grass filter strip. The design, installation and management of these design variants are quite different. In some cases, filter strips can treat concentrated flows, but only if the concentrated flow is converted to sheet flow by an engineered level spreader. The water quality treatment processes employed by filter strips are runoff volume reduction, settling (sedimentation), filtering (filtration), adherence (sorption) to the soil, and plant uptake (biological transformation).

8.2.2.2. Swales or Open Channels

The following practices are explicitly designed to capture and treat the full Treatment Volume (T_v) within dry or wet cells formed by check dams or other means, or within the channel itself through a slow velocity and relatively long resistance time.

- 1. Grass Channel (#3) (Figure 8.30 below). Grass Channels can provide runoff filtering and treatment within the conveyance system and produce less runoff and pollutants than a traditional system of curb and gutter, storm drain inlets, and pipes. Grass channels provide a modest amount of runoff reduction and pollutant removal that varies depending on the underlying soil permeability. Grass Channels, however, are not capable of providing the same stormwater functions as Dry Swales, since they lack the engineered soil media and storage volumes. Their runoff reduction performance can be boosted when Soil Compost Amendments are added to the bottom of the swale. Grass channels are a preferable alternative to both curb and gutter and storm drains as a stormwater conveyance system where development density, topography and soils permit. The water quality treatment processes employed by grass channels are runoff volume reduction (minimal), settling (sedimentation), filtering (filtration), adherence (sorption) to the soil, and plant uptake (biological transformation).
- 2. Dry Swale (#10) (Figure 8.31 below). While Grass Channels and Dry Swales are both considered variations of the open channel concept, they are fundamentally different in terms of their designs. Dry swales are essentially volume-based shallow bioretention cells that are configured as a linear channel that temporarily stores and then filters the desired Treatment Volume. Grass channels are conveyance systems that can provide water quality treatment based on flow rate-based design criteria.





Figure 8.30. Grass Channel

Figure 8.31. Dry Swale

Dry Swales rely on the same pre-mixed soil media filter below the channel as is used for bioretention practices. If soils are extremely permeable, runoff infiltrates into underlying soils. In most cases, however, the runoff treated by the soil media flows into an underdrain, which conveys treated runoff back to the conveyance system further downstream. The underdrain system consists of a perforated pipe within a gravel layer on the bottom of the swale. Dry Swales may appear as simple grass channels with similar shape and turf cover, while others may have more elaborate landscaping. Dry Swales can be planted with turf grass, tall meadow grasses, decorative herbaceous cover, or trees. The water quality treatment processes employed by Dry Swales are runoff volume reduction, settling (sedimentation), filtering (filtration), sorption to the soil, and plant uptake (biological transformation).

8.2.2.3. Filtering Systems

The following practices capture and temporarily store the Treatment Volume (T_v) before passing it through a filter bed of sand, organic matter, soil, or other media.

1. Filtering Practices (#12) (Figure 8.32 below). Employing stormwater filters is a useful practice to treat stormwater runoff from small, highly impervious sites. Stormwater filters capture, temporarily store, and treat stormwater runoff by passing it through an engineered filter media, collecting it in an underdrain, and then returning it back to the storm drain system. The filter consists of two chambers: the first is devoted to settling, and the second serves as a filter bed consisting of sand or an organic filter media. Because they consume very little surface land area and have few site restrictions, stormwater filters are a versatile option that offers moderate pollutant removal performance at small sites where space is limited. The water quality treatment process employed by filtering practices are settling (sedimentation), filtering (filtration), adherence (sorption) to the soil, and plant uptake (biological transformation) or removal by bacteria.





Figure 8.32. Sand Filter

Figure 8.33. Bioretention Filter Cell

2. **Bioretention** (#9) (Figure 8.33). Individual bioretention areas serve highly impervious drainage areas less than five acres in size. Surface runoff is directed into a shallow landscaped depression that incorporates many of the pollutant removal mechanisms that operate in forested ecosystems. The primary component of a bioretention practice is the filter bed, which has a mixture of sand, soil, and organic material as the filtering media. The filter is composed of a sand/soil bed with a surface layer of mulch. During storms, runoff temporarily ponds 6-12 inches above the mulch layer and then rapidly filters through the bed.

Normally, the filtered runoff is collected in an underdrain and returned to the storm drain system. The underdrain consists of a perforated pipe in a gravel jacket installed along the bottom of the filter bed. Bioretention creates a good environment for runoff reduction, filtration, biological uptake, and microbial activity, and provides high pollutant removal. Bioretention can become an attractive landscaping feature with high amenity value and community acceptance. The water quality treatment processes employed by dry swales are runoff volume reduction, settling (sedimentation), filtering (filtration), adherence (sorption) to the soil, separation from solution (precipitation) onto the media, and plant uptake (biological transformation) or removal by bacteria.

8.2.2.4. Infiltration Practices

The following practices capture and temporarily store the T_v before allowing it to infiltrate into the B and/or C soil horizons. Runoff that discharges directly into limestone (karst) areas may be treated by certain kinds of infiltration practices (e.g., small-scale infiltration, permeable pavers and, perhaps, micro-bioretention/rain gardens).

1. Permeable Pavement (#7) (Figures 8.34 and 35). Permeable pavements are alternative paving surfaces that allow stormwater runoff to filter through voids in the pavement surface into an underlying stone reservoir where it is temporarily stored. Often, the filtered runoff is collected in an underdrain and returned to the storm drain system. If infiltration rates in native soils permit, permeable pavement practices can be designed without an underdrain for full

infiltration. A combination of these methods can be used to infiltrate a portion of the filtered runoff.





Figure 8.34. Permeable Asphalt Pavement

Figure 8.35. Permeable Interlocking Pavers

There are a variety of permeable pavement surfaces available in the commercial marketplace, including pervious concrete, porous asphalt, permeable interlocking concrete pavers, concrete grid pavers, and plastic grid pavers. While the specific design configuration may vary according to each product, nearly all permeable pavement types have the same general structure, consisting of a surface layer, aggregate base, and sub-base. The aggregate base layer serves to retain stormwater and also supports the design traffic loads. Permeable pavements are typically designed to treat rainfall on the pavement surface area, but can also be used to treat run-on from small adjacent impervious areas, such as impermeable driving lanes or rooftops.

Permeable pavements promote runoff reduction and provide high pollutant removal. Permeable pavement can also be used to reduce the impervious cover of a development site. The water quality treatment process employed by permeable paving materials is mainly runoff volume reduction. Pre-treatment must be provided to remove sediment, which would otherwise clog the pores in the paving material. A filter fabric is typically installed beneath the aggregate base, as well. So little or no treatment (filtering, etc.) is provided within the structure.

2. Infiltration Practices (#8) (Figure 8.36 below). Infiltration practices utilize temporary surface or underground storage to allow incoming stormwater runoff to exfiltrate into underlying soils. Runoff first passes through multiple pretreatment mechanisms to trap sediment and organic matter before it reaches the practice. As the stormwater penetrates the underlying soil, water quality treatment processes such as chemical adsorption (sorption, precipitation) and biological transformation processes remove pollutants. Infiltration practices are suitable for use in residential and other urban areas where measured soil permeability rates exceed 0.5 inch per hour. Infiltration is not recommended at sites designated as stormwater hotspots, to prevent possible groundwater contamination.

Infiltration has the highest runoff reduction capability of any stormwater practice, and probably comes closest to replicating predevelopment hydrology. On the other hand, infiltration practices have experienced consistent problems and failures over the years. These anecdotal

reports, along with groundwater concerns, have limited the use of infiltration practices. Toward this end, the Department, with assistance from the Chesapeake Stormwater Network and the Center for Watershed protection, has prepared a new infiltration practice design specification that should result in more widespread use of infiltration and better water quality protection and runoff management, while minimizing the risk of failure.





Figure 8.36. Infiltration Trench Construction

Figure 8.37. Bioinfiltration Cell

3. Bioinfiltration (#9) (Figure 8.37): Bioinfiltration (Level 2 Bioretention and Level 2 Dry Swale) can also be designed to infiltrate runoff into native soils. This can be done at sites with highly permeable soils, a low groundwater table, and a low risk of groundwater contamination. This type of design features the use of a "partial exfiltration" system that promotes greater groundwater recharge. Underdrains are only installed beneath a portion of the filter bed or are eliminated altogether, thereby increasing stormwater infiltration. Bioretention is also known as a "rain garden" when used on individual residential lots, often without an underdrain. The water quality treatment processes employed by Bioinfiltration are runoff volume reduction, settling (sedimentation), filtering (filtration), adherence (sorption) to the soil, separation from solution (precipitation) onto the soil, and plant uptake (biological transformation) or removal by bacteria.

8.2.2.5. Basins (Ponds and Wetlands)

Practices that have one or more permanent pools capable of treating the Treatment Volume (T_v) and may incorporate extended detention or significant shallow marsh areas. Basins are the final element in the roof-to-stream runoff reduction sequence. However, they should only be considered after all other upland runoff reduction techniques have been exhausted, and there is still a remaining water quality or channel protection volume to manage.

1. Constructed Wetlands (#13) (Figure 8.38). Constructed Wetlands are shallow depressions that receive stormwater inputs for treatment. Wetlands are typically less than one foot deep (although they have deeper pools at the forebay and micropool) and possess variable microtopography to promote dense and diverse wetland cover. Runoff from each new storm displaces runoff from previous storms, and the long residence time allows multiple pollutant removal processes to operate. The wetland environment provides an ideal environment for gravitational settling, biological uptake, and microbial activity. The water quality treatment processes exhibited by constructed wetlands are settling (sedimentation), flotation of light solids, adherence (sorption) to bottom soils, chemical separation from solution (precipitation) in the water, and biological transformation by bacteria and plant uptake.





Figure 8.38. Constructed Wetland

Figure 8.39. Small Wet Pond

- 2. Wet Ponds (#14) (Figure 8.39). Wet Ponds consist of a permanent pool of standing water that promotes a better environment for gravitational settling, biological uptake, and microbial activity. Runoff from each new storm enters the pond and partially displaces pool water from previous storms. The pool also acts as a barrier to re-suspension of sediments and other pollutants deposited during earlier storms. When sized properly, Wet Ponds have a residence time that ranges from many days to several weeks, which allows numerous pollutant removal mechanisms to operate. Wet Ponds can also provide extended detention (ED) above the permanent pool to help meet channel protection requirements. The water quality treatment processes exhibited by Wet Ponds are settling (sedimentation), flotation of light solids, adherence (sorption) to bottom soils, chemical separation from solution (precipitation) in the water, and biological transformation free floating algae.
- 3. Extended Detention (#15) (Figure 8.40 below). Extended Detention (ED) ponds rely on gravitational settling as their primary pollutant removal mechanism. Consequently, they generally provide fair to good removal of particulate pollutants but low or negligible removal for soluble pollutants, such as nitrate and soluble phosphorus. Extended Detention is different from stormwater detention, which is used for peak discharge or flood control purposes and often detains flows for just a few minutes or hours. This option relies on 12 to 24 hour detention of stormwater runoff after each rain event. An under-sized outlet structure restricts stormwater flow so it backs up and is stored within a pond or wetland. The temporary ponding enables particulate pollutants to settle and reduces stress on downstream banks. The use of ED alone generally has the lowest overall pollutant removal rate of any stormwater treatment option. As

a result, ED is normally combined with wet ponds or constructed wetlands to maximize pollutant removal rates. The water quality treatment process exhibited by extended detention basins is mainly settling (sedimentation).



Figure 8.40. Dry Extended Detention Basin

8.2.2.6. Manufactured Treatment Devices (MTDs) (Figures 8.41 and 8.42)

Virginia allows the use of certain Manufactured Treatment Devices (MTDs) for which pollution removal performance has been verified and certified through by the Virginia Stormwater BMP Clearinghouse Committee and the DEQ. There is a wide variety of products within this category, which provides different kinds of stormwater management options, ranging from underground detention storage to flow control to filtering technologies.

8.2.2.7. Treatment Trains

BMPs suitable to meet channel protection and overbank flood criteria should not be used by themselves to also address water quality requirements but should, instead, be combined in a "treatment train" with one or more other BMPs to meet water quality requirements. Pre-treatment BMPs are designed to improve water quality and enhance the effective design life of practices by consolidating sedimentation location, but they also cannot meet the water quality requirements by themselves. Pre-treatment practices must be combined with other water quality BMPs to meet the water quality criteria. It is important that the various BMPs employed in a treatment train should use *different* treatment mechanisms in order to maximize pollution removal (e.g., rooftop disconnection to a grass channel to biofilters and bioretention to a constructed wetland, as depicted in **Figure 8.41** below).

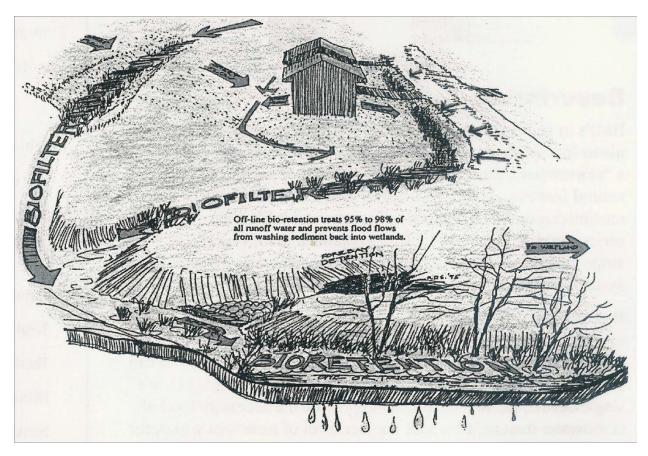


Figure 8.41. Treatment Train
Source: Robert Sykes, Dept. of Landscape Architecture, University of Minnesota

8.3. POST-CONSTRUCTION BMP DESIGN & CONSTRUCTION STANDARDS AND SPECIFICATIONS

Complete standards and specifications for Virginia-approved post-construction BMPs and MTDs can be found on the Virginia BMP Clearinghouse web site, at http://www.vwrrc.vt.edu/swc/. For each public domain BMP, criteria are provided to address the following topics:

Description: Describes the practice and explains its purpose and how it functions.

Performance: Identifies how well the practice addresses various objectives of stormwater management.

- Runoff Reduction (which includes Groundwater Recharge)
- Total Phosphorus Removal
- Total Nitrogen Removal
- Total Suspended Solids (TSS) Removal
- Channel Protection
- Flood Mitigation

Design Table: Identifies the sizing criteria for the practice needed to accommodate the full T_v and geotechnical or other testing that must be done to provide information needed to correctly design the facility.

Typical Graphical Details: Provides visual guidance regarding how to correctly design and build the particular practice.

Physical Feasibility and Design Applications: Identifies site considerations and physical constraints that determine where a practice may be applied or that may restrict the use of a practice.

Design Criteria: Identifies the specific standards and specifications that govern the correct design of specific devices, including dimensions, components, orientation, etc. The design criteria include but is not limited to information about the following:

- *Pretreatment:* Identifies the type of measures used to trap coarse elements before they enter the facility, thus reducing the maintenance burden and ensuring a long-lived practice.
- *Conveyance:* Identifies how to convey runoff to the practice in a manner that is safe, minimizes erosion and disruption to natural channels, and promotes filtering and infiltration.
- *Geometry:* Identifies any practice-specific configurations, such as optimum length-to-width-to-depth ratios, minimum flow lengths, etc.
- *Material Specifications:* Identifies the specific kinds of materials (e.g., stone sizes, landscaping materials, etc.) needed to correctly construct the particular practice.
- *Environmental/Landscaping:* Identifies how to reduce secondary environmental impacts of facilities through features that minimize disturbance of natural stream systems and comply with environmental regulations. Provides landscaping that enhances the pollutant removal and aesthetic value of the practice.
- Maintenance Considerations for the Design: Identifies the design elements that ease the maintenance burden.

Regional and Climate Design Adaptations: Identifies considerations and adaptations needed to address particular kinds of regional characteristics or climate variations, including the following:

- Hot spots
- Ultra-Urban Development Sites
- Infill and Redevelopment Sites
- Single-Family Lots
- Karst terrain
- Coastal plain
- Steep terrain
- Sensitive Waters
 - Lakes and Water Supply Reservoirs
 - o Trout and Other High-Quality Streams
 - o Groundwater Drinking Water Source Areas
 - Wetlands
 - Impaired Waters
- Cold climates/winter performance

• Linear/highway sites

Construction Sequence and Inspection: Identifies factors important to the proper construction and long-term viability of the particular practice.

Maintenance: How to maintain the long-term performance of the practice through regular maintenance activities.

Community and Environmental Considerations: Addresses issues such as physical safety, potential for vectors, aesthetics, etc.

References: A list of resources from which the criteria and information in the design specification were taken.

Overviews of the public domain post-construction BMPs that DEQ has approved for use in Virginia can be found in Section 8.4.2 (above) of this chapter.

8.4 BMP SELECTION CATEGORY DESCRIPTIONS AND TABLES

8.4.1 Land Use (Table 8.3 below)

Which practices are best suited for the proposed land use at this site? In this step, the designer makes an initial screening to select practices that are best suited to a particular land use.

Rural. This column identifies BMPs that are best suited to treat runoff in rural or very low density areas (e.g., typically at a density of less than ½ dwelling unit per acre) with few neighborhoods and relatively large amounts of open space. Stormwater control measures with larger area demands may be easier to locate with appropriate buffers in rural areas. Additionally, typical stormwater pollutants from rural areas include sediments and nutrients, which can be effectively managed by most stormwater control measures. As a result, most BMPs are suitable for rural areas.

Residential. This column identifies the best treatment options in medium to high density residential developments, which typically have limited space and higher property values compared to rural undeveloped land. Also, stormwater control measures in residential areas are likely to be located in close proximity to residences. Public safety and nuisance insects are common concerns related to control measures in residential areas. BMPs with large land requirements or open pools of water may be less desirable in these areas. In some situations, stormwater ponds or other open water practices may be incorporated into the landscape as amenities to provide for habitat, recreation, and aesthetic value.

Roads and Highways. This column identifies the best practices to treat runoff from major roadway and highway systems, which typically generate high stormwater pollutant loads due to vehicle traffic and winter deicing activities. Sediments, metals, chlorides, and hydrocarbons are the primary pollutants associated with roads and highways. Nitrogen from vehicle exhausts and bacteria are also commonly present in road and highway runoff. As a result, most treatment practices provide some treatment benefit but do not adequately address all of the water quality

impacts associated with this land use. In addition, open water and deep pools can also be a safety issue near roads and highways.

Commercial/Industrial Development. This column identifies practices that are suitable for commercial and industrial development, which often have more intensive traffic, increased risk of spills, and exposure of materials to precipitation. Pollutants associated with these land uses can vary significantly, depending on the nature of activities at each site, although traffic-related pollutants such as sediments, metals, and hydrocarbons are commonly present in runoff from most commercial and industrial sites. These developments may also have more available space for locating stormwater control measures.

Hotspot Land Uses. This column examines the capability of BMPs to treat runoff from designated hotspots. BMPs that receive hotspot runoff may have design restrictions, as noted.

Ultra-Urban Sites. This column identifies BMPs that work well in the ultra-urban environment, where population is dense, land area and space are limited, stormwater infrastructure is already in place, a wide range of potential pollutants is present, and original soils have been disturbed. Ultra-urban sites are the most restrictive in terms of BMP selection. Stormwater control measures appropriate for ultra-urban sites are also frequently used at redevelopment and infill sites and to retrofit existing urban development.

Table 8.3. BMP Selection Matrix 1 - Land Use

BMP Group	Specific BMP	Rural	Residential	Roads and Highways	Commercial/ Industrial	Hotspots	Ultra- Urban ¹
	Rooftop Disconnection 1	0	0	•	0	0	•
Runoff	Sheet flow to Veg. Filter/Open Space	0	0	0	0	$ ightharpoonup^2$	•
Volume Reduction	Soil Compost Amendments	0	0	0	0	▶2	0
	Vegetated Roof	•	•	•	0	0	0
	Rainwater Harvesting	0	0	•	0	O ³	0
Swales &	Grass Channel	0	•	0	•	▶4	
Open Channels	Dry Swale	0	•	0	Þ	▶4	•
Filtering	Bioretention 1	•	•	0	0	O ⁴	O ¹
Systems	Filtering Practice	•	•	0	0	O ⁵	0
	Permeable Pavement	•	•	•	•	•	0
	Infiltration	•	•	0	0	•)
Infiltration Practices	Urban Bioretention	•	•	0	0	O ² (Needs underdrain)	0
	Bioretention 2	•	•	0	0	O ² (Needs underdrain)	0
	Wet Swale	0	0	0	•		•
Basins	Constructed Wetland	0	0	0	•) ²	•
Basins	Wet Pond	0	0	0	•	▶5	•
	Extended Detention	0	0	0)	▶5	•
Mfr	Hydrodymanic Devices	•	0	0	0	•	0
Treatment	Filtration Devices	•	0	0	0	•	0
Devices	Storage Devices	•	•	•	0	▶2,4	0

O Appropriate. Good option in most cases.

Depends. Suitable under certain conditions, or may be used to treat a portion of the site.
 Least appropriate. Seldom or never suitable.

Secondary treatment practices and stormwater treatment trains are typically more appropriate for Ultra-Urban land uses

Not allowed unless pretreatment provided to remove hydrocarbons, trace metals, and toxicants

Unless the roof is considered a hotspot

Acceptable option, if not designed as an exfilter. (An exfilter is a conventional stormwater filter without an underdrain system. The filtered volume ultimately infiltrates into the underlying soils.)

Acceptable option, but may require an impermeable liner to reduce risk of groundwater contamination.

8.4.2 Physical Feasibility (Table 8.4 below)

Are there any physical constraints at the project site that may restrict or preclude the use of a particular BMP? In this step, the designer screens the various BMP design criteria to determine if the soils, water table, drainage area, slope or head conditions present at a particular development site might limit the use of a BMP. More detailed testing protocols are often needed to confirm physical conditions at the site. The following are the primary factors.

Soil Infiltration Rate. The key evaluation factors are based on an initial investigation of the NRCS Hydrologic Soil Groups at the site. Note that more detailed geotechnical tests are usually required for infiltration feasibility and during design to confirm permeability and other factors. Knowledge of all soil groups present on the site is needed for runoff calculations, but the presence of HSG-A or HSG-D soils are most likely to constrain the choice of certain BMPs.

Water Table Separation. This column indicates the minimum depth to the seasonally high water table from the bottom elevation, or floor, of a BMP. A relatively shallow depth to water table may limit the choice of certain BMPs.

Shallow Soils/Depth to Bedrock. Likewise, this column indicates the minimum depth to bedrock from the bottom elevation, or floor, of a BMP. A relatively shallow depth to bedrock may also limit the choice of certain BMPs.

Contributing Drainage Area. This column indicates the minimum or maximum drainage area that is considered optimal for a practice. If the drainage area present at a site is slightly greater than the maximum allowable drainage area for a practice, some leeway is warranted where a practice meets other management objectives. Likewise, the minimum drainage areas indicated for ponds and wetlands should not be considered inflexible limits, and may be increased or decreased depending on water availability (base flow or groundwater), mechanisms employed to prevent clogging, or the ability to assume an increased maintenance burden.

Slope. This column evaluates the effect of slope on the practice. Specifically, the slope guidance refers to how flat the area where the practice is installed must be and/or how steep the contributing drainage area or flow length can be.

Hydraulic Head. This column provides an estimate of the elevation difference needed for a practice (from the inflow to the outflow) to allow for gravity operation.

Karst Geology. This column provides information regarding the appropriateness of the various BMPs for installation in karst environments and conditions that apply to those BMPs in such areas. Karst is a dynamic landscape formed over the millenia by the dissolution of bedrock such as limestone, dolomite, and marble. Karst is characterized by landscape features such sinkholes, springs, caves, a highly irregular soil-rock interface, and typically a poorly defined surface drainage network. Karst terrain is considered to be any landscape underlain by carbonate bedrock in the shallow subsurface or any area expressing characteristic karst features. Karst poses many challenges to BMP selection and design. Many sinkholes form due to the collapse of the surface sediments caused by the intrusion of stormwater from the surface. Some BMPs inadvertently

promote sinkhole formation that may threaten the integrity of the practice as well as structures on the site. In addition, Karst geology provides rapid pathways for water to travel from the surface to deep groundwater and aquifers, so it should be assumed that any treated or untreated runoff that is infiltrated will reach the drinking water supply in karst areas.

Table 8.4. BMP Selection Matrix 2 - Physical Feasibility

BMP Group	Specific BMP	Soils ¹	Water Table Separation	Depth to Bedrock/ Shallow Soils	Contrib. Drainage Area (Ac.)	Max. Site Slope ²	Hydraulic Head (Ft.)	Karst Geology or a Sinkhole	Cold Climate (cf Table 8.5)
	Rooftop Disconnect.	Join with additional runoff reduction practice on C-D soils	2 feet	2 feet	Maximum 1,000 sq. ft. to each roof discharge point	1-2%	1 foot	Preferred	Frozen ground may hinder disposal of water
	Sheet flow to Vegetated Filter or Conserved Open Space	Any soil except fill; best to use w/ compost amend's on C-D soils	2 feet	2 feet	3 max.	6% for consrv filter; 8% for grass filter strip	1 to 2 feet	Preferred	No concerns or needed adapta- tions
Runoff Volume Reduction	Soil Compost Amendments	HSG B-D soils	1.5 feet	1.5 feet	Contrib. Imperv. area should not exceed area of amended soil	10%	1 foot	ОК	OK, except for areas used for snow storage
	Vegetated Roof	NA	NA	NA	NA	NA	1 to 2 feet	Preferred	Plan for snow loading and hardy veg. cover
	Rainwater Harvesting	NA	Below- grade tanks must be above water table	Below- grade tanks must be above bedrock	Rooftop (only) area draining to the tank	NA	Varies with purpose and design	Preferred	Locate indoors or underground; others should be operated seasonally
Swales & Open Channels	Grass Channel	Must achieve additional res. time (min. 10 minutes) if C-D soils	2 feet	2 feet	5 max.	2-4%	2 to 3 feet	OK ³	ок
Onamicis	Dry Swale	Made Soil; must use underdrain if on C-D soils	2 feet	2 feet	5 max.	4%	3 to 5 feet	Prefer'd ³	Medium benefit & limitation

BMP Group	Specific BMP	Soils ¹	Water Table Separation	Depth to Bedrock/ Shallow Soils	Contrib. Drainage Area (Ac.)	Max. Site Slope ²	Hydraulic Head (Ft.)	Karst Geology or a Sinkhole	Cold Climate (cf Table 8.5)
Filtering Systems	Filtering Practice	NA	2 feet	2 feet	5 max. ⁴ ; 0.5 to 2 preferred	NA	2 to 10 feet	Prefer'd, but must use imper- meable liner	OK if place below frost line and use pretreatment; Chlorides will move through untreated
	Bioretention 1 (with underdrain)	Made Soil	2 feet	2 feet	5 max. ⁴ ; 0.5 to 2 preferred	1-5%	4 to 5 feet	OK, but must use under- drain and imper- meable liner	OK; use salt-tolerant veg. and pretreatment; Chlorides will move through untreated
	Permeable Pavement 1	Must use underdrain on C-D soils			Ratio of contrib. pavement area to Permeable	1-3%	2 to 4 feet	Large- scale or Level 2 Prohibit- ed; Small-	Limited; Use special design features; Active
	Permeable Pavement 2	Minimum measured f _c > 0.5 inch/hour	2 feet	2 feet	Pavement area may not exceed 2:1			scale OK; must have liner and under-	mgmt needed to prevent infiltra-
	Infiltration	Minimum measured f _c > 0.5 inch/hour			< 2, and close to 100% impervious	0-5%	2 to 4 feet	drain; extensive pre- treatment required	tion of chlorides and soluble toxics
Infiltration Practices	Urban Bioretention	NA	2 feet	2 feet	5 max. ⁴ ; 0.5 to 2 preferred	1-5%	4 to 5 feet	Preferred	OK; use salt-tolerant veg. and pretreatment; Chlorides will move through untreated
	Bioretention 2 (Bioinfiltration, with no underdrain)	Made Soil; use underdrain if C or D ³ base soils	3 feet	2 feet	5 max. ⁴ ; 0.5 to 2 preferred	1-5%	4 to 5 feet	Not Recmd, esp. large scale; extensive pre- treatment required	OK; use salt-tolerant veg. and pretreatment; Chlorides will move through untreated

BMP Group	Specific BMP	Soils ¹	Water Table Separation	Depth to Bedrock/ Shallow Soils	Contrib. Drainage Area (Ac.)	Max. Site Slope ²	Hydraulic Head (Ft.)	Karst Geology or a Sinkhole	Cold Climate (cf Table 8.5)
	Wet Swale	Best on HSG C or D soils	Below water table	2 feet below bottom of swale	5 max	2% thru swale	2 feet	Not Recmd	Medium benefit & limitation
	Constructed Wetland	HSG-A or B soils may require liner	Below water table if no hotspot or aquifer present; otherwise, a 2 foot separation	2 feet below bottom of wetland	25 min. ⁶	NA	2 to 4 feet	OK; use impermeable liner; limit depth; geotech. tests needed; max. ponding depth	OK; use salt- tolerant vegeta- tion
Basins	Wet Pond	HSG-A or B soils may require liner	Below water table if no hotspot or aquifer present; otherwise, a 2 foot separation	2 feet below bottom of wetland	25 min. ⁵	NA	6 to 8 feet	Not Recmd ⁶	OK; limit depth to avoid stratifica- tion; adapt outlet structure
	Extended Detention 1	HSG-A or B	0 ()	0 ()	< 10	N/A	0.15.40.65.51	Not	014
	Extended Detention 2	soils may require liner	2 feet	2 feet	> 10	NA	6 to 10 feet	Recmd ⁶	OK
	Hydrodymanic Devices	NA			?	NA	?	OK	?
	Filtration Devices	NA	Varies with	Varies with	?	NA	?	ОК	?
Mfr Treatment Devices	Storage Devices	NA	device; Must have clearance below bottom of device	device; Must have clearance below bottom of device	?	NA	?	Must have liner and under- drain; Signifi- cant pre- treatment required	?

KEY: OK = not restricted; WT = water table; PT = pretreatment; f_c = soil permeability

Cold Climate/Winter Conditions. This column presents guidance on how to choose BMPs for areas of Virginia where much colder temperatures, greater snowfall, and more ice prevail. While there may be fewer runoff events during winter months, snow and ice may significantly impact the operation of some BMPs during winter rain events and periods of snowmelt. Some of these

¹ USDA-NRCS Hydrologic Soil Groups (HSGs)

² Refers to post-construction slope across the location of the practice

³ Denotes a required limit, other elements are planning level guidance and may vary somewhat, depending on site conditions

⁴ Drainage area can be larger in some instances.

^{5 10} acres may be feasible if ground water is intercepted and/or if water balance calculations indicate a wet pool can be sustained, and an anti-clogging device must be installed

⁶ If detention is used, then an impermeable liner must be placed at the bottom of the basin and geotechnical tests should be conducted to determine the maximum allowable depth

potential impacts are (1) pipe freezing, (2) ice formation on permanent pools, (3) reduced biological activity, and (4) reduced soil infiltration. Frozen conditions typically inhibit performance throughout the winter and generate a significant volume of melt water and associated pollutant loads. In particular, melt water from roadways typically has high chloride and sediment content from salt and sand treatments. **Table 8.5** summarizes winter operation and cold weather considerations for various stormwater treatment practices.

Table 8.5. BMP Selection Matrix 3 – Winter and Cold Weather Stormwater Control Operational Criteria

Category	Practice	Pipe Freezing	Ice Formation	Reduced Biological Activity	Reduced Soil Infiltration
	Wet Ponds	•	•		0
Ponds	Extended Detention Ponds	•	•		0
	Vegetated Roofs	•	•	0	0
Wetlands	Constructed Wetlands	•	•	•	0
vvetiands	Wet Swales	0	•	(0
	Level 1 Infiltration	1	•	0	•
	Level 2 Infiltration	0	•	0	•
Infiltration	Level 2 Bioretention	0	•	0	•
	Level 2 Dry Swale	0	•	(•
	Permeable Pavement	1	•	0	•
	Surface Filtering Practices	1	•	0	•
	Underground Filtering Practices	0	0	0	0
Filters	Level 1 Bioretention	1	•	0	•
	Level 1 Dry Swale	1	•	0	•
	Sheet flow to Vegetated Filter or Conserved Open Space	0	•	0	•

Key: ● = Significant

8.4.3 Critical Water Resources (Table 8.6 below)

What watershed protection goals need to be met in the water resources the site drains to? The design and implementation of BMPs is strongly influenced by the nature and sensitivity of the receiving waters. In some cases higher pollutant removal, more recharge or other environmental performance is warranted to fully protect the resource quality and human health and/or safety. Critical resource areas include: groundwater and source water areas, high value trout streams, other freshwater streams, freshwater lakes and ponds, drinking water reservoirs, freshwater wetlands, and coastal waters (including tidal wetlands), as described below. **Table 8.6** below outlines the key design variables and considerations that must be addressed for sites that drain to any of the above critical resource areas.

^{■ =} Moderately Significant

O = Least Significant

Table 8.6. BMP Selection Matrix 4 – Critical Water/Watershed Resources

BMP Group	Specific BMP	Groundwater, Source Water Areas and Septic Systems	100-Year Flood Plains	Trout and Other Freshwater Streams	Freshwater Lakes and Ponds	Freshwater Wetlands (May be regulated)	Coastal Waters (incl. Tidal Wetlands	Impaired Waters
Genera	General Location		Restrict grading & fill; no raising 100-year water surface elevation	Outside the stream buffer, where required or otherwise established	Outside of shoreline buffer, where required or otherwise established	Outside of wetland buffer, where required or otherwise established	Outside of wetland buffer, where required or otherwise established	Selection based on Pollutant Removal for Target Pollutant
	Rooftop Disconnect.	ОК	OK	Preferred; best if used with suppl. practices	ОК	ОК	Preferred	OK; best if used with suppl. practices
Runoff Volume Reduction	Sheet flow to Vegetated Filter or Conserved Open Space	ОК	OK	Preferred	ОК	Does NOT apply to jurisdic- tional wetlands	Preferred	ОК
	Soil Compost Amendments	OK	ОК	Preferred	OK	OK	OK	OK
	Vegetated Roof	NA	NA	OK	NA	NA	OK	NA
	Rainwater Harvesting	OK ¹	ОК	Preferred	OK	OK	Preferred	ОК
Swales & Open Channels	Grass Channels Dry Swales	Pre-treat hotspots prior to discharge to channel or swale	ОК	Preferred; link w/ other BMPs to protect channel and prevent	OK; dry swale provides the best TP removal	OK, dry swale provides the best TP removal	Restricted (poor bacteria removal)	ОК
Filtering Systems	Filtering Practices	OK – a Preferred practice		flooding Preferred, but link w/ other BMPs to protect channel and prevent flooding	OK get moderate to high TP removal	OK, moderate to high TP removal	OK, moderate to high bacteria and TN removal	Preferred practices
	Bioretention 1	OK, with cautions for PSHs		Preferred practice	Preferred practice	Preferred practice	Preferred; mod to high bacteria and TN removal	
	Permeable Pavement	100 foot SD		Preferred if			Preferred	
Letter of	Infiltration	from water supply wells; pre-treat runoff in	Use only practices with imper-	site has appropriate soils	Preferred, if site has appropriate	Preferred, if	Lg. scale OK; small scale restricted	Restricted
Infiltration Practices	Urban Bioretention	limestone regions; Restricted, if site is a PSH;	meable liners and	Extremely limited feasibility	soils, in which case these are	site has appropriate soils	ОК	for some target pollutants
	Bioretention 2	may need injection well permit	under- drains	Preferred if site has appropriate soils	preferred practices		Preferred; mod to high bacteria and TN removal	

BMP Group	Specific BMP	Groundwater, Source Water Areas and Septic Systems	100-Year Flood Plains	Trout and Other Freshwater Streams	Freshwater Lakes and Ponds	Freshwater Wetlands (May be regulated)	Coastal Waters (incl. Tidal Wetlands	Impaired Waters
	Wet Swales	Preferred practice	ОК	OK, but use only shaded swales near trout streams	ОК	Preferred practice	Preferred	Preferred practice
	Constructed Wetlands	Preferred practice	ОК	OK, but use only wooded wetlands near trout streams	Some designs restricted due to seasonally variable P removal, combined with other treatments	Preferred practice, but no use of existing natural wetlands	Preferred	Preferred practice
Basins Basins	Wet Ponds	Pre-treat hotspots; provide a 2 foot SD from seasonal high groundwater elevation	May not locate ponds in the flood plain	Restricted due to pool and stream warming concerns; overland erosion and channel protection is necessary	Design for enhance TP removal; use ponds with wetlands for best TP removal	Design for enhance TP removal; use ponds with constr. (NOT natural) wetlands for best TP removal	OK; Moderate bacteria removal; good to moderate TN removal; max. normal pool depth of 4 feet; Provide long ED (> 48 hrs) for max. bacteria die-off	Preferred practice
	Extended Detention	Does not meet Treatment Volume pre- treatment requirements	May not locate ponds in the flood plain	Not recm'd near trout streams unless need to provide for channel protection and flood protection; then use special design; Not recm'd within stream	Generally not necessary if discharge is directly to a large lake	Not recm'd within natural wetlands, nor should they inundate or otherwise change the wetland's hydroperiod	Restricted (limited feasibility)	May be restricted if warming is part of impairment
Mfr	Hydrodymanic Devices		May not	?		?		?
Treatment Devices	Filtration Devices	ОК	locate in the flood	?	OK	?	OK	?
NOTES: SE	Storage Devices	istanas: ED - 4	plain	?		?		?

NOTES: SD = separation distance; ED = extended detention PSH = potential stormwater hotspot

¹ This is a matter of the scale of the use of rainwater harvesting; if sufficient water is diverted for recycling, a nearby aquifer may be deprived of recharge water.

8.4.4 Stormwater Management Capability (Table 8.7 below)

Can one BMP meet all design criteria, or is a combination of practices needed? In this step, designers can screen the BMP list to determine if a particular BMP can meet each of the SWM criteria: water quality, groundwater recharge, receiving channel/overland flow protection, and flood control storage requirements. At the end of this step, the designer can screen the BMP options down to a manageable number and determine if a single BMP or a group of BMPs (e.g., a treatment train) are needed to meet stormwater sizing criteria at the site.

Water Quality Treatment. This column indicates whether each practice can be used to provide for effective water quality treatment (i.e., pollutant removal). For more detail on specific pollutant removal, consult **Table 8.8** below.

Runoff Volume Reduction. This column indicates whether each practice can provide for a reduction of runoff volume from the site, which contributes to pollutant removal and may contribute to groundwater recharge, depending on the specific practice. Obviously, the more runoff can be reduced in ways that keep it on the development site, the less runoff will be discharged from the site.

Groundwater Recharge. This column indicates whether each practice can provide for groundwater recharge. It may also be possible to accomplish some groundwater recharge by using Environmental Site Design techniques (see **Chapter 6**).

Receiving Channel/Overland Flow Protection. This column indicates whether the BMP can typically provide for the channel protection storage volume. The finding that a particular BMP cannot meet the channel protection requirement does not necessarily imply that the BMP should be eliminated from consideration, but is a reminder that more than one practice may be needed at a site (e.g., a bioretention area and a downstream extended detention pond).

Flood Control. This column indicates whether a BMP can typically meet the overbank and extreme flood control criteria for the site. Again, the finding that a particular BMP cannot meet the channel protection requirement does not necessarily imply that the BMP should be eliminated from consideration, but is a reminder that more than one practice may be needed at a site (e.g., a bioretention area and a downstream extended detention pond).

8.4.5 Pollutant Removal

How do each of the BMP options compare in terms of pollutant removal? In this step, the designer views removal of select pollutants to determine the best BMP options for water quality. It is important to note that the Total Pollutant Reductions (TR) indicated in **Table 8.8** below for TP, TN, and TSS reflect a combination of pollutant removal processes. These numbers assume a typical concentration for each pollutant in the total site runoff. These concentrations are typically expressed as an amount per unit of volume (e.g., 0.26 mg/L of TP). When part of the total runoff volume is removed through the use of Runoff Reduction practices (e.g., rainwater capture, infiltration, etc.), the pollutants in that removed volume are removed from the remaining runoff that must still be managed. Then, as Stormwater Treatment processes (e.g., settling, filtration,

chemical conversion, vegetation uptake, etc.) are applied to that remaining runoff, the actual concentration of pollutant in the runoff is further reduced. So the total mass load removal of pollutants is a result of the combination of runoff volume reduction and supplementary treatment practices. **Table 8.8** examines the capability of each BMP option to remove specific pollutants from stormwater runoff.

Table 8.7. BMP Selection Matrix 5 – Stormwater Management Capability

BMP Group	Specific BMP	Water Qual. Treatment	Runoff Volume Reduction	Groundwater Recharge	Channel/ Overland Flow Protection	Flood Control
	Vegetated Roof	•	0	•	4	•
	Rooftop Disconnection	•	0	•	4	•
Runoff	Rainwater Harvesting	•	0	•	● 4	•
Volume Reduction	Soil Compost Amendments	•	0	•	4	•
	Sheet flow to Vegetated Filter or Conserved Open Space	•	•	•	•	•
Swales &	Grass Channel	0	0	0	•	•
Open Channels	Dry Swale	0	0	O ¹	4	•
Filtering	Filtering Practice	0	•	•	•	•
Systems	Bioretention 1	0	0	O ¹	4	•
	Permeable Pavement 1	0	0	•	4	O ²
Infiltration Practices	Permeable Pavement 2	0	0	0	■ 4	O ²
	Infiltration	0	0	0	4	O ²
	Bioretention 2	0	0	0	0	O ²
	Constructed Wetland	0	0	O ³	0	0
	Wet Swale 1	0	•	•	•	•
	Wet Swale 2	0	•	•	•	•
Basins	Wet Pond	0	0	0	0	0
	Extended Detention 1	•	•	•	0	0
	Extended Detention 2	•	•	•	0	0
Mfr	Hydrodynamic Devices	Varies	•	•	•	•
Treatment	Filtration Devices	Varies	Varies	•	•	•
Devices	Storage Devices	•	0	Varies	Varies	Varies

- O Practice generally meets this stormwater management goal.
- Practice may partially meet this goal, or under specific site and design conditions
- Practice can almost never be used to meet this goal.
- ¹ Provides recharge only if designed as an exfilter system.
- ² Can be used to meet flood control in rare conditions, with very cobbly or highly permeable soils.
- ³ Yes, unless impermeable liners are required or the pool intercepts groundwater
- ⁴ By removing/infiltrating water, thus reducing the overall volume of runoff

Table 8.8. BMP Pollutant Removal Efficiencies

Practice	Runoff Volume Reduc. ¹ (%RR)	TP EMC Reduc. ² (%PR)	Total TP Reduc. ³ (%TR)	TN EMC Reduc. ² (%PR)	Total TN Reduc. ³ (%TR)	TSS EMC Reduc. ² (%PR)	Total TSS Reduc. ³ (%TR)	Total Bacteria Reduc. ^{3, 4} (%TR)	Total Metals Reduc. ³ (%TR)	Total Hydro- carbons Reduc. ³ (%TR)
Rooftop Disconnect. 12, 14	25 or 50 ¹⁰	0	25 or 50 ¹⁰	0	25	50	50	NA		
Sheet flow to Veg. Filter 1	25 or 50 ¹⁰	0	25 or 50 ¹⁰	0	25 or 50 ¹⁰	50 or 75 ¹⁰	50 or 75 ¹⁰	20*		
Sheet flow to Veg. Filter and Consrv. Open Space 2 12	50 or 75 ¹⁰	0	50 or 75 ¹⁰	0	50 or 75 ¹⁰	60 or 85 ¹⁰	60 or 85 ¹⁰	20*		
Grass Channel	10 or 20 ¹⁰	15	23	20	28	30	35	0	70 ⁷	62
Soil Compost Amendments	site. See de to Veg. Filt			isconnect., S	Sheet Flow	0	50	NA		
Vegetated Roof 1	45	0	45	0	45	50	70	NA		
Vegetated Roof 2 Rainwater Harvesting	90 ^{11, 12}	0	90 ^{11, 12}	0	90 ^{11, 12}	50 0	80 90 ¹¹	NA NA		
Permeable Pavement 1	45	25	59	25	59	65	80	NA	99 ⁹	
Permeable Pavement 2	75	25	81	25	81	65	90	NA	99 ⁹	
Infiltration 1	50	25	63	15	57	50	75	40*	99 ⁹	NA
Infiltration 2	90	25	93	15	92	50	95	40*	99 ⁹	NA
Bioretention 1	40	25	55	40	64	50	70	40 *		62+
Bioretention 2	80	50	90	60	90	75	95	40*		62+
Urban Bioretention	40	25	55	40	64	50	70	40*		62+
Dry Swale 1	40	20	52	25	55	40	65	0 ⁵	70 ⁷	
Dry Swale 2	60	40	76	35	74	70	90	25*	70 ⁷	
Wet Swale 1 Wet Swale 2	0	20 40	20 40	25 35	25 35	40 70	40 70	0		
Filtering Practice 1	0	60	60	30	30	60	60	35 ⁵	69 ⁷	84
Filtering Practice 2	0	65	65	45	45	85	85	70 ⁶	69 ⁷	84
Constructed Wetland 1	0	50	50	25	25	50	50	80 ⁷	42 ⁷	85
Constructed Wetland 2	0	75	75	55	55	80	80	80	42 ⁷	85
Wet Pond 1	0	50 (45 ¹³)	50 (45 ¹³)	30 (20 ¹³)	30 (20 ¹³)	50	50	70 ⁷	62 ⁷	81
Wet Pond 2	0	75 (65 ¹³)	75 (65 ¹³)	40 (30 ¹³)	40 (30 ¹³)	80	80	70	62 ⁷	81
Ext. Detention Pond 1	0	15	15	10	10	50	50	30 ⁵		
Ext. Detention Pond 2	15	15	31	10	24	70	75	60 ⁶		

Based upon 1 inch of rainfall - 90% storm ,Annual average runoff reduction as reported in CWP (2008b)

Change in stormwater event mean concentration (EMC) as it flows through the practice and is subjected to treatment processes, as reported in CWP (2008b)

³ Total removal (TR) = product of RR and PR

Bacteria removal rates, as reported by Schueler et al (2007). An asterisk denotes where monitoring data is limited and estimates should be considered extremely provisional. NA indicates the practice is not designed for bacterial removal or is located far up in the treatment pathway, such that bacteria source areas are largely absent (e.g. green roofs and cisterns).

Median value from International BMP database.

- ⁶ Q3 value from International BMP database.
- Median value from the National Pollutant Removal Performance Database (NPRPD, managed by the Center for Watershed Protection)
- Average of zinc and copper, but only zinc for infiltration.
- 9 Based on fewer than five data points (i.e., independent monitoring studies).
- 10 The lower rate is for Hydrologic Soil Group (HSG) class C and D soils; the higher rate is for HSG class A and B soils
- 11 Credit up to 90% is possible if all water from storms 1 inch or less is used through demand, and the tank is sized such that no overflow occurs. Total credit is not to exceed 90% as an isolated practice.
- 12 See BMP design specification for an explanation of how additional pollutant removal can be achieved.
- ¹³ Lower nutrient removals in parentheses apply to wet ponds in coastal plain terrain.
- ¹⁴ The removal can be increased to 50% for HSG C and D soils by adding soil compost amendments, and may be higher yet if combined with secondary runoff reduction practices.

Source: Adapted from CWP (2008b) and Volume II of the Northern Marianas/Guam Stormwater Management Manual (2006)

8.4.6 Community and Environmental Factors (Table 8.9 below)

Do the remaining BMPs have any important community or environmental benefits or drawbacks that might influence the selection process? In this last step, **Table 8.9** is used to assess the following community and environmental considerations involved in BMP selection:

Maintenance. This column assesses the relative effort needed to maintain the BMP, in terms of three criteria: (1) frequency of scheduled maintenance, (2) chronic maintenance problems (such as clogging), and (3) reported failure rates. It should be noted that the regulations require routine BMP inspection and maintenance under certain circumstances, for which Virginia requires a long-term Maintenance Agreement between the BMP owner and the local jurisdiction within which the BMP is located. This provides legal assurance that routine maintenance will be done to assure the continued proper functioning of the BMP.

Overall Affordability. The BMPs are ranked according to (1) their relative construction cost per impervious acre treated and (2) their long-term maintenance costs. These costs exclude design, land acquisition, and other costs.

Community acceptance. This column assesses community acceptance, as measured by three factors: (1) market and preference surveys, (2) reported nuisance problems, and (3) visual orientation (i.e., is it prominently located or is it in a discrete underground or other out-of-sight location). It should be noted that a low rank can often be improved by a better landscaping plan.

Safety. This column provides a comparative index that expresses the relative public safety of a BMP. An open circle indicates a reasonably safe BMP, while a darkened circle indicates that deep pools may present potential public safety risks. The safety factor is included at this stage of the screening process because liability and safety are of paramount concern in many residential settings. It should be noted that a low rank can be improved by using measures that restrict access, such as fencing. However, such measures may affect the ranking related to aesthetics.

Habitat. BMPs are evaluated on their ability to provide wildlife or wetland habitat, assuming that an effort is made to landscape them appropriately. Objective criteria include size, water features, wetland features, and vegetative cover of the BMP and its buffer.

Aesthetic, Recreational Benefits or Other Concerns. BMPs are evaluated on their ability to (1) provide a perceived positive influence on the visual appearance of the lot or development, (2) contribute to the recreational value at the lot, development or community scale, ideally as part of a community greenway network, or (3) provide other perceived ancillary benefits.

Table 8.9. BMP Selection Matrix 6 - Community and Environmental Factors

BMP Group	Specific BMP	Ease of Maintenance	Overall Affordability	Community Acceptance	Safety	Habitat	Aesthetics and Other Concerns
	Vegetated Roof	(•	(0	•	Invasive veg. and water leaks; reg. inspection and maint. can address these Impediments to
Runoff	Rooftop Disconnect.	O to	O to •	•	0	•	use in existing local health and building codes
Volume	Rainwater Harvesting	•	•	•	0	•	
Reduction	Soil Compost Amendments	0	0	0	0	0	Helps prevent standing water and adds soil moisture for plant materials
	Sheet flow to Veg. Filter and Conserv. Open Space	0	0	0	0	0	Inc. into landscape; overgrown vegetation
	Grass Channels	0	0	0	0	•	Attractive natural drainage mechanism
Swales & Open Channels	Dry Swales	0	•	0	0	•	Attractive natural drainage mechanism with enhanced infiltration and treatment
Filtering Systems	Filtering Practices	•	•	0	0	•	Filter media replacement; Underground practices are not seen and therefore often not maintained
	Bioretention 1	•	•	•	0	•	Inc. into landscape; mosquitoes; overgrown vegetation
	Permeable Pavement	•	•	•	0	•	Susceptible to failure if poorly installed or maintained
Infiltration Practices	Infiltration	•	•	0	0	•	Susceptible to failure if poorly installed or maintained
	Bioretention 2	(((0	•	Inc. into Landscape; Mosquitoes; Overgrown vegetation

BMP Group	Specific BMP	Ease of Maintenance	Overall Affordability	Community Acceptance	Safety	Habitat	Aesthetics and Other Concerns
	Constructed Wetlands	•	•	(•	0	Undesirable animals; Mosquitoes; Overgrown vegetation and unsightly conditions
Basins	Wet Swales	0	•	•	0	•	Undesirable animals; Mosquitoes; Overgrown vegetation and unsightly conditions
	Wet Ponds	0	0	•	•	0	Geese, Odors, Mosquitoes, Floatable Trash; Safety & liability concerns
	Extended Detention 1	0	0	•	•	•	Undesirable animals; Overgrown vegetation and unsightly conditions
	Hydrodymanic Devices	•	•	0	0	•	Underground practices are not seen and therefore often not maintained
Mfr Treatment Devices	Filtration Devices	•	•	0	0	•	Underground practices are not seen and therefore often not maintained
O Dieb oo	Storage Devices	•	•	0	0	•	Underground practices are not seen and therefore often not maintained

O High or Good or Easy

8.4.7 Consideration of Regulatory Restrictions and Setbacks (Table 8.10 below)

Table 8.10 presents an overview of ten site-specific considerations of environmental resources or infrastructure present on the site or Virginia rules or conditions that may apply that will influence where a BMP can be located on the site (i.e., setback or similar restriction).

[■] Medium

Low or Difficult

Table 8.10. Location-Specific Restrictions and Setbacks

Factor	Considerations
Jurisdictional Wetland	Wetlands should be delineated prior to siting BMPs
U.S. Army Corps of Engineers(USACE) Section 404 Permit	Demonstrated that the impact to a wetland complies with all of the following principles in descending order of priority: (1) avoid direct or indirect impacts; (2) minimize impact by limiting the degree or magnitude of activity; and (3) mitigate unavoidable impacts through wetland restoration or creation, providing justification that no practical
Va. Department of Environmental Quality (DEQ) Section 401 Water Quality Certification and Wetlands and Water Protection Permits	 upland treatment alternatives exist. Always check with local, state and federal jurisdictions for applicable regulations. Using natural wetlands for stormwater treatment is strongly discouraged, unless they are severely impaired and construction would enhance or restore wetland functions; impacts to natural wetlands will require state and federal permits. Direct pipe outfalls to natural wetlands should be restricted; stormwater must be treated prior to discharge into a natural wetland and, where practical, excess stormwater flows should be conveyed away from jurisdictional wetlands. BMPs are restricted from location within the Chesapeake Bay Preservation Act RPA buffer. RPA buffers may be used as a non-structural filter strip accepting sheet flow, not concentrated flows.
Stream Channel USACE Section 404 Permit and/or Va. DEQ Section 401 Water Quality Certification and Wetlands and Water Protection Permits	 All waterways (including streams, ponds, lakes, etc.) should be delineated prior to design. Use of any Waters of the U.S. for stormwater quality treatment is contrary to the goals of the Clean Water Act and should be avoided. BMPs should not be placed on-line (in-stream) under most conditions and will require federal and state permits, if necessary, providing justification that no practical upland treatment alternatives exist. If an on-line pond is necessary, its use for channel protection or flood protections purposes are preferred to use for water quality treatment. Implement measures that reduce downstream warming. Activities such as excavation, shore protection, structures, dams, and water level controls are regulated. State (DEQ) water quality standards apply and may not be violated.
Shoreland Management, Chesapeake Bay Preservation Areas, and Stream Buffers Va. Marine Resource Commission (VMRC) and/or Applicable shoreland development ordinances	 VMRC regulates tidal wetlands (elevations below 1.5 x the mean high tide elevation), associated shorelands, and all state bottoms (the land beneath streams, rivers, etc. that comprise state waters). All Tidewater Virginia local governments (§ 62.1-44.15:67 et seq., Code of Virginia) have Chesapeake Bay Preservation Area ordinances that require buffers and setbacks from shorelines; other localities outside Tidewater Virginia may also have shoreland development ordinances with similar requirements. Consider how stormwater outfall channels will cross a buffer to reach a stream.

Factor	Considerations				
100-Year Floodplain Va. Department of Conservation and Recreation (DCR) Division of Dam Safety and Floodplain Management and Applicable local floodplain management ordinances and stormwater review authority	 Grading and fill for BMP construction is strongly discouraged within the ultimate 100-year floodplain, as delineated on FEMA flood insurance rate maps, FEMA flood boundary and floodway (or more stringent local) maps. Floodway fill may not raise the 100-year water surface elevation by more than 0.5 feet (local regulations may be more stringent). 				
Water Wells Local health authority	 Observe local wellhead protection zones and minimum setbacks. Consult the Virginia Department of Health, the local health department, and the local water utility. A 100-foot setback for infiltration practices and 50-foot setback for other BMPs is recommended. There should be no infiltration of confirmed hotspot runoff; runoff from potential hotspot runoff should be restricted and have suitable pretreatment. 				
Utilities Local review authority	 Contact "Miss Utility" to locate existing utilities prior to design. Note the location of proposed utilities to serve development. BMPs are discouraged within utility easements or rights-of-way for public or private utilities. 				
Septic Drain Fields Local health authority	Consult the local health authority. A minimum 50-foot setback from a drainfield edge is recommended for BMP location.				
Roads Virginia Department of Transportation (VDOT) and/or Local transportation	 Consult the local transportation authority, DPW or subdivision ordinance/regulations for setback requirements from local roads and streets. Consult VDOT for setbacks from state-maintained roads. Approval must also be obtained for any stormwater discharges to a local or state-owned storm drain or conveyance channel. 				
authority or DPW Structures Local review authority	Consult the local review authority for any BMP setback from structures.				

Factor	Considerations				
Karst (Sinkholes)	Geotechnical testing is recommended and may be required within karst areas.				
Local review authority EPA Region III UIC Pgm Virginia Cave Board	Existing sinkholes should be identified and delineated on site plans.				
	 BMPs should be designed to be off-line to limit volumes and flow rates managed by individual practices; infiltration or pooling of stormwater near sinkholes is discouraged; sinkhole formation is less likely when practices such as bioretention and vegetated filters are used; sinkholes should be remediated and stormwater directed away from these areas during and after construction. 				
	 Any discharge of stormwater runoff to a sinkhole or other karst feature must meet the water quality control criteria set out in 9 VAC 25-870-63 and the water quantity control criteria set out in 9 VAC 25-870-66 of the Virginia Stormwater Management Regulations 				
	 Formation of sinkholes within an BMP is evidence of failure; sinkholes occurring within BMPs should be repaired as soon as feasible after the first observation, using appropriate engineering techniques (e.g., VDOT IIM228 – Sinkholes: Guidelines for the Discharge of Stormwater at Sinkholes; WVDEP, 2004; MDE, 2000; etc.). 				
	 Consistent with federal environmental regulations at 40 CFR parts 144-148, some karst features receiving runoff may be considered to be class V injection wells and must be registered as such with the EPA Region III. To ensure compliance in cases where stormwater runoff is discharged to a karst feature, DEQ recommends coordination with the EPA Groundwater & Enforcement Branch (3WP22), U.S. EPA Region 3, 1650 Arch Street, Philadelphia, PA 19103 (Phone: 215-814- 5427; FAX: 215-814-2318). 				

8.4.8 Spatial Scale At Which Practices Are Applied (8.11 below)

The matrix provided in **Table 8.11** below compares the different spatial scales at which the various stormwater control measures can be applied to reduce runoff and remove pollution. The major change in the new BMP design specifications is that most practices are applied at a smaller spatial scale than has been done in the past. This means that more practices will be needed at each site. Note that the area ranges specified in **Table 8.11** for contributing drainage areas (CDAs) are approximate, and may actually be greater or smaller depending on the specific design and site characteristics. Multiple BMPs of the same or different kind may be used in combination to treat a larger CDA.

Table 8.11. Comparison of Practices Based on Contributing Drainage Area Served

Practice	Spec No.	Space ¹	Micro Scale	Small Scale	Normal Scale	Moderate Scale	Large Scale
Rooftop Disconnection	1	Nominal	250 to 1000 sq. ft.				
Sheet Flow to Veg. Filter or Conserved Open Space	2	15-25%		1000 to 5000 sq. ft.	5000 to 25,000 sq. ft.		
Grass Channels	3	5-15%	20,000 sf to 2 sq. ft.		50,000		
Soil Compost Amendments	4	Nominal	250 sq. ft. to 2 acres				
Vegetated Roofs	5	Nominal	Residential	l ('ommercial			
Rainwater Harvesting	6	Nominal	250 to 2000 sq. ft.	2,000 to 200,0	000 sq. ft.		
Permeable Pavement	7	Nominal	250 to 1000 sq. ft.	1000 to 10,000 sq. ft.	10,000 to 200,000 sq. ft.		
Infiltration	8	1-4%	250 to 2500 sq. ft.	2500 to 20,000 sq. ft.	20,000 to 100,000 sq. ft.		
Bioretention	9	3-5%	250 to 2500 sq. ft.	2500 to 20,000 sq. ft.	20,000 to 100,000 sq. ft.		
Urban Bioretention	9A	Nominal	250 to 2500 sq. ft.	2500 to 20,000 sq. ft.			
Dry Swales	10	5-15%	20,000 to		20,000 to 250	,000 sq. ft.	
Wet Swales	11	5-15%	20,000 to 25		20,000 to 250	,000 sq. ft.	
Filtering Practices	12	0-3%	20,000 to 250,			,000 sq. ft.	
Constructed Wetlands	13	3%					10 + acres,
Wet Ponds	14	1-3%				unless favorable	
Extended Detention Ponds	15	1-3%					water balance

8.5 REFERENCES

Alexander, D., and J. Heaney. 2002. Comparison of Conventional and Low Impact Development Drainage Designs. Final Report to the Sustainable Futures Society. University of Colorado, Boulder.

Balusek. 2003. Quantifying Decreases in Stormwater Runoff from Deep-Tilling, Chisel-Planting and Compost Amendments. Dane County Land Conservation Department. Madison, WI.

Barten, J., and J. Johnson. 2007. Nutrient management with the Minnesota phosphorus fertilizer law. *Lakeline* (summer):23-28

Bean, E. Z., W. F. Hunt, and D. A. Bidelspach. 2007. Evaluation of Four Permeable Pavement Sites in Eastern North Carolina for Runoff Reduction and Water Quality Impacts. ASCE Journal of Irrigation and Drainage Engineering 133(6):583-592.

Bender, G. M., and M. L. Terstriep. 1984. Effectiveness of street sweeping in urban runoff pollution control. The Science of the Total Environment 33:185-192.

Bernhardt, E., M. Palmer, J. Allen, G. Alexander, K. Barnas, S. Brooks, J. Carr, S. Clayton, C. Dahm, J. Follstad-Shah, D. Galat, S. Gloss, P. Goodwin, D. Hart, B. Hassett, R. Jenkinson, S. Katz, G. M. Kondolf, P. S. Lake, R. Lave, J. L. Meyer, T. K. O'Donnell, L. Pagano, B. Powell, E. Sudduth. 2005. Ecology: Synthesizing US river restoration efforts. *Science*: 308:636-637.

Bernhardt, E., and M. Palmer. 2007. Restoring streams in an urbanizing landscape. Freshwater Biology 52:731-751.

Bernot, M., and W. Dodds. 2005. Nitrogen retention, removal and saturation in lotic ecosystems. *Ecosystems* 8:442-453.

Braskerud, B. C. 2001. The Influence of vegetation on sedimentation and resuspension of soil particles in small constructed wetlands. Journal of Environmental Quality 30:1447-1457.

Brinkman, R., and G. A. Tobin. 2001. Urban Sediment Removal: The Science, Policy, and Management of Street Sweeping. Boston, MA: Kluwer Academic.

Brown, E., D. Carac, and R. Pitt. 2004. Illicit discharge detection and elimination: A guidance manual for program development and technical assessments. Ellicott City, MD: Center for Watershed Protection.

Bukaveckas, P. 2007. Effects of channel restoration on water velocity, transient storage and nutrient uptake in a channelized stream. *Environmental Science and Technology* 41:1570-1576.

Cappiella, K., and K. Brown. 2000. Derivation of impervious cover for suburban land uses in the Chesapeake Bay. Final Report. Chesapeake Research Consortium. Center for Watershed Protection. Ellicott City, MD.

Cappiella, K., T. Schueler, and T. Wright. 2006. Urban Watershed Forestry Manual. Part 2: Conserving and Planting Trees at Development Sites. Newtown Square, PA: USDA Forest Service.

CASQA (California Stormwater Quality Association). 2007. Municipal Stormwater Program Effectiveness Assessment Guidance. California Association of Stormwater Quality Agencies. Sacramento.

Center for Watershed Protection (CWP). 1997. Stormwater BMP Design Supplement for Cold Climates. Ellicott City, MD.

Chang, Y., Chou, C., Su, K., and C. Tseng. 2005. Effectiveness of street sweeping and washing for controlling ambient TSP. Atmospheric Environment 39:1891-1902.

Chang, M. 2006. Forest Hydrology: An Introduction to Water and Forests, 2nd Ed. New York: CRC Press.

Clark, S., M. Lalor, R. Pitt, and R. Field. 2005. Wet-weather pollution from commonly used building materials. Paper presented at the 10th International Conference on Urban Drainage, August 21-26, Copenhagen.

Cheng, M., L. Coffman, Y. Zhang, and J. Licsko. 2005. Hydrologic responses from low impact development compared to conventional development. Pp 337-357 in *Stormwater Management for Smart Growth*. New York: Springer.

Chollak, T., and P. Rosenfeld. 1998. Guidelines for Landscaping with Compost-Amended Soils. Prepared for City of Redmond Public Works. Redmond, WA. Available at (accessed 8/26/2008): http://www.ci.redmond.wa.us/insidecityhall/publicworks/environment/pdfs/compostamendedsoils.pdf.

Coombes, P., J. Argue, and G. Kuczera. 2000. Figtree Place: A case study in water sensitive urban development (WSUD). Urban Water Journal 4(1):335-343.

Coombes, P. 2004. Water sensitive design in the Sydney Region—Practice Note 4. Rainwater Tanks. Published by the Water Sensitive Design in the Sydney Region Project.

Cross, L., and L. Duke. 2008. Regulating industrial stormwater: State permits, municipal implementation, and a protocol for prioritization. Journal of the American Water Resources Association 44(1):86-106.

CWP (Center for Watershed Protection). 1998a. Better Site Design: A Handbook for Changing Development Rules in Your Community. Ellicott City, MD: Center for Watershed Protection.

CWP. 1998b. The benefits of better site design in residential subdivisions. Watershed Protection Techniques 3(2):633-646.

CWP. 1998c. The benefits of better site design in commercial developments. Watershed Protection Techniques 3(2):647-656.

CWP, 2002

CWP. 2004. Stormwater pond and wetland maintenance guidebook. Ellicott City, MD: Center for Watershed Protection.

CWP. 2005. Pollution Source Control Practices. Manual 8, Urban Subwatershed Restoration Manual Series. Ellicott City, MD: Center for Watershed Protection.

CWP. 2008a. Municipal good housekeeping practices. Manual 9, Urban Small Watershed Restoration Manual Series. Ellicott City, MD: Center for Watershed Protection.

CWP. 2008b. Draft Virginia Stormwater Management Nutrient Design System. Prepared for Technical Advisory Committee and Virginia DCR. Richmond, VA. Center for Watershed Protection. Ellicott City, MD.

Davis, A. P., W. F. Hunt, R. G. Traver, and M. E. Clar. 2008. Bioretention technology: An overview of current practice and future needs. *ASCE Journal of Environmental Engineering* (accepted).

Deschesne, M., S. Barraud, and J. P. Bardin. 2005. Experimental Assessment of Stormwater Infiltration Basin Evolution. Journal of Environmental Engineering 131(7):1090–1098.

Dietz, M., and J. Clausen. 2006. Saturation to improve pollutant retention in a rain garden. Environmental Science and Technology 40(4):1335-1340.

Doll, R., and G. Jennings. 2003. Stream restoration: A natural channel design handbook. North Carolina State University Extension, Raleigh.

Duke, L., and C. Augustenberg. 2006. Effectiveness of self regulation and self-reported environmental regulations for industry: the case of stormwater runoff in the U.S. Journal of Environmental Planning and Management 49(3):385-411

Emerson, C., and R. Traver. 2008. Long-Term and Seasonal Variation of Stormwater Infiltration Best Management Practices. ASCE Journal of Irrigation and Drainage, In press.

EPA. 2007. Evaluation Report: Development Growth Outpacing Progress in Watershed Efforts to Restore the Chesapeake Bay. Office of the Inspector General. EPA 2007-P-0031. Washington DC. EPA.

Ermilio, J., and R. Traver. 2006. Hydrologic and pollutant removal performance of a bio-infiltration BMP. EWRI 2006, National Symposium.

Ferguson, B. K. 2002. Stormwater Management and Stormwater Restoration, Chapter I.1 of *Handbook of Water Sensitive Planning and Design*, Robert L. France, editor, Lewis Publishers.

FISRWG (Federal Interagency Stream Restoration Working Group). 2000. Stream Corridor Restoration: Principles, Processes and Practices. Washington, DC: USDA Natural Resource Conservation Service.

GAO (General Accounting Office). 2007. Goetz, S., R. Wright, A. Smith, E. Zinecker, and E. Schaub. 2003. IKONOS imagery for resource management: Tree cover, impervious surfaces, and riparian buffer analyses in the mid-Atlantic region. Remote Sensing in the Environment 88:195-208.

Gomi, T., R. Sidle, and J. Richardson. 2002. Understanding processes and downstream linkages of headwater systems. *BioScience* 53(10):905-915.

Greenway, M., P. Dale, and H. Chapman. 2003. An assessment of mosquito breeding and control in 4 surface flow wetlands in tropical–subtropical Australia. Water Science and Technology 48(5):249–256.

Gregory, J., M. Duke, D. Jones, and G. Miller. 2006. Effect of urban soil compaction on infiltration rates. *Journal of Soil and Water Conservation*. 61(3):117-133.

Groffman, P., A. Dorset, and P. Mayer. 2005. N processing within geomorphic structures in urban streams. Journal North American Benthological Society 24(3):613-625. 05.

Hardy, M, P. Coombes, and G. Kuczera. 2004. An investigation of estate level impacts of spatially distributed rainwater tanks. Proceedings of the 2004 International Conference on Water Sensitive Urban Design—Cities as Catchments, November 21–25, 2004, Adelaide.

Hathaway, J., and W. Hunt. 2006. Level spreaders: Overview, design and maintenance. Urban Waterways. North Carolina State University and Cooperative Extension. Raleigh.

Hillel, D. 1998. Environmental Soil Physics. San Diego: Academic Press.

Holman-Dodds, J., A. Bradley, and K. Potter. 2003. Evaluation of hydrologic benefits of infiltration based urban stormwater management. Journal of the American Water Resources Association 39(1):205-215.

Horner, R., H. Lim, and S. Burges. 2003. Hydrologic Monitoring of the Seattle Ultra-Urban Stormwater Management Project. Water Resources Series. Technical Report 170. Seattle, WA: University of Washington Department of Civil and Environmental Engineering.

Huber, W. L. Cannon and M. Stouder. 2006. BMP Modeling Concepts and Simulation. Oregon State University, Corvallis. EPA/600/R-06/033 U.S. Environmental Protection Agency.

Hunt, W., and W. Lord. 2006. Bioretention Performance, Design, Construction, and Maintenance. AG588-05. North Carolina Cooperative Extension Service. Urban Waterways.

Hunt, W. F., J. T. Smith, S. J. Jadlocki, J. M. Hathaway, and P. R. Eubanks. 2008. Pollutant removal and peak flow mitigation by a bioretention cell in urban Charlotte, NC. ASCE Journal of Environmental Engineering 134(5):403-408.

Jefferies, C. 2004. Sustainable Drainage Systems in Scotland: The Monitoring Programme. Scottish Universities SUDS Monitoring Project. Dundee, Scotland.

Johnson, C., T. Driscoll, T. Siccama and G. Likens. 2000. Elemental fluxes and landscape position in a northern hardwood forest ecosystem. *Ecosystems*. 3: 159-184.

Kaushal, S., P. Groffman, P. Meyer, E. Striz, and A. Gold. 2008. Effects of stream restoration on denitrification in an urbanizing watershed. *Ecological Applications* 18(3):789-804.

Kitchell, A. 2002. Managing for a pure water supply. Watershed Protection Techniques 3(4):800-812.

Konrad, C. 2003. Opportunities and constraints for urban stream rehabilitation. Pp in Restoration of Puget Sound Rivers, D. Montgomery, S. Bolton, D. Booth, and L. Wall, eds. Seattle: University of Washington Press.

Kwiatkowski, M., A. L. Welker, R. G. Traver, Vanacore, M., & Ladd, T. 2007. Evaluation of an infiltration best management practice (BMP) utilizing pervious concrete. Journal of the American Water Resources Association (in press).

Lager, J. A., W. G. Smith, and G. Tchobanoglous. 1977. Catchbasin Technology Overview and Assessment. EPA-600/2-77-051. Cincinnati, OH: EPA.

Larson, M. L., D. B. Booth, and S. M. Morley. 2001. Effectiveness of large woody debris in stream rehabilitation projects in urban basins. Ecological Engineering 18(2):211-226.

Law, N. 2006. Research in support of an interim pollutant removal rate for street sweeping and storm drain cleanout. Technical Memo No. 2. Prepared for the EPA Chesapeake Bay Program and Urban Stormwater Working Group. Ellicott City, MD: Center for Watershed Protection.

Law, N., K. Diblasi, and U. Ghosh. 2008. Deriving Reliable Pollutant Removal Rates for Municipal Street Sweeping and Storm Drain Cleanout Programs in the Chesapeake Bay Basin. Ellicott City, MD: Center for Watershed Protection.

Legg, A., R. Bannerman, and J. Panuska. 1996. Variation in the relation of runoff from residential lawns in Madison, Wisconsin. USGS Water Resources Investigations Report 96-4194. U.S. Geological Survey.

Lichter, J., and P. Lindsey. 1994. Soil compaction and site construction: Assessment and case studies. The Landscape Below Ground. International Society of Arboriculture.

Lloyd, S., T. Wong and C. Chesterfield. 2002. Water sensitive urban design: a stormwater management perspective. Cooperative Research Centre for Catchment. Monash University, Victoria 3800 Australia. Industry Report 02/10.

Loucks, D. P., E. van Beek, J. R. Stedinger, J. P. M. Dijkman, and M. T. Villars. 2005. Water Resources Systems Planning and Management: An Introduction to Methods, Models, and Applications. Paris: UNESCO.

Lowrance, R., and J. Sheridan. 2005. Surface runoff quality in a managed three zone riparian buffer. Journal of Environmental Quality 34:1851-1859.

Maryland Department of Environment (MDE). 2000. "Geotechnical Methods for karst feasibility testing." *Maryland Stormwater Design Manual*. *Appendix D-2*. Available at: http://www.mde.state.md.us/Programs/WaterPrograms/SedimentandStormwater/stormwater design/index.asp

Maryland Department of Natural Resources (MD DNR). 2005. A Users Guide to Watershed Planning in Maryland. Annapolis, MD: DNR Watershed Services.

McBride, M., and D. Booth. 2005. Urban impacts on physical stream condition: Effects on spatial scale, connectivity, and longitudinal trends. Journal of the American Water Resources Association 6:565-580.

McCuen, R. H. 1979. Downstream effects of stormwater management basins. Journal of the Hydraulics Division 105(11):1343-1356.

Metropolitan Council. 2001. *Minnesota Small Urban Sites BMP Manual*. Metropolitan Council Environmental Services. St. Paul, MN. Prepared by Barr Engineering Co.

Meyers, J. 2003. Where Rivers Are Born: The Scientific Imperative for Defending Small Streams and Wetlands. Washington, D.C.: American Rivers.

Mineart, P., and S. Singh. 1994. Storm Inlet Pilot Study. Performed by Woodward Clyde Consultants for Alameda County Urban Runoff Clean Water Program.

Minton, Gary. 2005. *Stormwater Treatment*. Seattle, WA. Resource Planning Associates (printed by Sheridan Books Inc.)

Moore, A. and M. Palmer. 2005. Invertebrate diversity in agricultural and urban headwater streams: Implications for conservation and management. Ecological Applications 15(4):1169-1177.

Morgan, R. A., F. G. Edwards, K. R. Brye, and S. J. Burian. 2005. An evaluation of the urban stormwater pollutant removal efficiency of catch basin inserts. Water Environment Research 77(5):500-510.

National Research Council (NRC). 2000. Watershed Management for a Potable Water Supply. Washington, DC: National Academy Press.

NRC, 2008. Water and Science Technology Board, Division of Earth and Life Studies. "Chapter 3 Hydrologic, Geomorphic, and Biological Effects of Urbanization on Watersheds." *Urban Stormwater Management in the United States*. Washington, DC: National Academies Press, 109+. http://www.nap.edu/catalog.php?record_id=12465#toc

Nichols, D., Akers, M.A., Ferguson, B., Weinberg, S., Cathey, S., Spooner, D., and Mikalsen, T. 1997. Land development provisions to protect Georgia water quality. The School of Environmental Design, University of Georgia. Athens, GA. 35pp.

Passeport, E., Hunt, W.F., Line, D.E., and Smith, R.A. 2008. Effectiveness of two grassed bioretention cells at reducing stormwater pollution. *Under review*.

Perez-Pedini, C., J. Limbruneer, and R, Vogel. Optimal location of infiltration-based Best management practices for stormwater management. *ASCE Journal of Water Resources Planning and Management*, 131(6): 441-448.

Philips, R., C. Clausen, J. Alexpoulus, B. Morton, S. Zaremba, and M. Cote. 2003. BMP research in a low-impact development environment: The Jordan Cove Project. Stormwater 6(1):1-11.

Pitt, R. 1979. Demonstration of Nonpoint Pollution Abatement Through Improved Street Cleaning Practices. EPA-600/2-79-161. Cincinnati, OH: EPA.

Pitt, R., with contributions from S. Clark, R. Field, and K. Parmer. 1996. Groundwater Contamination from Stormwater. ISBN 1-57504-015-8. Chelsea, MI: Ann Arbor Press, Inc. 219 pages.

Pitt, R., T. Brown, and R. Morchque. 2004a. National Stormwater Quality Database. Version 2.0. University of Alabama and Center for Watershed Protection. Final Report to U.S. Environmental Protection Agency.

Pitt, R., Maestre, A., and Morquecho, R. 2004b. National Stormwater Quality Database. Version 1.1. Available at http://rpitt.eng.ua.edu/Research/ms4/Paper/Mainms4paper.html.

Pitt, R., S. Chen, S. Clark, and J. Lantrip. 2005. Soil structure effects associated with urbanization and the benefits of soil amendments. Pp. in World Water and Environmental Resources Congress. Conference Proceedings. American Society of Civil Engineers. Anchorage, AK.

Pouyat, R., M. McDonnel, and S. Pickett. 1995. Soil characteristics of oak stands along an urban-rural land use gradient. Journal of Environmental Quality 24:516-526.

Pouyat, R., I. Yesilonis, J. Russell-Anelli, and N. Neerchal. 2007. Soil chemical and physical properties that differentiate urban land use and cover types. Soil Science Society of America Journal 71(3):1010-1019.

Rea, M., and R. Traver. 2005. Performance monitoring of a stormwater wetland best management practice, National Conference, World Water & Environmental Resources Congress 2005 (EWRI/ASCE).

Reed, S. C., R. W. Crites, and E. J. Middlebrooks. 1998. Natural systems for waste management and treatment. McGraw-Hill Professional. ISBN 0071346627, 9780071346627.

Richman, T. 1997. Start at the Source: Design Guidance for Storm Water Quality Protection. Oakland, CA: Bay Area Stormwater Management Agencies Association.

Roy, A., C. Faust, M. Freeman, and J. Meyer. 2005. Reach-scale effects of riparian forest cover on urban stream ecosystems. *Canadian Journal of Fisheries and Aquatic Science* 62:2312-2329.

Roy, A., M. Freeman, B. Freeman, S. Wenger, J. Meyer, and W. Ensign. 2006. Importance of riparian forests in urban subwatersheds contingent on sediment and hydrologic regimes. *Environmental Management* 37(4):523-539.

Rushton, B. 2002. Low impact parking lot design infiltrates stormwater. Florida Department of Environmental Protection.

Schollen, M., T. Schmidt, and D. Maunder. 2006. Markham Small Streams Study—Policy Update and Implementing Guidelines for the Protection and Management of Small Drainage Courses. Town of Markham, Ontario.

Schueler, T. 1998. Irreducible pollutant concentration discharged from stormwater practices. Watershed Protection Techniques 2(2):369-372.

Schueler, T. 2001a. The compaction of urban soils. Watershed Protection Techniques 3(2):661-665.

Schueler, T. 2001b. Can urban soil compaction be reversed? Watershed Protection Techniques 3(2):666-669.

Schueler, T. 2001c. On watershed education. Watershed Protection Techniques 3(3):680-689.

Schueler, T., and K. Brown. 2004. Urban Stream Repair Practices: Manual 4. Urban Subwatershed Restoration Manual Series. Ellicott City, MD: Center for Watershed Protection.

Sharkey, L. J. 2006. The Performance of Bioretention Areas in North Carolina: A Study of Water Quality, Water Quantity, and Soil Media. Thesis: North Carolina State University, Raleigh.

Singer, M., and R. Rust. 1975. Phosphorus in surface runoff from a deciduous forest. Journal of Environmental Quality 4:302-311.

Smith, R. A., and W. F. Hunt. 2007. Pollutant removal in bioretention cells with grass cover. Pp. 1-11 in the Proceedings of the World Environmental and Water Resources Congress, 2007.

Stagge, J. 2006. Field Evaluation of Hydrologic and Water Quality Benefits of Grass Swales for Managing Highway Runoff. Master's Thesis, University of Maryland.

Stephens, K., P. Graham, and D. Reid. 2002. Stormwater Planning: A Guidebook for British Columbia. Vancouver, BC: Environment Canada.

Sudduth, E., J. Meyer, and E. Bernhardt. 2007. Stream restoration practices in the southeastern US. Restoration Ecology 15:516-523.

Traver, R. G., and R. A. Chadderton. 1992. Accumulation Effects of Stormwater Management Detention Basins. Hydraulic Engineering: Saving a Threatened Resource—In Search of Solutions. Baltimore, MD: American Society of Civil Engineers.

Turner, M. 2005. Leachate, Soil and Turf Concentrations from Fertilizer-Results from the Stillhouse Neighborhood Fertilizer Leachate Study. Austin: City of Austin Watershed Protection and Development Review Department.

United States Geological Survey (USGS). 2005. Evaluation of Street Sweeping as a Water-Quality Management Tool in Residential Basins in Madison. Scientific Investigations Report. September. Reston, VA: USGS.

Van Metre, P. C., B. J. Mahler, M. Scoggins, and P. A. Hamilton. 2006. Parking Lot Sealcoat: A Major Source of Polycyclic Aromatic Hydrocarbons (PAHs) in Urban and Suburban Environmental, USGS Fact Sheet 2005-3147.

Van Seters, T., D. Smith and G. MacMillan. 2006. Performance evaluation of permeable pavement and a bioretention swale. *Proceedings 8 International Conference on Concrete Block Paving*. November 6-8, 2006. San Francisco, CA.

Virginia Department of Conservation and Recreation (DCR). 1992. Virginia Erosion and Sediment Control Handbook, Third Edition. Richmond, VA.

Walsh, C, K. Waller, J. Gehling, and R. MacNally. 2007. Riverine invertebrate assemblages are degraded more by subwatershed urbanization than riparian deforestation. Freshwater Biology. Early on-line edition.

Wang, L., J. Lyons, and P. Kanehl. 2003. Impacts of urban land cover on trout streams in Wisconsin and Minnesota. Transactions of the American Fisheries Society 132:825-839.

West Virginia Department of Environmental Protection. (WVDEP). 2006. Stormwater management structure guidance document. Groundwater/UIC program. Morgantown, WV.

Winter, T. 2007. The role of groundwater in generating streamflow in headwater areas in maintaining baseflow. Journal of American Water Resources Association 43(1):15-25.

Zarriello, P., R. Breault, and P. Weiskel. 2002. Potential effects of structural controls and street sweeping on stormwater loads to the Lower Charles River, Massachusetts. USGS: Water Resources Investigations Report 02-4220. U.S. Geological Survey.

Appendix 8-A

EXAMPLE BMP DESIGN CHECKLISTS

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8-A.1.0. INTRODUCTION

Design and plan review checklists provide general guidance, for both the designer and plan reviewer, regarding the proper design of BMPs. Some items listed on the checklists may not apply to every design, so it is up to the designer to indicate items as "not applicable" (or "NA") where appropriate. Similarly, the reviewer must be able to distinguish which items are required, based on the local conditions or requirements, and verify the status of those items.

These checklists can be used as tools to provide designers with the necessary information needed to develop an approvable plan, as well as to provide the plan review authority with a consistent review procedure. The various "basin" checklists (Constructed Wetlands, Wet Pond, and Extended Detention Basin) have items included that reflect design criteria in Appendices A through E of the document entitled *Introduction to the New Virginia Stormwater Design Specifications*, found on the Virginia Stormwater BMP Clearinghouse web site at the following URL:

http://www.vwrrc.vt.edu/swc/NonProprietaryBMPs.html

These appendices address a number of design issues common to basin-type practices, such as the sediment forebay, earthen embankment, principal spillway, emergency spillway, and pond landscaping.

8-A.2.0. ROOFTOP DISCONNECTION: DESIGN CHECKLIST

Plan Submission Date		
Project Name		
Site Plan/Permit Number		
Practice No./Location on Site		
Owner		Phone Number
BMP Designer		
General Contractor		Phone Number
Signature and stamp certification	of licensed profess	ional design consultant and owner
Plan Status		
Approved	Legend:	🖟 Complete
Not Approved	· ·	Inc Incomplete/Incorrect N/A - Not Applicable
Commonantani davias timo (inglisda	if the new days area fla	noth is loss they the manying durining many
length): (NOTE: See the separate p		w path is less than the required minimum
☐ Dry Well (Micro-Infiltration, S		
•	• •	•
☐ French Drain (Micro-Infiltration		,
Amended Soils (Stormwater	• .	•
Rain Garden (Micro-Bioreter	•	•
Stormwater Planter (Micro-B	Bioretention, Stormwater D	Design Specification No. 9, Appendix A))
☐ Other:		
this practice fits into the overbasin, infiltration trench, etc. Provide a site map showing Facility area and an Contributing draina Areas of the site contributing draina Areas of the site contributing draina Areas of the site contribution of the soil boring logs with Depth to seasonal of the facility) Depth to bedrock (Soil suitability for inside a site of the seasonal Areas of the facility)	rerall plan, and stating all c.). g the location of this BMP my compensatory devices age area (CDA) boundaries ompensated for in water quesite site h Unified Soils Classificat high groundwater table (numinimum 2 ft 4 ft. below of litration (HSG A or B soiles.)	es and acreage quality calculations ions, showing: minimum 2 ft 4 ft. below the design bottom
worksheets. Provide time of concentrati Provide hydrograph genera	on (pre- and post-develop ation (pre- and post-devel	re- and post-developed conditions) with ped conditions), with worksheets. loped conditions) for appropriate design and
		tional-critical storm duration method)

B. 	Hydi	Specify assumptions and coefficients used. Hydraulic head required = 1-3 ft. for Micro-Infiltration and Micro-Bioretention Provide a stage-storage table and curve Show that compensatory devices are able to drain within 48 hours following a storm.
C.	Wate	Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet) When soil amendments are used in the downspout discharge flow path, the Runoff Reduction Spreadsheet will self-credit improved runoff volume reduction based on the change of the soil drainage characteristics (see Stormwater Design Specification No. 4)
III.	PLA	N REQUIREMENTS
A.	ВМР	Plan View Information Show the limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier. Show the layout and dimensions of the BMP(s)
	1.	Simple Rooftop Disconnection Maximum rooftop area treated = 1,000 sq. ft. Longest flow path (roof/gutter) = 75 ft. Disconnection length = longest flow path, but no less than 40 ft. Distance downspouts are extended from buildings or foundations = 5 ft. for simple foundations if grade is < 1% (15 ft. in karst areas)
	2.	Rooftop Disconnection to Micro-Infiltration (Dry Well or French Drain) Maximum rooftop area treated = 250 to 2,500 sq. ft. Runoff reduction sizing based on Stormwater Design Specification #8 Observation well NOT required Soil test/boring required = 1 per practice Distance downspouts are extended from buildings or foundations = 5 ft. down-gradient for simple foundations (15 ft. in karst areas), or 25 ft. up-gradient
	3.	Rooftop Disconnection to Micro-Bioretention (Rain Garden, Stormwater Planter, etc.) Maximum rooftop area treated = 1,000 sq. ft. Type of inflow to secondary practice = sheet flow or roof leader Runoff reduction sizing based on a bioretention surface area = 5% of roof area (Level 1) or 6% of roof area (Level 2); for Stormwater Planters, an infiltration planter is sized to store a minimum of 1/2-inch of runoff from the contributing roof area Observation well NOT required Underdrain and gravel layer = Required for Level 1; Optional for Level 2, depending on soils (refer to Stormwater Design Specification No. 9, Table 2) Soil test/boring required = 1 per practice, but only when an underdrain is NOT used Distance downspouts are extended from buildings or foundations = 5 ft. down-gradient for simple foundations (15 ft. in karst areas), or 25 ft. up-gradient Stormwater filter planters can be placed right next to the building; infiltration planters must be placed a minimum of 10 ft. from the building

B. BMP Section Views & Related Details

C.

D.

1.	Simple Rooftop Disconnection
	Disconnection slope = < 2% (or < 5% with specified turf reinforcement)
	Distance downspouts are extended from buildings or foundations = 5 ft. for simple
	foundations if grade is < 1% (15 ft. in karst areas)
	Pre-treatment = external (leaf screens, etc.)
2.	Rooftop Disconnection to Micro-Infiltration (Dry Well or French Drain)
	Recommended maximum depth = 3 ft.
	Minimum soil infiltration rate = 0.5 in./hr.
	Observation well NOT required
	Pre-treatment = external (leaf screens, grass filter strip, etc.)
	Soil test/boring required = 1 per practice
	Distance downspouts are extended from buildings or foundations = 5 ft. down-gradient
	for simple foundations (15 ft. in karst areas), or 25 ft. up-gradient
3.	Rooftop Disconncection to Micro-Bioretention (Rain Garden, Stormwater Planter, etc.)
	Type of inflow to secondary practice = sheet flow or roof leader
	Minimum soil infiltration rate = 0.5 in./hr. (or use underdrain)
	Observation well NOT required
	Pre-treatment = external (leaf screens, etc.)
	Underdrain and gravel layer = Required for Level 1; Optional for Level 2, depending on
	soils (refer to Stormwater Design Specification No. 9, Table 2)
	Stormwater filter planters must have an overflow pipe installed to prevent water from
	spilling over the side when excess rainfall occurs
	Minimum filter media depth = 18 in. for Level 1; 24 inches for Level 2; for a stormwater
	planter, 30 in. for an infiltration planter, and a min. 18 in. for a filter planter
	Media source = mixed on site consistent with Stormwater Design Specification No. 9;
	planting media should have an infiltration rate of at least 2 in./hr., and the sand/gravel
	on the planter bottom should have a rate of at least 5 in./hr.
	Soil test/boring required = 1 per practice, but only when an underdrain is NOT used
	Distance downspouts are extended from buildings or foundations = 5 ft. down-gradient
	for simple foundations (15 ft. in karst areas), or 25 ft. up-gradient
	Stormwater filter planters can be placed right next to the building; infiltration planters
	must be placed a minimum of 10 ft. from the building
Lan	dscape Plan (perimeter)
	Provide a planting schedule and specifications (transport / storage / installation / maintenance)
	Ensure that plant selection is appropriate for the site's vegetation climatic zone (4-8 in Virginia),
	emphasizing native species
	Specify preservation measures for existing vegetation
	Ensure that topsoil / planting soil is included in the final grading
	The construction contract should include a Care and Replacement Warranty to ensure that new
	vegetation is properly established and survives during the first growing season following
	construction.
Con	struction Notes
	Construction sequence for BMP(s) and E&S controls:
	Install applicable temporary E&S control measures.
	Convey base flow around secondary practice while it is being constructed.
	Prepare the bottom surface of the stone reservoir,
	Lay down filter fabric, if applicable.
	Install french drain tile, if applicable.
	Place aggregate for dry well or french drain.

	 Install overflow and underdrain, if applicable. Place bioretention media, if applicable. For other compensatory BMP(s), see the plan review checklists for those practices Install temporary and permanent stabilization measures
E.	Maintenance Items (can include BMP Operation & Maintenance Inspection Checklists from Chapter 9, Appendix 9-C of this Handbook) Provide a Maintenance Agreement, indicating the person or organization responsible for maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist. Include a Maintenance Narrative which describes the long-term maintenance requirements. Record a deed restriction, drainage easement, and/or other enforceable mechanism, including GPS coordinates of the area, to ensure property owner awareness, access for inspections and maintenance, and that downspouts remain disconnected.
IV.	COMMENTS
_	
	Pur Data:

8-A.3.0. SHEET FLOW TO VEGETATED FILTER AREAS AND CONSERVED OPEN SPACE: DESIGN CHECKLIST

Plan Submission Date		
Project Name		
Site Plan/Permit Number		
Practice No./Location on Site		
Owner		
BMP Designer		
General Contractor		Phone Number
Signature and stamp of licer certification	nsed professio	nal design consultant and owner
Plan Status		
Approved	Legend:	🗓 Complete
Not Approved	_ 	Inc Incomplete/Incorrect N/A - Not Applicable
Control device type:	Receiv	ring filter area:
☐ Engineered Level Spreader (ELS)		Vegetated filter area (amended soils
☐ Level Spreader with vegetated lip		with dense turf cover or herbaceous
☐ Gravel Diaphragm (GD)		cover, shrubs and trees
,		Forested/vegetated buffer/open space
□ Permeable Berm (PB)		(undisturbed soils and native veg.)
☐ Other:	_	Other:
this practice fits into the overall plan, basin, infiltration trench, etc.). Provide a site map showing location and a site map showing location are also as a site map showing location are also as a site map showing location are also as a site map showing location are a site map showing location are a site map showing location are as a site part of the site compensate. Show the location of boundary sprear and/or Engaged Diaphragm and/or Engaged Site are are a site part of the strip AND a Permeable Berm are a soil map for site and area are as a site part of the site and area are as a site part of the site and area are as a site part of the site and area are as a site part of the site and area are as a site part of the site and area are as a site part of the site and area are as a site part of the site and area are as a site part of the site and area are as a site part of the site and area are as a site part of the site area.	ing the stormwate, and stating all as of this BMP and so, and receiving filt CDA) boundaries ed for in water quaders: ngineered Level of at the toe of the of facility	er area and acreage ality calculations Spreader at the top of a conserved open Spreader at the top of a vegetated filter filter area.
Provide soil boring logs with Unified S	ouis Ciassilicatioi	
II. COMPUTATIONS		
worksheets. Provide time of concentration (pre- all Provide a hydrograph generation (pre-	nd post-developed e- and post-developed	- and post-developed conditions), with d conditions), with worksheets. oped condition) for appropriate design and rational-critical storm duration method)

В.	Hydi	raulics Specify assumptions and coefficients used. Provide a stage-storage table and curve
		Show that compensatory devices are able to drain within 48 hours following a storm.
C. —	Wate	Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet) When soil amendments are used, the Runoff Reduction Spreadsheet will self-credit improved runoff volume reduction based on the change of the soil drainage characteristics (see Stormwater Design Specification No. 4)
III.	PLA	N REQUIREMENTS
A.	ВМР	Plan View Information (see example graphics in Design Specification No. 2) Show limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier. Show the layout and dimensions of the BMP(s) Maximum flow length = 150 ft. from adjacent pervious area OR 75 ft. from adjacent impervious area
		Show location of perimeter protection of Conserved Open Space(s) and note that no grading or heavy equipment access is allowed except for temporary disturbances associated with incidental utility construction, restoration operations, or management of nuisance vegetation
	1.	If Soils Are Amended Show the full length and width of any area of amended soils
	2.	Engineered Level Spreader Avoiding concentrated flows: Length of ELS lip = 13 lin. ft. per each 1 cfs of inflow (min. 13 lin. ft.; max 130 lin. ft.) for vegetated filter strips or for undisturbed conserved open space with at least 90% veg. cover (per Section 6.2 of the Design Specification) Length of ELS lip = 40 lin. ft. per 1 cfs for forested or reforested filter areas Overflow/bypass to a reinforced swale designed to convey all peak flows greater than the water quality design storm (1-inch rainfall)
	3.	Gravel Diaphragm Show the location, if applicable, at top of veg. filter area or conserv. open space slope
	4.	Permeable Berm Show the location, if applicable, at the toe of the vegetated filter area slope Show the location of the outlet pipe (or gravel lens with perforated pipe) through berm
В.	ВМР	Section Views & Related Details (see example graphics in Design Specification No. 2)
		Topographic conditions meet minimum slope and width requirements The first 10 ft. of filter must be 1-2% slope in all cases 0.5% - 3% slope for conserved open space or 1% - 4% slope for veg. filter strip = minimum 35 ft. filter width 3% -6% slope for conserved open space or 4% - 6% slope for veg. filter strip = minimum 50 ft. filter width 6% - 8% slope for veg. filter strip = minimum 65 ft. width

	1.	If Soils Are Amended Note the depth to which soil compost amendments must be incorporated
	2.	Engineered Level Spreader Avoiding concentrated flows: Length of ELS lip = 13 lin. ft. per each 1 cfs of inflow (min. 13 lin. ft.; max 130 lin. ft.) for veg. filter strips or for undisturbed conserved open space with at least 90% veg. cover (per Section 6.2 of the Design Specification) Length of ELS lip = 40 lin. ft. per 1 cfs for forested or reforested filter areas Overflow to reinforced swale if ELS designed for 1-in./hr. storm Section through the ELS system, including the forebay or ELS channel/trench located above the ELS, consistent with the Design Specification (No. 2) Detail showing any temporary or permanent biodegradable fabric or matting (EC-2, or EC-3) employed to stabilize steeper slopes Ends of ELS tied back into the natural slope to prevent scouring around the ends
	3.	Gravel Diaphragm Show a section through the gravel diaphragm, if used, at top of veg. filter area or conserv. open space slope, consistent with the Design Specification (No. 2) Filter fabric, stone and other materials should be consistent with the Design Spec
	4.	Permeable Berm Show a section through the permeable berm at toe of veg. filter area slope, consistent with the Design Specification (No. 2) Note the filter media composition and other materials, which should be consistent with the Design Specification
c .	Lar	There should be NO grading or clearing of native vegetation within conserved open space area; invasive species may be removed, if the locality approves Provide specifications for any compost amendments used and depth of incorporation (see Stormwater Design Specification No. 4) – soil amendments should NOT be incorporated until after the gravel diaphragm or level spreader are installed Ensure that planting specifications for the conserved open space or vegetated filter areas are consistent with the Stormwater Design Specification No. 2. Provide a planting schedule and specifications (transport / storage / installation / maintenance) Ensure that plant selection is appropriate for the site's vegetation climatic zone (4-8 in Virginia), emphasizing native vegetation Specify preservation measures for existing vegetation Ensure that topsoil / planting soil is included in the final grading The construction contract should include a Care and Replacement Warranty to ensure that new vegetation is properly established and survives during the first growing season following construction.
D.	Co	nstruction Notes Construction sequence for BMP(s) and E&S controls: The filter area should be clearly marked off before construction begins to prevent construction traffic from compacting the area Install applicable temporary E&S control measures. Convey base flow around secondary practice while it is being constructed. Install temporary and permanent stabilization measures.

	In addition:
1. 	Perimeter of Conserved Open Space should be protected by acceptable signage, super silfence, snow fence, chain link fence, orange safety fence or other comparable methods Note that no clearing, grading or heavy equipment access is allowed except for temporary disturbances associated with incidental utility construction, restoration operations of management of nuisance vegetation Note (if applicable) that (1) construction of the gravel diaphragm or engineered level spreade shall not commence until the contributing drainage area has been stabilized and perimeter E&S controls have been removed and cleaned out; and (2) stormwater should not be diverted into the filter area until the gravel diaphragm and/or level spreader are installed and stabilized. Note that any light grading necessary at the filter area boundary must be done with tracked vehicles to prevent compaction
2.	Note that only vehicular traffic necessary for the filter strip construction should be allowed within 10 feet of the filter strip boundary Note that if existing topsoil is stripped during grading, it shall be stockpiled and stabilized for later use Note that construction runoff shall be directed away from the proposed filter strip area, using perimeter silt fence or, preferably, a diversion dike. Note (if applicable) that (1) construction of the gravel diaphragm or engineered level spreade shall not commence until the contributing drainage area has been stabilized and perimeter E&S controls have been removed and cleaned out; and (2) stormwater should not be diverted into the filter area until the gravel diaphragm and/or level spreader are installed and stabilized and until the turf cover is dense and well-established. Note that amended soils should be hand-raked to the most level slope without using heave equipment, but that any light grading necessary to achieve desired elevations and slopes must be done with tracked vehicles to prevent compaction. Note that compost amendments and/or topsoil shall be incorporated evenly across the filter strip area, stabilized with seed, and, if slopes exceed 3%, protected by biodegradable E&S contromatting or blankets (EC-2).
E	Maintenance Items (can include BMP Operation & Maintenance Inspection Checklists from Chapter 9, Appendix 9-C of this Handbook) Provide a Maintenance Agreement, indicating the person or organization responsible for maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist. Include a Maintenance Narrative which describes the long-term maintenance or requirements of the facility and all components, including installation/maintenance or signage; removal and disposal of trash, debris and sediment accumulations; and mowing. Record a deed restriction, drainage easement, and/or other enforceable mechanism, including GPS coordinates of the area, to ensure property owner awareness, access for inspections and maintenance, and that the filter area is remains intact and fully functional. Provide sufficient facility access from the public ROW or roadway to both the filter area and accessory practices.

IV. COMMENTS		
	By:	Date:

8-A.4.0. GRASS CHANNELS: DESIGN CHECKLIST

	Submission Date		
	ect Name		
Drag	Plan/Permit Numberctice No./Location on Site		
	ner		
	P Designer		Phone Number
Gen	neral Contractor		Phone Number
	Signature and stamp of li certification	censed profess	ional design consultant and owner
Plar	n Status		
	Approved Not Approved	Legend:	Inc Complete Inc Incomplete/Incorrect N/A - Not Applicable
Тур	e of pretreatment facility:		
	☐ Check Dams (channel flow)		
	☐ Tree Check Dams (channel flow)		
	☐ Grass Filter Strip (sheet flow)		
	☐ Gravel or Stone Diaphragm (sheet	flow)	
	☐ Gravel or Stone Flow Spreaders (c	•	
	□ Other:		
	□ None		
	this practice fits into the overall p basin, infiltration trench, etc.). Provide a site map of the location Grass channel area and p Contributing drainage are any individual grass chan Topography Areas of the site compenency of the solid boring logs with Unifile Pre-treatment is recommended for down runoff velocity. Minimum depth to bedrock in kars Minimum depth to groundwater in In areas of steep terrain, terracin 5% to 10% grade, where the drop inches and the check dams shou	olan, and stating all of this BMP showing per-treatment practices (CDA) boundaring asted for in water questions of the grass chartest areas is 18 inches a coastal areas is 12 and a series of grass p in elevation between	ice es and acreage, not to exceed 5 acres for uality calculations nnel ions o dissipate energy, trap sediments and slow s.
II.	to prevent erosion. COMPUTATIONS		
A .	Hydrology Provide runoff curve number worksheets. Provide time of concentration (pre		re- and post-developed conditions), with ped conditions), with worksheets.

	Provide hydrograph generation (pre- and post-developed condition) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method)
B.	Hydraulics Show that compensatory devices are able to drain within 48 hours following a storm. Grass channels are designed based on peak flow rate – the maximum flow velocity of the channel must be less than 1 foot per second during a 1-inch water quality storm event The longitudinal slope of the channel should, ideally, be between 1% and 2% in order to avoid scour and short-circuiting within the channel; longitudinal slopes up to 4% are acceptable, but check dams will be necessary to reduce the effective slope in order to meet the limiting velocity requirements) Verify hydraulic capacity using Manning's Equation or an accepted equivalent method, such as erodibility factors and vegetal retardance
	The flow depth for the peak treatment volume (1-inch rainfall) should be maintained at 3 inches or less Manning's "n" value for grass channels should be 0.2 for flow depths up to 4 inches, decreasing to 0.03 at a depth of 12 inches (which applies to the 2-year and 10-year storms if an on-line application Peak flow rates for the 2-year and 10-year frequency storms must be non-erosive or subject to site-specific analysis of the channel lining material and vegetation The 10-year peak flow rate must be contained within the channel banks, with a minimum of 6 inches of freeboard Specify assumptions and coefficients used. Provide a stage-storage table and curve Calculations for peak flow depth and velocity should reflect any increase in flow along the length of the channel, as appropriate. If a single flow is used, the flow at the outlet should be used. The hydraulic residence time should be a minimum of 9 minutes for the treatment volume (1-inch rainfall) design storm. If flow enters the channel at multiple locations, a 9-minute minimum hydraulic residence time should be demonstrated for each entry point, using equations in Stormwater Design Specification No. 3. The minimum length may be achieved with multiple swale segments connected by culverts with energy dissipators
C .	Water Quality Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet) When soil amendments are used, the Runoff Reduction Spreadsheet will self-credit improved runoff volume reduction based on the change of the soil drainage characteristics (see Stormwater Design Specification No. 4) Specific sizing/dimensions determined from criteria in Stormwater Design Specification No. 3. Grass channels should NOT be used as stand-alone water quality treatment systems in Coastal Plain settings, due to poor nutrient and bacteria removal rates (Dry Swales or Wet Swales are a better choice).
	PLAN REQUIREMENTS BMP Plan View Information (see example graphics in Design Specification No. 2) Show the limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier. Layout and dimensions of the grass channel and pre-treatment device(s) The bottom width of the channel should be from 4 to 8 feet. If a channel must be wider, incorporate benches, check dams, level spreaders or multi-level cross-sections to prevent braiding and erosion along the channel bottom. Grass channels should generally be aligned adjacent to and the same length (minimum) as the contributing drainage area identified for treatment.

-	In karst areas, the channel may have off-line cells and must be connected to an adequate discharge point. In coastal areas, the channel may have off-line cells and must be connected to the ditch system.
	,
B	BMP Section Views & Related Details (see example graphics in Design Specification No. 2) Topographic conditions must meet minimum slope and width requirements. Grass channels should be designed with a trapezoidal or parabolic cross-section. A parabolic shape is preferred for aesthetic, maintenance and hydraulic reasons. The channel side slopes should be 3H:1V or flatter. For ease of mowing and routine maintenance, side slopes should be no steeper than 4H:1V. Flatter slopes are encouraged to aid in pre-treatment of sheet flows entering the channel. The longitudinal slope of the channel should, ideally, be between 1% and 2% in order to avoid scour and short-circuiting within the channel; Longitudinal slopes up to 4% are acceptable, but check dams will be necessary to reduce the effective slope in order to meet the limiting velocity
	requirements). A minimum slope of 0.5% must be maintained in karst or coastal areas to ensure positive drainage.
C.	Check Dams (generally discouraged in karst areas, where flow spreaders flush with the ground surface and spaced along the channel length may be useful in spreading flows more evenly across the channel width)
	Check dams should be should configured with elevated driveway culverts or be composed of wood, concrete, rip-rap, or other non-erodible material, underlain with filter fabric conforming to the following standards: Needled, non-woven, polypropylene geotextile.
	Grab Tensile Strength (ASTM D4632): ∃ 120 lbs.
	Mullen Burst Strength (ASTM D3786): ∃ 225 lbs./sq. in.
	Flow Rate (ASTM D4491): ∃ 125 gpm/sq. ft.
	Apparent Opening Size (ASTM D4751): ∃ US #70 or #80 sieve
	Wood used for check dams should consist of pressure-treated logs or timbers, or water-resistant tree species such as cedar, hemlock, swamp oak or locust.
	It is necessary to compute check dam materials, based on the surface area and depth used in the design computations.
	Check dams should be spaced (based on the channel slope) as needed to increase residence time and provide adequate storage for the treatment volume (1-inch rainfall) or any additional volume attenuation requirements. The ponded water at a downhill check dam should not touch the toe of the upstream check dam.
	The maximum desired check dam height is 12 inches (for maintenance purposes). However, for challenging sites, a maximum of 18 inches can be allowed, with additional design elements to ensure the stability of the check dam and the adjacent and underlying soils The average ponding depth throughout the channel should be 12 inches.
	Soil plugs serve to help minimize the potential for blow-out of the soil media underneath the check dams due to hydrostatic pressure from the upstream ponding. Soil plugs are appropriate for Grass Channels (1) on slopes of 4% or greater, or (2) with check dams equal to or greater than 12-inches in height.
	Armoring may be needed at the downstream toe of the check dam to prevent erosion. Check dams must be firmly anchored into the side-slopes to prevent outflanking; check dams must also be anchored into the channel bottom so as to prevent hydrostatic head from pushing out the underlying soils.
	Check dams must be designed with a center weir sized to pass the channel design storm peak
	flow (10-year storm event for man-made channels). Check dams should be designed and constructed so as to facilitate easy mowing of the channel. Each check dam should have a weep hole or similar drainage feature so it can dewater after
	storms. Individual channel segments formed by check dams or driveways should generally be at least 25 to 40 feet in length.

D.	Diaphragms
	Pea gravel used to construct pre-treatment diaphragms should consist of washed, open-graded, course aggregate between 3 and 10 mm in diameter and must conform to local design standards.
F	Soil Compost Amendments
	The compost-amended strip should extend over the length and width of the channel bottom, and
	the compost should be incorporated to a depth as outlined in Stormwater Design Specification
	No. 4.
	The amended area will need to be rapidly stabilized with perennial, salt tolerant grass species.
	For grass channels on steep slopes, it may be necessary to install a protective biodegradable geotextile fabric to protect the compost-amended soils. Care must be taken to consider the
	erosive characteristics of the amended soils when selecting an appropriate geotextile. For redevelopment or retrofit applications, the final elevation of the grass channel (following compost amendment) must be verified as meeting the original design hydraulic capacity.
	compost amendment) must be verified as meeting the original design hydraulic capacity.
F.	Landscape Plan
•	Choose grass species that can withstand both wet and dry periods as well as relatively high-
	velocity flows. Taller and denser grasses are preferable, though the species is less important than the ability to provide effective stabilization. (Consult Standard and Specification 3.32 of the Virginia E&S Control Handbook for a list of acceptable grass species.)
	For channels adjacent to roads and parking lots, salt-tolerant species should be chosen.
	Use grass seed, NOT sod.
	Seed at a density that achieves a 90% turf cover by the end of the second growing season.
	Provide specifications for any compost amendments used, including the depth of incorporation
	(see Stormwater Design Specification No. 4)
	Provide immediate stabilization of the channel bed and banks using a biodegradable erosion
	control fabric (netting or mats) durable enough to last at least two growing seasons (conforming
	to Standard and Specification 3.36 of the Virginia E&S Control Handbook).
	Provide a planting schedule and specifications (transport / storage / installation / maintenance) Ensure that plant selection is appropriate for the site's vegetation climatic zone (4-8 in Virginia),
	emphasizing native species
	Specify preservation measures for existing vegetation
	Ensure that topsoil / planting soil is included in the final grading
	The construction contract should include a Care and Replacement Warranty to ensure that new
	vegetation is properly established and survives during the first growing season following construction.
G	Construction Notes
	Ideally, grass channels should be constructed during months that are best for establishing turf
	cover without irrigation (February 15 – April 15; September 15 – November 15).
	Applicable temporary E&S control measures
	Ideally, grass channels should remain outside the limit of disturbance during construction to
	prevent soil compaction by heavy equipment. If this is not feasible, temporary E&S controls such
	as dikes, silt fences and similar measures should be integrated into the channel design.
	Specifically, barriers should be installed at key check dam locations, and E&S control fabric
	should be used to protect the channel bottom.
	Grass channel construction should begin only after the entire contributing drainage area has
	been stabilized with vegetation. Sediment accumulation must be removed during final grading to
	achieve the design cross-section.
	Stormwater flows should be bypassed and not allowed into the grass channel until the bottom
	and side slopes are stabilized.
	Construction sequence for BMP(s) and E&S controls:
	Grade the channel to the final dimensions shown on the plan.

L M	the plan Fill material used to construct the che compacted to prevent settlement. The level at the design elevation. (Optional) Till the bottom of the charamendments according to Stormwate Add soil amendments as needed, hypeg in erosion control fabric or biodegradable E&S control fabric Specification 3.36 of the VESCH. Prepare planting holes for any trees landscaping plan and water them were	dro-seed the bottom and banks of the channel, and blanket where needed. After initial planting, a should be used, conforming to Standard and and shrubs, then plant materials as shown in the
	hapter 9, Appendix 9-C of this Handbook) Provide a Maintenance Agreement, indicar maintenance, authorizing access for inspection inspection checklist. Include a Maintenance Narrative requirements for the grass channels disposal of trash, debris and sedimental Record a deed restriction, drainage easemental GPS coordinates of the area, to ensure proposition maintenance, and that the grass channels remaintenance.	ting the person or organization responsible for one and maintenance, and including a maintenance which describes the long-term maintenance and all their components, including removal and accumulations; and mowing. nt, and/or other enforceable mechanism, including terty owner awareness, access for inspections and
IV. C	OMMENTS	
	Ву:	Date:

8-A.5.0. SOIL COMPOST AMENDMENTS: DESIGN CHECKLIST

Plan Submission Date		
Project Name		
Site Plan/Permit Number		
Practice No./Location on Site		
Owner		Phone Number
BMP Designer		Phone Number
General Contractor		Phone Number
Signature and stamp certification	of licensed profession	onal design consultant and owner
Plan Status		
Approved	Legend:	Complete
Not Approved		Inc Incomplete/IncorrectN/A - Not Applicable
I. SUPPORTING INFORMATION		
Provide a concise narrative this practice fits into the own basin, infiltration trench, etc. Provide a site map show applied Show the contributing drain any individual Grass Chanter Provide topography of the series Provide a soil map for site. Provide two soil tests (presproposed amendment area First test done evenutrients (to determ Second test done organic matter adjucton construction inspectively show the areas of the site. The following are site cond Existing soils have needed were B-soid The water table or The slope exceeds Existing soils are second Incorporation of colline. The downhill slope The contributing im The area under contributing im The area under contribution In karst areas, enserted.	rerall plan, and stating all as c.). ing location of area(s) who mage area (CDA) boundaries and area of soil amendment are need for plant at the soil amendment are mass-graded, in order and soil amendment are soil amendment are massible are massible are massible are assonally wet ampost would harm tree room are runs toward an existing or a pervious surface area excensions are soil amendment are soil are soil amendment are soil amendment are room are soil amendment	soil properties to a depth 1 foot below the nents have been incorporated): e bulk density, porosity, pH, salts, and soil blems and what amendments are needed) utritional requirements, pH, adjustment, or t growth (done in conjunction with the final soiling has achieved design depths). Insulative calculations Immendments should NOT be used: E A and B), although amendments may be er to maintain the runoff reduction rate. If the soil surface eded on slopes between 5% and 10% Its (keep amendments outside the tree drip proposed building foundation. Eeds the surface are of the amended soils. It is needed to conform to the pre-existing
In coastal areas, of		ald be a minimum of 2 feet to ensure the

II. COMPUTATIONS

A. 	Hydrology Provide runoff curve number determinations (pre- and post-developed conditions), with worksheets. Provide time of concentration (pre- and post-developed conditions), with worksheets. Provide hydrograph generation (pre- and post-developed conditions) for appropriate design and
	safety storms (USDA-NRCS methods or modified rational-critical storm duration method)
B.	Hydraulics Specify assumptions and coefficients used. Provide a stage-storage table and curve
C.	Water Quality Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet) When soil amendments are used, the Runoff Reduction Spreadsheet will self-credit improved runoff volume reduction based on the change of the soil drainage characteristics (see Stormwater Design Specification No. 4)
III.	PLAN REQUIREMENTS
A.	BMP Plan View Information (see example graphics in Design Specification No. 2) Show the limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier. Show the layout and dimensions of the soil amendment area Topographic conditions must meet minimum slope requirements
B	Landscape Plan Use grass seed, NOT sod. Seed at a density that achieves a 90% turf cover by the end of the second growing season. Provide material specifications for any compost amendments used, including the depth of incorporation (see Stormwater Design Specification No. 4) Provide a planting schedule and specifications (transport / storage / installation / maintenance) Ensure that plant selection is appropriate for the site's vegetation climatic zone (4-8 in Virginia), emphasizing native species Specify preservation measures for existing vegetation Ensure that topsoil / planting soil is included in the final grading The construction contract should include a Care and Replacement Warranty to ensure that new vegetation is properly established and survives during the first growing season following construction.
C .	 Construction Notes For rooftop disconnection, vegetative filter strip or grass channel applications, see the checklists for those practices. For larger, more expansive areas, the following criteria apply: ldeally, the soil amendment area should remain outside the limit of disturbance during construction to prevent soil compaction by heavy equipment. Prior to construction, the proposed soil amendment area should be deep-tilled to a depth of 2 to 3 feet using a tractor and subsoiler with two deep shanks (curved metal bars) to create rips perpendicular to the direction of flow. A second deep tilling to a depth of 12-18 inches is needed after final building lots have been graded. It is important to have dry conditions at the site prior to incorporating compost. Incorporate the acceptable compost mix into the soil using a rototiller or similar equipment at the volumetric rate of 1 part compost to 2 parts soil.

	Lime and/or irrigation may be needed Areas of compost amendments exc	r sod used to establish a vigorous grass cover. initially to help the grass grow quickly. eeding 2500 sq. ft. should employ simple E&S, to reduce the potential for erosion and to trap
D.	. Maintenance Items (can include BMP Operation Chapter 9, Appendix 9-C of this Handbook)	on & Maintenance Inspection Checklists from
	If the soil amendment area exceeds 10,000 Agreement, indicating person or organization for inspections and maintenance, and includin Record a deed restriction or other enforceab area, to ensure the infiltrating areas are not dis To educate the property owner, provide a mai and long-term maintenance requirements.	le mechanism, including GPS coordinates of the
IV.	. COMMENTS	
		•
	Ву:	Date:

8-A.6.0. VEGETATED ROOF: DESIGN CHECKLIST

Plan Submission Date	
Project Name	
Site Plan/Permit Number	
Practice No./Location on Site	
Owner	Phone Number
BMP Designer	Phone Number
General Contractor	Phone Number
Signature and stamp of licensed profess certification	sional design consultant and owner
Plan Status	
Approved Legend:	Complete
Not Approved	Inc Incomplete/Incorrect - Not Applicable
Facility Type: Level 1 Level	el 2
Provide a concise narrative describing the stormwate practice fits into the overall plan, and stating all assurinfiltration trench, etc.). Show the location of the BMP roof on the site map. A structural engineer, architect or other qualified profesensure that the building has enough structural capacity held in the planting media (typical fully saturated extellos./sq. ft.). Adequate access to the roof must be provided to de perform routine maintenance. The roof hatch or trap does a minimum dimension of 24 inches. Vegetated roofs can be applied to most roof surfaces Certain roof materials, such as exposed treated we appropriate decks for vegetated roofs. Vegetated roof designs should comply with the Virginia to roof drains and emergency everflow devices.	essional should be involved with the design to the ty to support the additional weight of the water tensive vegetated roof loads range from 15-25 aliver and stockpile construction materials and for should be not less than 16 sq. ft. in area with sq. although concrete roof decks are preferred and uncoated galvanized metal, are not of the stockpile of the systems.
to roof drains and emergency overflow devices. Vegetated roofs can be used as retrofits, based on accessibility, as well as the owner's ability to provide ne Special design adaptations: In karst areas, direct the roof downspout discharminimize the risk of sinkhole formation In coastal areas, designers should choose plant In cold climates, it is important to match the plant	ecessary maintenance. arges at least 15 feet away from the building to t materials that tolerate drought and salt spray. Int materials to the plant hardiness zone, design
the roof so the growing media is not subject structural capacity to account for winter snow lo Where acid rain falls, growing media can neuton clear whether the acid rain will impair plant grow	pads. tralize the pH of the rainfall; however, it is not

I. COMPUTATIONS

Α.	 Hydrology Determine the runoff curve number (pre-development and post-development conditions), providing the worksheets; post-development recommendations for 4 design storm events are provided in Table 5.1 of Stormwater Design Specification No. 5. Determine the time of concentration (pre- and post-developed conditions), providing the worksheets. Generate hydrographs (pre- and post-developed conditions) for appropriate design and safety storms
	(USDA-NRCS methods or modified rational-critical storm duration method), providing the results.
В.	Hydraulics The drainage layer below the growing media should be designed to convey the 10-year storm without backing up water into the growing media, conveying the flow to an outlet or overflow system such as a traditional rooftop drainage system with inlets set slightly above the elevation of the vegetated roof surface. Specify assumptions and coefficients used. Provide a stage-storage table and curve.
C.	 Water Quality Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet)
III.	PLAN REQUIREMENTS
Α.	BMP Plan View Information (see example graphics in Design Specification No. 2) Layout and dimensions of the vegetated roof.
	A 2-foot wide vegetation-free zone is recommended along the perimeter of the roof (may be a 1-foot setback for very small vegetated roof applications), with a 1-foot vegetation-free zone around all roof penetrations, to act as a firebreak. The roof design should include strategically located non-vegetated walkways (e.g., permeable paver blocks) to allow for easy access to the roof for weeding and making spot repairs. Size (surface area) to address the required treatment volume per equation in Stormwater Design Specification #5 or per manufacturer recommendations. Show the layout of the outlet or overflow system and locations of roof drains
В.	BMP Section Views & Related Details (see example graphics in Design Specification No. 2)
	Vegetated roofs are composed of up to 8 different systems or layers, which may consist of a wide variety of materials and differ in cost, performance and structural load. Proprietary designs are available. The entire system must be assessed to meet the design requirements (see Stormwater Design Specification No. 5). Roof drains immediately adjacent to the growing media should be boxed and protected by flashing extending at least 3 inches above the growing media, to prevent clogging.
C.	Planting Plan
	The planting plan must be prepared by a landscape architect, botanist or other professional
	experienced with vegetated roofs. Plant materials are selected based on local climate (plant hardiness zone) and design objectives, as well as toleration of the difficult growing conditions on building rooftops. Selected plants should be fire-resistant and able to withstand heat, cold and high winds; the primary groundcover for most vegetated roof installations is a hardy, low-growing succulent such as Sedum, Delosperma, Talinum, Semperivum, or Hieracium. Plant choices can be much more diverse for deeper intensive vegetated
	roof systems.

	The species selection and planting plan layout should reflect the building location in terms exposure to wind, snow loading, heat stress, sun orientation, and shading by trees or buildings. Note: Most effective vegetated roof plant species will <i>NOT</i> be native to Vin Chesapeake Bay watershed.	surrounding
	Species should also be selected to match the expected rooting depth of the growing media	t.
	Accent plants may be included to provide seasonal diversity and color.	
	Due to limited vegetated roof plant nurseries in the region, designers should order plant m	aterials 6-12
	months prior to the expected planting date and to have the plants contract-grown.	
	The planting period extends from spring to early fall, but it is important to allow plants en	ough time to
	root thoroughly prior to the first killing frost.	
	Typically, most vegetated roofs will not require supplemental irrigation, except for tempor	ary irrigation
	during dry months as the roof vegetation becomes established.	
	Plants can be established using cuttings, plugs, mats and, more rarely, seedlings or containing plants also provide mate rolls or proprietory roof planting modules.	amers, some
	vendors also provide mats, rolls, or proprietary roof planting modules. Initial fertilization may be needed to support growth, using a slow-release fertilizer with min	orale
	Initial refullzation may be needed to support growth, using a slow-release refullzer with min Hand weeding must be performed regularly during the first 2 years.	erais.
	The construction contract should include a Care and Replacement Warranty that specifies	a minimum
	survival for species planted of 75% after the first growing season, and a minimum effe	
	cover of 75% for flat roofs and 90% for pitched roofs.	olivo grodina
	cover of 7070 for hacroole and 6070 for phones recte.	
D.	Construction Notes	
	An experienced installer should be retained to construct the vegetated roof system.	
	The roof system should be constructed in sections to facilitate easier inspection and mainton	enance.
	Construction sequence:	
	Construct the roof deck with the appropriate slope and material.	
	Install the waterproofing method according to the manufacturer's specifications.	
	Conduct a flood test to ensure the system is water-tight, by placing 2 inches of water-tight, by placing 3 inches of water-tight, by	ater over the
	membrane for 48 hours.	
	Add the additional system components, taking care not to damage the waterproofi	
	Drain collars and protective flashing should be installed to ensure free flow	v or excess
	stormwater.	
	The growing media should be mixed prior to delivery to the site.	il planting to
	The media should be spread evenly over the filter fabric surface and covered unt	i pianting, to
	prevent weeds from growing. Sheets of exterior-grade plywood can be laid over the growing media to accomm	adata faat ar
	wheelbarrow traffic (however, limit this traffic to reduce compaction).	Juale 1001 01
	Moisten the growing media prior to planting.	
	Plant the vegetation in accordance with the planting plan of ASTM E2400.	
	Water the plants immediately after planting and routinely during the establishmen	t period and.
	especially, during the first summer (generally 12-18 months for full establishment).	
	,	
E.	Maintenance Items (can include BMP Operation & Maintenance Inspection Checklists fr	om Chapter
	9, Appendix 9-C of this Handbook)	
	Provide a Maintenance Agreement, indicating the person or organization responsible for n	
	authorizing access for inspections and maintenance, and including a maintenance inspecti	
	Include a Maintenance Narrative which describes the long-term maintenance req	uirements of
	the facility and all components.	
	Record a deed restriction or other enforceable mechanism, including GPS coordinates of	
	ensure the the vegetated roof is not converted to a conventional roof surface (in order to	maintain this
	component of the site's stormwater management plan).	
	Avoid the use of herbicides, insecticides and fungicides, because their presence of	
	deterioration of the waterproof membrane and contaminate runoff discharged from the roof Avoid power-washing so that the cleaning agents do not harm the rooftop plant communities	
	Avoid power-washing so that the dealing agents do not harm the roomop plant community	<i>5</i> 0.

IV. COMMENIS		
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	By:	Date:

8-A.7.0. RAINWATER HARVESTING: DESIGN CHECKLIST

	ate		
Project Name			
Site Plan/Permit N	umber		
Owner	on on Site		Phone Number
			Phone Number Phone Number
	·		
Concrai Contracto			
Signatu certifica	-	nsed profession	onal design consultant and owner
Plan Status		Legend:	🗓 Complete
Approved		3	Inc Incomplete/Incorrect
Not Appro			N/A - Not Applicable
0 1 5145			
•	ed with Rainwater Harvest	_	
·	connection (No. 1)	L	Storage and release in Foundation
	o Veg Filter/Open Space		Planter (No. 9, Appendix A)
(No. 2)			Dry Swale (No. 10)
Grass Chan	nel (No. 3)		Underground infiltration soak-away pit
☐ Infiltration (N	lo. 8)		Other:
☐ Micro-Bioret	ention (rain garden) (No. 9)	
this pract purpose for purpose	ice fits into the overall place or which the harvested rail butdoor non-potable uses, adoor, non-potable uses, uilding code and health egulatory approvals are obtained on the properties of rainwater as a resount in the infiltration to promote good and the infiltration to promote good and the infiltration of the infiltration of the infiltration of BMP on the security of the infiltration of the infiltrati	an, and stating all nwater will be used including irrigation, such as toilet fludepartment regulationed. Cluding food prepand health departovals are obtained irce to meet on-site iroundwater rechard only due to reduct alized due to reduct alized due to reduct considered during it is sufficient details to the made of site of or efficient roof in water will have point the roofing mat	ushing, fire suppression, etc., assuming ations allow such uses and appropriate paration, drinking water, showers, etc., atment regulations allow such uses and a demand (above) or design in conjunction a demand (above) or design in conjunction and a demand (above) or design in conjunction are devolume of runoff leaving the site) are space is needed to house the tank and anitial design and site layout). In dentified prior to determining the final tank at the construct the six primary components of anooth, non-porous material with efficient

	Some industrial roof surfaces may be designated as "hot spots," limiting the use
Collec tank)	and benefits of harvesting the rainwater. tion and conveyance system (e.g., gutters, downspouts and pipes to the stroage
	Runoff should be routed from rooftops to cisterns in closed roof drain systems or storm drain pipes, avoiding surface drainage which could increase contamination of the water
	_ Aluminum, round-bottom gutters and round downspouts are generally recommended.
	Gutter slopes should be 0.5% for 2/3 of the length and 1% for the remaining 1/3. Gutters should be sized to contain the 1-inch rainfall event (treatment volume) at a rate of 1 inch/hour.
	If volume control credit is desired for channel protection and flood protection purposes, gutters should be sized to convey 1-year and 10-year design storms. Pipes connecting the downspouts to the storage tank should have a minimum
Pre-so	slope of 1.5% and be sized to convey the intended design storm. creening and first flush diverter (filters out sediment, leaves, contaminants and
<u>———</u>	Pre-filtration devices that filter out large debris should be low-maintenance or maintenance free (e.g., leaf screens, gutter guards, etc.)
_	For larger tank systems, the initial first flush (0.02 – 0.06 inches of rooftop runoff) must be diverted from the tank and directed to an acceptable non-erodible pervious flow path or secondary BMP for infiltration (preferably the same practice that receives tank overflows).
	A 95% filter efficiency (including the first flush diversion) must be achieved for the 1-inch rainfall event. For the 1-year and 10-year design storms, the filtering must have a minimum efficiency of 90%.
	If leaf screens are used, note in the maintenance agreement that they must be cleaned regularly to be effective and maintain flow from the gutters into the storage tank.
	If a roof washer tank is used just ahead of the storage tank, note in the maintenance agreement that they must be cleaned regularly to be effective. A first flush diverter , which filters out small contaminants such as dust, pollen and animal feces, require the ability to actively drain the first flush water volume to a pervious area (filter path) following each rainstorm (this is the preferred pretreatment method if the harvested water is intended for indoor uses). A vortex filter can be used to filter rooftop rainwater for larger rooftop areas.
Storag	ge tank
	The tank volume must be calculated to meet the water demand and the stormwater treatment volume credit objectives. Dead storage below the outlet to the distribution system and an air gap at the top of the tank should be added to the total volume. For gravity-fed systems, a minimum of 6 inches of dead storage should be provided. For systems using a pump, the dead storage depth is be based on the pump specifications. The system should be sealed using a water-safe, non-toxic substance.
	Storage tanks should be opaque or otherwise protected from direct sunlight to inhibit algae growth and should be screened to inhibit mosquito breeding and reproduction.
	The relationship of tank location to site topography should be considered as they relate to all inlet and outlet invert elevations in the system and to the amount of pumping that may be needed. The total elevation drop will be realized beginning from the downspout leaders to the final mechanism receiving gravity-fed discharge and/or overflow from the cistern. Storage tanks should be placed on native soils or on fill in accordance with the manufacturer's guidelines.

	The soil pH must be considered in relation to the material of which the tank/cistern is made.
	Storage tanks should be designed to be watertight to prevent water damage when placed near building foundations.
	Rainfall pH must also be considered (Virginia rain tends to be acidic, from 4.5
	5.0), due to the risk of leaching metals form the roof surface, tank lining or water
	laterals to interior connections. Limestone or other neutralizing substances ma be added in the tank to buffer acidity.
_	Underground storage tanks are most appropriate in areas where the tank ca
	be buried <i>above</i> the water table and in a manner that it will not be subject to flooding. If buried <i>below</i> the water table, special design features must be employed to prevent the tank from "floating," etc.
	Underground systems should be placed in areas without vehicle traffic and
	designed to support the overlying sediment and other anticipated loads, of otherwise be designed to support live loads from heavy trucks (this may
	increase construction costs). Underground systems should have a standard size manhole or equivaler
	opening to allow access for cleaning, inspection, and maintenance purposes
	The opening must be able to be locked or otherwise secured to prever
	unwanted access. Distribution system
	The system should be equipped with an appropriately sized pump that produce
	sufficient pressure for all end-uses.
	The typical pump and pressure tank arrangement consists of a multi-stage centrifugal pump that draws water from the storage tank and sends it to
	pressure tank, where it is stored for distribution.
	The municipal code may require the separate plumbing to be labeled as non
	potable Any hookup to a municipal backup water supply must have a backflow
	prevention device, subject to local codes, to keep municipal water separate from stored rainwater. This may include incorporating an air gap to separate the
	two supplies.
	Distribution lines must be buried beneath the frost line. If above-ground outdoor pipes are installed, they must be insulated or heat-wrapped to prevent freezing
	and ensure uninterrupted operation during the winter.
	Distribution lines to the building must have shut-off valves that are accessible when snow cover is present.
	A drain plug or cleanout sump, draining to a pervious area, must be installed to
	allow the system to be completely emptied.
	Overflow, filter path or secondary runoff reduction practice(s)
	An overflow mechanism must be included in the system design to handle an individual storm event or multiple events in succession that exeed the capacit
	of the storage tank.
	Overflow pipes must have a capacity equal to or grater than the inflow pipe(s and have a diameter and slope sufficient to drain the storage tank while
	maintaining an adequate freeboard height.
	Overflow pipes must be screened to prevent access to the tank by rodents and birds.
	The filter path should be a pervious or grass corridor that extends from the
	overflow to the next runoff reduction practice, the street, an adequate existing or
	proposed channel, or the storm drain system. The filter path must be graded with a slope that results in sheet flow conditions.
	If compacted or impermeable soils are present along the filter path, compose amendments may be necessary (see Stormwater Design Specification #4).

II. COMPUTATIONS

A.	Hydrology
	The contributing drainage area is the impervious area draining to the tank, generally only the rooftop surface. Paved surfaces can be included in rare circumstances with appropriate treatment.
	Determine the time of concentration (pre- and post-developed conditions), providing the worksheets.
	Generate hydrographs (re- and post-developed conditions) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method)
	Hydraulics The required hydraulic head depends upon the ultimate use/destination of the harvested water. Specify the assumptions and coefficients used. Provide a stage-storage table and curve. Show that compensatory devices are able to drain within 48 hours following a storm.
C.	 Water Quality Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA
	The Cistern Design Spreadsheet (explanation and instructions provided in Stormwater Design Specification No. 6) must be used to determine cistern sizing, including the treatment volume requirements, and by extension, pollutant load removal (provide a copy of the spreadsheet calculations)
	IMPORTANT NOTE: In order to adequately address the required design treatment volume, the design specification assumes the practice will achieve a dedicated year-round drawdown. While seasonal uses (such as warm weather irrigation, etc.) may be incorporated into the site design, they are not considered to contribute to the treatment volume credit (for stormwater management purposes) unless a drawdown at an equal or greater rate is also realized during non-seasonal periods (e.g., infiltration during non-irrigation months, etc.). Designing for constant drawdown of the stored water is also important in assuring that the tank will have sufficient storage capacity for future rainstorms.
III.	PLAN REQUIREMENTS
A	BMP Plan View Information (see example graphics in Design Specification No. 2) Show the layout and dimensions of the rainwater harvesting system. In general, underground tanks should be set at least 10 feet from any building foundation. Cistern overflow devices should be designed to avoid causing ponding or soil saturation within 10 feet of building foundations. The roof design should include strategically located non-vegetated walkways (e.g., permeable paver blocks) to allow for easy access to the roof for weeding and making spot repairs. Ensure sizing (surface area) sufficient to address the required treatment volume consistent with the equation in Stormwater Design Specification No. 5 or manufacturer recommendations. Show the layout of the outlet or overflow system and locations of roof drains
В.	BMP Section Views & Related Details (see example graphics in Design Specification No. 2) Show sections through the system and, as appropriate, through system components
C.	Planting Plan Provide a planting schedule and specifications (transport / storage / installation / maintenance) Ensure plant selection appropriate for the site's vegetation climatic zone (4-8 in Virginia)

	The construction contract should include a <i>Care and Re</i> vegetation is properly established and survives during construction.	
D	D. Construction Notes It is advisable that a single contractor, with a plumble harvesting system sizing, installation and placement, i outdoor irrigation system, and secondary runoff reduction. The tank location must be identified on the site and the tank location must be identified on the site and the tank location must be installed on the site and the tank location must be routed to pre-screed. The pre-treatment system must be installed. Mosquito screens must be installed on all openings. The overflow device must be installed and directed, as since the catchment area and overflow area must be stabilized. The secondary runoff reduction practice(s) must be installed.	nstall the rainwater harvesting system practices. ank installed. ening devices and first flush diverters. hown on the plans. d.
E	E. Maintenance Items (can include BMP Operation & Main Chapter 9, Appendix 9-C of this Handbook) Provide a Maintenance Agreement, indicating the p maintenance, authorizing access for inspections and mainspection checklist. Include a maintenance narrative describing the owner's primary responsibilities for long-term components, require the owner to pay to have specified schedule, and authorize the qualifying property for inspection or corrective action in the Record a drainage easement to allow for inspection as include the tank, the filter path, and any secondary runof Provide sufficient facility access from public ROW of maintenance. If the system is located on a private residential lot, its extended of record.	erson or organization responsible for intenance, and including a maintenance purpose of the facility and the property maintenance requirements of all itset the system inspected according to a ring local program staff to access the event this is not done. The easement should freduction practice(s).
IV.	IV. COMMENTS	
	By:	Date:

8-A.8.0. PERMEABLE PAVEMENT: DESIGN CHECKLIST

Plan Submission Date		
Site Plan/Permit Number		
Practice No./Location on Site		
Owner		
BMP Designer		Phone Number
General Contractor		Phone Number
Signature and stamp of lic	ensed profession	al design consultant and owner
Plan Status		
Approved	Legend:	Complete
Not Approved	J	Inc Incomplete/Incorrect - Not Applicable
Facility Type: Level 1	L	evel 2
Type of Pre-Treatment Facility:		
☐ Stone diaphragm		
☐ Grass filter strip		
☐ Other:	_	
this practice fits into the overall basin, infiltration trench, etc.). Showing the location of the per Facility area Contributing drainage a Proposed topographic Delineation of FEMA 10 Areas of the site compered Provide a soil map for the site boundaries Show soil boring locations and descriptions (at least one boring depth where infiltration is descriptions to table/bedrock or karst is identified Provide the results of soil infilted 0.5-inch/hour for Level 2 designment area)	I plan, and stating all at meable pavement are area (CDA) boundaries contours 00-year floodplain ensated for in water quand permeable paver provide the soil boring must be taken to designed to occur, to ied) tration rate testing to agn (minimum of one in the sign of the soil boring must be taken to designed to occur, to ied)	uality calculations ment area and its CDA, showing the facility g logs with Unified Soils Classifications and confirm the underlying soil properties at the o ensure that depth to the groundwater confirm a subsoil infiltration rate of at least infiltration test per 1,000 sq. ft. of planned
	l high groundwater ta	ble and bedrock (minimum 2 ft. below the
If karst is present, a detaile installation does not aggrav impermeable liner (min. 30 mi	vate potential karst il PVC Geo-membrandace beneath the perm	stigation is recommended to ensure the impacts (e.g., sinkholes, etc.) and an e liner covered by 8 to 12 oz./sq. yd. non-neable pavement, which must be designed

II. COMPUTATIONS

A.	Hydrology Determine the runoff curve number (pre- and post-developed conditions), providing the
	worksheets.
	Determine the time of concentration (pre- and post-developed conditions), providing the worksheets.
	Generate hydrographs (pre- and post-developed conditions) for appropriate design and safety
	storms (USDA-NRCS methods or modified rational-critical storm duration method)
В.	Hydraulics Verify that 2 to 4 feet of hydraulic head is available to drive flows through the facility Verify that the pavement will drain within 48 hours following a storm (minimum 36 hours).
	Specify the assumptions and coefficients used.
	Provide a stage-storage table and curve The designer may use the PICP Permeable Design Pro Software to design the pavement, including hydraulics (software available from the Interlocking Concrete Pavement Institute, at www.icpi.org)
C.	Water Quality
	Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet)
III.	PLAN REQUIREMENTS
Α.	BMP Plan View Information
	Show the limits of clearing and grading, noting that they should be identified and protected by
	acceptable signage, silt fence, snow fence, or other comparable barrier. Show the layout and dimensions of permeable pavement facility
	Ensure the proper orientation and slope of the facility, including pre-treatment, to avoid short-
	circuiting Show the location of the observation well(s)
_	 -
В.	BMP Section Views & Related Details
1.	Porous Asphalt
	Subgrade preparation Aggregate
	Aggregate Bedding layer: 2-inch layer of VDOT No. 8 choker stone (ASTM D448 size, 3/8 to 3/16
	inch diameter)
	Reservoir layer (required to support structural load): VDOT No. 2 open graded course aggregate or equivalent
	Filter layer: 2 to 4 inch layer of No. 8 choker stone laid over the native soil and covered by a 6 to 8 inch layer of coarse sand (e.g., ASTM C 33, 0.02-0.04 inch diameter
	particles) Porous asphalt surface layer
	Void content: 15% to 20%
	Thickness: Typically 3 to 7 inches, depending on the traffic load Open void fill media: None
	Underdrains Observation well (perforated vertical 4 to 6 inch diameter Schedule 40 PVC pipe – AASHTO M
	252 – with 3/8-inch diameter perforations at 6 inches on center and a lockable cap, installed
	flush with the surface) and underdrain pipes, which are of the same material – or equivalent corrugated HDPE may be used for smaller load-bearing applications – installed at a minimum
	0.5% slope for the full length of the permeable pavement cell and located no more than 20 feet

	from the next pipe. Non-perforated pipe may be used to connect with the storm drain system, and Ts and Ys may be installed, as needed, based on the underdrain configuration. Cleanout pipes should be extended to the surface with vented caps at the Ts and Ys.) Ensure there are no perforations in clean-outs and observation wells within 1 foot of the surface. Filter fabric: (Optional) Non-woven, polypropylene geotextile with:
	Grab tensile strength: ∃ 120 lbs. (ASTM D4632)
	Mullen burst strength: ∃ 225 lbs./sq. in. (ASTM D3786)
	Flow rate: > 125 gpm/sq. ft. (ASTM D4491)
	Apparent opening size (AOS): equivalent to US #70 or #80 sieve (ASTM D4751). The geotextile AOS selection is based on the percent passing the No. 200 sieve in "A" soil subgrade, using FHWA or AASHTO selection criteria.
2. F	Pervious Concrete
	Subgrade preparation
	Aggregate
	Bedding layer: None Reservoir layer (may not be needed to support structural load, but may be included to
	increase runoff storage or infiltration): VDOT No. 57 open graded course aggregate
	(ASTM D448 size, 1-1/2 to 1/2 inch diameter) or equivalent
	Filter layer: 2 to 4 inch layer of No. 8 choker stone (ASTM D448 size, 3/8 to 3/16 inch
	diameter) laid over the native soil and covered by a 6 to 8 inch layer of coarse sand
	(e.g., ASTM C 33, 0.02-0.04 inch diameter particles) Permeable concrete surface layer
	Void content: 15% to 25%
	Thickness: Typically 4 to 8 inches
	Compressive strength: 2.8 to 28 Mpa.
	Open void fill media: aggregate
	Underdrains
	Observation well
	Filter fabric: (Optional) Non-woven, polypropylene geotextile with:
	Grab tensile strength: ∃ 120 lbs. (ASTM D4632)
	Mullen burst strength: ∃ 225 lbs./sq. in. (ASTM D3786)
	Flow rate: > 125 gpm/sq. ft. (ASTM D4491)
	Apparent opening size (AOS): equivalent to US #70 or #80 sieve (ASTM D4751). The geotextile AOS selection is based on the percent passing the No. 200 sieve in "A" soil subgrade, using FHWA or AASHTO selection criteria.
3. F	Permeable Interlocking Concrete Pavers (PICP) Subgrade preparation
	Aggregate
	Bedding layer: 2-inch layer of No. 8 choker stone (ASTM D448 size, 3/8 to 3/16 inch diameter) laid over 3 to 4 inches of VDOT No. 57 open graded course aggregate (ASTM D448 size, 1-1/2 to 1/2 inch diameter) or equivalent
	Reservoir layer (required to support structural load): VDOT No. 57 open graded course aggregate (ASTM D448 size, 1-1/2 to 1/2 inch diameter) or equivalent
	Filter layer: 2 to 4 inch layer of No. 8 choker stone laid over the native soil and covered by a 6 to 8 inch layer of coarse sand (e.g., ASTM C 33, 0.02-0.04 inch diameter
	particles)
	Concrete paver surface layer (must conform to ASTM C936 specifications)
	Surface open area: 5% to 15%
	Thickness: 3.125 inches for vehicles Compressive strength: 55 Mpa.
	Compressive strength. 55 Mpa. Open void fill media: aggregate
	Underdrains
	Observation well

	Filter fabric: (Optional) Non-woven, polypropylene geotextile with:
	Grab tensile strength: ∃ 120 lbs. (ASTM D4632)
	Mullen burst strength: ∃ 225 lbs./sq. in. (ASTM D3786)
	Flow rate: > 125 gpm/sq. ft. (ASTM D4491)
	Apparent opening size (AOS): equivalent to US #70 or #80 sieve (ASTM D4751). The
	geotextile AOS selection is based on the percent passing the No. 200 sieve in "A" soil subgrade, using FHWA or AASHTO selection criteria.
	and Oct I Barrers
4.	oncrete Grid Pavers
	Subgrade preparation Aggregate
	diameter) laid over 3 to 4 inches of VDOT No. 57 open graded course aggregate (ASTM D448 size, 1-1/2 to 1/2 inch diameter) or equivalent
	Reservoir layer (required to support structural load): VDOT No. 57 open graded course
	aggregate (ASTM D448 size, 1-1/2 to 1/2 inch diameter) or equivalent
	Filter layer: 2 to 4 inch layer of No. 8 choker stone laid over the native soil and covered
	by a 6 to 8 inch layer of coarse sand (e.g., ASTM C 33, 0.02-0.04 inch diameter
	particles)
	Concrete paver surface layer (must conform to ASTM C1319 specifications) Open void area: 20% to 50%
	Open void area. 20% to 50% Thickness: 3. 5 inches
	Compressive strength: 35 Mpa.
	Open void fill media: aggregate, coarse sand, topsoil and grass
	Underdrains
	Observation well
	Filter fabric: (Optional) Non-woven, polypropylene geotextile with:
	Grab tensile strength: ∃ 120 lbs. (ASTM D4632)
	Mullen burst strength: ∃ 225 lbs./sq. in. (ASTM D3786)
	Flow rate: > 125 gpm/sq. ft. (ASTM D4491)
	Apparent opening size (AOS): equivalent to US #70 or #80 sieve (ASTM D4751). The
	geotextile AOS selection is based on the percent passing the No. 200 sieve in "A" soil subgrade, using FHWA or AASHTO selection criteria.
5.	astic Reinforced Grid Pavers
•	_ Subgrade preparation
	Aggregate
	Bedding layer: 2-inch layer of No. 8 choker stone (ASTM D448 size, 3/8 to 3/16 inch diameter) laid over 3 to 4 inches of VDOT No. 57 open graded course aggregate (ASTM
	D448 size, 1-1/2 to 1/2 inch diameter) or equivalent
	Reservoir layer (required to support structural load): VDOT No. 57 open graded course
	aggregate (ASTM D448 size, 1-1/2 to 1/2 inch diameter) or equivalent
	Filter layer: 2 to 4 inch layer of No. 8 choker stone laid over the native soil and covered
	by a 6 to 8 inch layer of coarse sand (e.g., ASTM C 33, 0.02-0.04 inch diameter
	particles) Concrete paver surface layer
_	Void content: Depends on fill material
	Compressive strength: Varies, depending on fill material
	Open void fill media: Aggregate, coarse sand, topsoil and grass
	Underdrains
	_ Observation well
	Filter fabric: (Optional) Non-woven, polypropylene geotextile with:
	Grab tensile strength: ∃ 120 lbs. (ASTM D4632)
	Mullen burst strength: ∃ 225 lbs./sq. in. (ASTM D3786)

		Flow rate: > 125 gpm/sq. ft. (ASTM D4491) Apparent opening size (AOS): equivalent to US #70 or #80 sieve (ASTM D4751). The geotextile AOS selection is based on the percent passing the No. 200 sieve in "A" soil subgrade, using FHWA or AASHTO selection criteria.
C.	Lan	dscape Plan (perimeter) Where grass is used in grid pavers, include specifications appropriate for the site's vegetation climatic zone (4-8 in Virginia)
		Specify preservation measures for existing vegetation surrounding permeable pavement area
D.	Con	struction Notes
		Permeable pavement areas should be clearly marked off and remain <i>outside</i> the limits of land
		disturbance during construction to prevent soil compaction by heavy equipment. Permeable pavement areas should <i>not</i> be used during construction as sites for temporary sediment traps or basins.
		Traffic control to avoid tracking mud and fine sediment
		Store materials in a protected area to keep them free from mud, dirt, and other foreign materials.
		Ensure that pre-treatment structures are properly installed and working effectively.
		Construction sequence: Construction inspections should occur before, during and after installation to ensure the
		permeable pavement installation is constructed according to specifications. Use detailed inspection checklists that require sign-offs by qualified individuals at critical states of construction, to ensure the contractor's interpretation of the plan is consistent with the
		designer's intent.
		Construction of the permeable pavement facility should begin only <i>after</i> site work is completed and the entire contributing drainage area has been stabilized with dense and healthy vegetation.
		Temporary E&S control measures (typically silt fence) to prevent sediment from moving into the stone base material or onto the pavement surface during construction), to avoid
		clogging Excavators or backhoes (with arms with adequate extension) should work from the
		sides to excavate the reservoir layer to its appropriate design depth and dimensions. For micro-scale and small-scale installations, excavators should avoid setting
		up inside the facility footprint to avoid compaction.
		Where feasible, use the cell construction approach, splitting the proposed permeable pavement area into 500 to 1,000 sq. ft. temporary cells with a 10 to 15 foot earth bridge in between, so the cells can be excavated from the side. Excavated material should be place away from the open excavation to avoid
		jeopardizing the stability of the side walls. Scarify or till the native soils along the bottom and sides of the permeable pavement
		system to a depth of 3 to 4 inches prior to placing the filter layer or filter fabric. For large scale paving applications with weak soils, the soil subgrade may need to be compacted to 95% of the Standard Proctor Density to achieve the desired load-bearing
		capacity (effectively eliminating any infiltration function, so this must be addressed during the hydrologic design stage).
		If used, filter fabric should be installed next along the bottom and sides of the reservoir
		layer. ——— Filter fabric strips should overlap down-slope by a minimum of 2 feet and should be secured a minimum of 4 feet beyond the edge of the excavation.
		Where the filter layer extends beyond the edge of the pavement (to convey runoff to the reservoir layer), install an additional layer of filter fabric 1 foot below the surface to prevent sediments from entering the reservoir layer.
		Do not trim excess filter fabric until the site is fully stabilized.
		Install the observation well(s) and, if used, install the underdrains.
		Check aggregate material prior to installation to confirm that it is clean and washed and meets specifications and is installed to the correct depth

		Check elevations (underdrain inverts, inflow and outflow point inverts, depth of aggregate installations, etc.) and the surface slope.
		Provide a minimum of 2 inches of aggregate above and below the underdrains. Underdrains should slope down towards the outlet at a grade of 0.5% or
		steeper Up-gradient ends of underdrains in the reservoir layer should be capped, but
		not the downstream ends.
		Where an underdrain pipe is connected to a structure, there must be <i>no</i> perforations within 1 foot of the structure.
		Ensure there are no perforations in clean-outs and observation wells within 1 foot of the surface.
		Moisten and spread 6-inch lifts of the appropriate clean, washed stone aggregate (usually No. 2 or No. 57 stone).
		Check aggregate material prior to installation to confirm that it is clean and washed and meets specifications and is installed to the correct depth. Place at least 4 inches of additional aggregate above the underdrain(s), and
		then compact it using a vibratory roller in static mode until there is no visible movement of the aggregate.
		Do not crush the aggregate with the roller. Install the design depth of bedding layer, depending on the type of pavement to be
		used.
		Install paving materials according to manufacturer or industry specifications for the type of pavement to be used (see Stormwater Design Specification No. 7 for specific guidance).
		Make sure the permeable pavement surface is even, that water spreads evenly across it, and the storage bed drains within 36 to 48 hours.
		Implement any remaining permanent stabilization measures.
		Log the GPS coordinates for each facility and submit them for entry into the local BMP maintenance tracking database.
Ε.		e Items (can include BMP Operation & Maintenance Inspection Checklists from Appendix 9-C of this Handbook)
	Provide mainter	a Maintenance Agreement, indicating the person or organization responsible for nance, authorizing access for inspections and maintenance, and including a maintenance ion checklist.
	———	Include a Maintenance Narrative which describes the long-term maintenance
		requirements of the facility and all components. a deed restriction or other enforceable mechanism, including GPS coordinates of the ensure the the permeable pavement is not converted to conventional pavement (in
	order to	maintain this component of the site's stormwater management plan).
IV.	COMMENTS	
		Rv. Date:

8-A.9.0. INFILTRATION PRACTICES: DESIGN CHECKLIST

Plan Submission Date	
Project Name	
Site Plan/Permit Number	
Practice No./Location on Site	
Owner	
BMP Designer	
General Contractor	Phone Number
Signature and stamp of licensed profe certification	ssional design consultant and owner
Plan Status	
Approved Legend :	Complete
Not Approved	Inc Incomplete/Incorrect N/A - Not Applicable
Facility Type: Level 1	Level 2
Hydraulic Configuration: On-line facility Off-line facility (sized to receive only a portion of the Treatment Volume) Type of Infiltration Facility: Surface facility (basin) Subsurface facility	Type of Pre-Treatment Facility: Sediment forebay (above ground) Sedimentation chamber Plunge pool Stone diaphragm Grass filter strip Grass channel Other:
 SUPPORTING INFORMATION Provide a concise narrative describing the sto this practice fits into the overall plan, and stating 	rmwater management strategy, describing how all assumptions made in the design.
Show the location of this BMP on the site map, i Facility area Contributing drainage area (CDA) boun as close to 100% impervious as possible Proposed topographic contours If a basin, the embankment area: cer abutments Delineation of FEMA 100-year floodplain	ncluding: daries and acreage (not to exceed 2 acres and e) nterline principal spillway, emergency spillway,
(HSG A and B soils are prime locations for infiltr Provide soil boring locations and soil boring descriptions (at least one boring must be taken depth where infiltration is designed to occutable/bedrock or karst is identified). NOTE: To content of less than 40% and a clay content of should not be located above fill soils, and "urbay graded are not good sites for infiltration. Nor in the soil of the	at the slope of the CDA does not exceed 15%. cility, showing the CDA and facility boundaries

_	Provide results of soil infiltration rate testing to confirm a subsoil infiltration rate of 0.5 to 1 inch/hour for Level 1 design or 1 to 4 inches/hour for a Level 2 design (the number of infiltration tests should be based on the scale of the planned infiltration facility area – see Table 8.3 and Appendix 8-A in Stormwater Design Specification No. 8). Depth to seasonal high groundwater table and bedrock (minimum 2 ft. below the design bottom of the facility)
	NOTE: An EPA UIC permit may be required for a facility exceeding 20,000 sq. ft. if the surface width is less than the maximum depth. Avoid installing geotextile filter fabric along the <i>bottom</i> of infiltration facilities (causes clogging). A layer of coarse washed choker stone is more effective. If karst is present, a detailed geotechnical investigation is recommended to ensure the installation does not aggravate potential karst impacts (e.g., sinkholes, etc.) and an impermeable liner (min. 30 mil PVC Geo-membrane liner covered by 8 to 12 oz./sq. yd. non-woven geotextile) must be place beneath the infiltration facility. Where karst is present, there must be at least 4 feet of vertical separation between the bottom of the infiltration facility and the karst layer. Furthermore, only micro-scale or small-scale infiltration facilities may be used, and they must be designed <i>ONLY</i> to meet the Level 1 design criteria (incorporating an underdrain). NOTE: Bioretention should be preferred to infiltration in karst locations.
II.	COMPUTATIONS
A.	 Hydrology Confirm a soil infiltration rate of 0.5 inch/hour minimum. NOTE: The <i>design</i> infiltration should be calculated to be 50% of the measured infiltration rate, to provide a factor of safety. A porosity value of 0.40 must be used in the design of stone reservoirs, although a larger value may be used if perforated corrugated metal pipe, plastic pipe, concrete arch pipe, or comparable materials are installed within the reservoir to detain runoff. Determine the runoff curve number (pre- and post-developed conditions), providing the worksheets. Determine the time of concentration (pre- and post-developed conditions), providing the worksheets. Generate hydrographs (pre- and post-developed conditions) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method)
B. 	Hydraulics Verify that there is sufficient hydraulic head to drive flows through the facility: 1 to 3 feet for micro-scale infiltration 1 to 5 feet for small-scale infiltration 2 to 6 feet for conventional large-scale infiltration The Treatment Volume should be infiltrated or drained from the facility within 36 to 48 hours. Specify the assumptions and coefficients used. Provide a stage-storage table and curve. Provide storm drainage and hydraulic grade line calculations.
C.	 Water Quality Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet) Specific sizing/dimensions must be determined from criteria in Stormwater Design Specification No. 8.

III. PLAN REQUIREMENTS

A.	BMF	P Plan View Information
		Show the limits of clearing and grading, noting that they should be identified and protected by
		acceptable signage, silt fence, snow fence, or other comparable barrier.
		Show the layout and dimensions of the infiltration facility
		Micro-scale infiltration from 250 to 2,500 sq. ft. (dry well, french drain, paving blocks)
		Small-scale infiltration from 2,500 to 20,000 sq. ft. (infiltration trench)
		Large-scale conventional infiltration from 20,000 to 100,000 sq. ft. (infiltration trench or
		basin)
		Show the location and confirm the proper orientation (to prevent short-circuiting) of all
		conveyance system outfalls into the basin with pre-treatment and outlet protection designed in accordance with the VE&SCH
		Ensure proper setbacks from building foundations, down-gradient slopes, etc.:
		5 feet down-gradient from dry or wet utility lines
		5 feet down-gradient and 25 feet up-gradient from building foundations for micro-scale
		infiltration facilities
		10 feet down-gradient and 50 feet up-gradient from building foundations for small-scale
		infiltration facilities
		25 feet down-gradient and 100 feet up-gradient from building foundations for large-scale infiltration facilities
		In cold climate areas, 25 feet from roadways to prevent potential frost heaving of the pavement
		50 feet from septic systems
		100 feet from any water supply well
		200 feet from down-gradient slopes with greater than 20% grade
		Infiltration basin features:
		Top of bank and basin bottom elevations
		Elevations of treatment volume and maximum design water surface elevations for all
		appropriate design storms and safety storms
		Side slope (H:V) of basin storage area and embankment (upstream and downstream
		slopes)
		Sediment forebay
		Maintenance access to the sediment forebay and riser structure Safety fence during construction, but <i>not after</i> completion of construction.
		Location of observation well for facilities larger than micro-scale (perforated vertical 6 inch
		diameter Schedule 40 PVC pipe – AASHTO M 252 – with 3/8-inch diameter perforations at 6 inches on center and a lockable cap, installed flush with the ground surface, with one for every 50 feet of length of the infiltration practice) and any underdrain pipes, which are of the same material – or equivalent corrugated HDPE may be used for smaller load-bearing applications – installed at a minimum 1.0% slope for the full length of the infiltration cell and located no more than 20 feet from the next pipe. Non-perforated pipe may be used to connect with the storm drain system, and Ts and Ys may be installed, as needed, based on the underdrain configuration. Cleanout pipes should be extended to the surface with vented caps at the Ts and Ys.) Ensure there are no perforations in clean-outs and observation wells within 1 foot of the surface. NOTE: An underdrain is required only for large-scale conventional infiltration facilities and for micro-scale infiltration facilities on marginal soils (where the underdrain must be elevated. Install non-perforated pipe with one or more caps, as needed from the structure.
В.	ВМР	P Section Views & Related Details
1.	Pre-	Treatment Practices
		Minimum 2 pre-treatment practices required for micro-scale infiltration facilities, but no minimum pre-treatment volume required.
		Minimum 3 pre-treatment practices required for small-scale infiltration facilities, and pre-treatment volume is required to be 15% of the Treatment Volume.

	Minimum 3 pre-treatment practices required for large-scale conventional infiltration facilities, and pre-treatment volume is required to be 25% of the Treatment Volume. If the facility footprint exceeds 20,000 sq. ft., a surface pre-treatment cell must be provided (e.g., sand filter or dry sediment basin).
	 Pre-treatment facilities designed so exit velocities are non-erosive for the 2-year design storm and evenly distribute runoff flows across the width of the facility (using a level spreader, etc.) In cold climate areas, oversize pre-treatment measures by up to 40% to account for additional sediment load caused by road sanding.
	iltration Basin (also refer to the checklists for Extended Detention Facilities – Section 8-16.0 – regarding Earthen Embankments, Principal Spillways, Emergency Spillways, etc.) Best if designed to be off-line, to avoid damage from the erosive velocities of larger storms. Elevations of treatment volume and maximum design water surface elevations for all appropriate design storms and safety storms Maximum depth no greater than 1 foot (a maximum of 2 feet if pre-treatment cells are used) Bottom of the basin should be flat (i.e., 0% longitudinal and lateral slopes). A maximum longitudinal slope of 1% is permissible if an underdrain is used.
	 Top of dam elevations: constructed height and settled height (allowing for 10% settlement). Adequate freeboard Top width labeled Elevation of crest of emergency spillway
	Principal/emergency spillway, with side slopes labeled.
	 Existing ground and proposed improvements along center line of emergency spillway Dimensions of zones for zoned embankment Foundation Cut Off Trench or Key Trench Materials labeled
	Bottom width (4' minimum, or greater, as specified in the geotechnical report). Side slopes labeled (4H:1V maximum steepness). Depth (4' minimum or as specified in the geotechnical report)
3. Inf	iltration Trench _ Dimensions provided _ Maximum depth:
	3 feet for micro-scale infiltration facilities 5 feet for small-scale infiltration trenches 6 feet for large-scale conventional infiltration trenches In cold climate areas, the bottom of the trench should extend below the frost line Bottom of the trench should be flat (i.e., 0% longitudinal and lateral slopes). A maximum longitudinal slope of 1% is permissible if an underdrain is used.
	Aggregate specifications:Reservoir stone must be clean washed VDOT No. 1 Open-Graded Coarse Aggregate (diameter of 3.5 to 1.5 inches) or equivalentStone jacket for the underdrain must be clean double-washed VDOT No. 57 open graded course aggregate (ASTM D448 size, 1-1/2 to 1/2 inch diameter) or equivalent, free of all soil fines, installed 3 inches above the underdrain and 12 inches below it.
	Filter fabric installed on the sides of the infiltration facility (to prevent piping) must be non-woven polyprene geotextile with a flow rate of > 110 gpm/sq. ft. (Geotex 351 or equivalent). The trench surface can be covered by a 3-inch layer of river stone or pea gravel. Turf is acceptable when there is sub-surface inflow (e.g., a roof leader).

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Ċ.	Lan	dscape	
			grass is used on the infiltration facility surface, include specifications appropriate for the egetation climatic zone (4-8 in Virginia)
			r preservation measures for existing vegetation surrounding the infiltration area
			adjacent vegetation from forming an overhead canopy above the infiltration facility, in
			b keep leaf litter, fruits and other vegetative litter from clogging the stone.
D.	Con	structio	n Notes
			on areas should be clearly marked off and remain outside the limits of land disturbance
			construction to prevent soil compaction by heavy equipment. Infiltration areas should not
			d during construction as sites for temporary sediment traps or basins, which can clog the
			pils with fine sediments.
			e traffic control to avoid tracking mud and fine sediment and compacting the soil.
			naterials in a protected area to keep them free from mud, dirt, and other foreign materials. that pre-treatment structures are properly installed and working effectively.
			ne infiltration facility "off-line" until construction is complete.
			uction sequence:
		Constit	Construction inspections should occur before, during and after installation to ensure the
			infiltration facility is constructed according to specifications. Use detailed inspection
			checklists that require sign-offs by qualified individuals at critical states of construction,
			to ensure the contractor's interpretation of the plan is consistent with the designer's
			intent.
			Construction of the infiltration facility should begin only after site work is completed and
			the entire contributing drainage area has been stabilized with dense and healthy
			vegetation.
			Temporary E&S control measures (typically super silt fence, diversion berms, etc.) to prevent sediment from moving into the stone base material or onto the pavement
			surface during construction), to avoid clogging. The plan should indicate the conditions
			that must be met before runoff may be directed to a conventional infiltration basin.
			Excavators or backhoes (with arms with adequate extension) should work from the
			sides to excavate the reservoir layer to its appropriate design depth and dimensions.
			The floor of the facility should be completely level, but equipment should be
			kept off the floor to prevent soil compaction.
			Correctly install filter fabric on the trench sides.
			Trim large tree roots flush with the sides of the trench to prevent puncturing or
			tearing of the filter fabric.
			When laying out the geotextile, the width should include sufficient material to compensate for perimeter irregularities in the trench and for a 6-inch minimum
			overlap at the top of the trench.
			Tuck filter fabric under the sand layer on the bottom of the trench.
			Place stones or other anchoring objects on the fabric at the trench sides to keep
			the trench open during windy periods.
			Place natural soils in any voids that occur between the fabric and the excavated
			sides of the trench, to ensure the fabric conforms smoothly to the sides of the
			excavation.
			Scarify or till the native soils along the bottom and sides of the permeable pavement
			system to a depth of 3 to 4 inches prior.
			Spread 6 inches of sand on the bottom as a filter layer.
			Install and anchor the observation well(s) and, if used, install the underdrains. Check aggregate material prior to installation to confirm that it is clean and
			washed and meets specifications and is installed to the correct depth
			Check elevations (underdrain inverts, inflow and outflow point inverts, depth of
			aggregate installations, etc.) and the surface slope.
			Provide a minimum of 2 inches of aggregate above and below the underdrains.
			Underdrains should slope down towards the outlet at a grade of 0.5% or
			steeper.

	Up-gradient ends of underdrains in the reservoir layer should be capped, but not the downstream ends. Where an underdrain pipe is connected to a structure, there must be no perforations within 1 foot of the structure. Ensure there are no perforations in clean-outs and observation wells within 1 foot of the surface. Moisten and spread 1-foot lifts of the appropriate clean, washed stone aggregate (usually No. 2 or No. 57 stone). Check aggregate material prior to installation to confirm that it is clean and washed and meets specifications and is installed to the correct depth. Place at least 4 inches of additional aggregate above the underdrain(s), and then compact it using a vibratory roller in static mode until there is no visible movement of the aggregate. Do not crush the aggregate with the roller. Use sod to establish a dense turf cover for at least 10 feet on each side of the infiltration facility, to reduce erosion and sloughing. If the vegetation is seeded instead, use native grasses primarily due to their adaptability to the local climate and soil conditions. Implement any remaining permanent stabilization measures. Log the GPS coordinates for each facility and submit them for entry into the local BMP
	maintenance tracking database. nce Items (can include BMP Operation & Maintenance Inspection Checklists from 9, Appendix 9-C of this Handbook)
Proma	ide a Maintenance Agreement, indicating the person or organization responsible for intenance, authorizing access for inspections and maintenance, and including a maintenance ection checklist. Include a Maintenance Narrative which describes the long-term maintenance requirements of the facility and all components, including removal and disposal of trash, debris and sediment accumulations, and regular mowing. ord a deed restriction or other enforceable mechanism, including GPS coordinates of the to ensure that infiltration areas are not converted to other uses. ide sufficient facility access from public ROW or roadway to facilitate inspection and intenance.
	By: Date:

8-A.10.0. BIORETENTION PRACTICES: DESIGN CHECKLIST

Plan Submission Date		
Project Name		
Site Plan/Permit Number		
Practice No./Location on Site		
Owner		Phone Number
		Phone Number
General Contractor		
Signature and stamp of lice certification	ensed profes	ssional design consultant and owner
Plan Status		
Approved	Legend:	Complete
Not Approved	Logona.	Inc Incomplete/Incorrect
Not Approved		N/A - Not Applicable
Facility Type: Level 1		Level 2
Hydraulic Configuration:		Type of Pre-Treatment Facility:
☐ On-line facility		☐ Sedimentation chamber
☐ Off-line facility		☐ Plunge pool
		☐ Stone diaphragm
		☐ Grass filter strip
		☐ Grass channel
		□ Other:
		□ Offici
I. SUPPORTING INFORMATION		
Provide a concise parrative descr	ihing the storm	water management strategy, describing how
this practice fits into the overall plan		
Show the location of this BMP on the		
Facility area	ic one map, mo	daing the following.
Contributing drainage area	(CDA) boundar	ries and acreage
Embankment area	(OD/I) Dodiladi	io and dorougo.
	ear floodplain (bioretention should be constructed outside the
limits of the floodplain).	cai nocapiam (i	olorotorition chould be concluded actored the
Areas of site compensated	for in water au:	ality calculations
		hotspot land use, then an underdrain must be
used.	C ranon nom a	notspot land use, then an underdrain must be
	located where	they will receive regular dry weather flows or
		n water, chlorinated wash-water or swimming
pool discharge, or other flows that		
		the slope of the CDA is between 1% and 5%.
Provide a soil map for site and area		
· · · · · · · · · · · · · · · · · · ·	•	I boring logs with Unified Soils Classifications
		en to confirm the underlying soil properties at
		esigned to occur, to ensure that depth to the
<u> </u>	,	. HSG-B, C or D soils typically require an
underdrain, whereas HSG-A soils of	jenerally do not	•

	Provide the results of soil infiltration rate testing to confirm a minimum subsoil infiltration rate of
	> 0.5 inch/hour (> 1 inch/hour in order to avoid the use of an underdrain). The number of
	infiltration tests is based on the scale of the planned infiltration facility area - see Tables 9.2 and
	9.3 in Stormwater Design Specification No. 9 and Appendix 8-A in Stormwater Design
	Specification No. 8).
	Confirm the depth to seasonal high groundwater table (minimum 2 ft. below the design bottom of
	the facility, or 1 ft. if in a coastal area and a large-diameter underdrain is used that only partially
	dewaters the bed)
	Confirm the depth to bedrock (minimum 2 ft. below the design bottom of the facility) If karst is present, a detailed geotechnical investigation is recommended to ensure the installation does not aggravate potential karst impacts (e.g., sinkholes, etc.) and an impermeable liner (recommend a min. 30 mil PVC Geo-membrane liner covered by 8 to 12 oz./sq. yd. non-woven geotextile) must be place beneath the bioretention facility. Where karst is present, there must be at least 3 feet of vertical separation between the bottom of the bioretention facility and the karst layer. Furthermore, only micro-scale or small-scale bioretention facilities not exceeding 20,000 sq. ft. may be used, and they must be designed ONLY to meet the Level 1 design criteria (incorporating an underdrain).
	Identify potential conflicts with other (existing?) structural components (pipes, underground
	utilities, etc.)
	Avoid installing geotextile filter fabric along the bottom of bioretention facilities (causes
	clogging).
II. A.	COMPUTATIONS Hydrology
	Determine the runoff curve numbers (pre- and post-developed conditions), providing the
	worksheets.
	Determine the time of concentration (pre- and post-developed conditions), providing the
	worksheets.
_	Generate hydrographs (pre- and post-developed conditions) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method) Urban Bioretention facilities, in particular, should be designed to fully drain within 24 hours following each storm.
R	Hydraulics
	Ensure that 4 to 5 feet of hydraulic head (3 to 5 feet for Urban Bioretention) are available above the bottom elevation needed to tie the underdrain into the storm drain system, in order to drive runoff through the filter bed. Less head is necessary for HSG-A soils. Specify assumptions and coefficients used. Provide a stage-storage table and curve Provide for large storm overflow or bypass Provide storm drainage and hydraulic grade line calculations.
_	
C.	Water Quality
	Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the
	CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet) Provide specific sizing/dimensions determined from criteria in Stormwater Design Specification
	No 9

III. PLAN REQUIREMENTS

Α.	BMP Plan View Information
	Show the limits of clearing and grading, noting that they should be identified and protected by
	acceptable signage, silt fence, snow fence, or other comparable barrier.
	Show the layout and dimensions of the bioretention facilities / planters. NOTE: The maximum
	contributing drainage area for a micro-bioretention facility (e.g., rain garden) is 0.5 acre (3% of
	the CDA or 5% of the roof area for Level 1 or 4% of the CDA or 6% of the roof area for Level 2);
	for an urban bioretention facility is 2,500 sq. ft., and for a conventional bioretention facility is 2.5
	acres.
	Observe proper setbacks from building foundations, down-gradient slopes, etc.:
	5 feet down-gradient from wet utility lines. NOTE: Dry utility lines (e.g., gas, electric,
	cable and telephone, etc.) may cross under bioretention areas if they are double-cased.
	10 feet down-gradient from building foundations for urban bioretention. NOTE: If the
	facility is lined and an underdrain is used, there is no minimum setback requirement.
	5 feet down-gradient and 25 feet up-gradient from building foundations for micro-scale
	(rain garden) facilities
	10 feet down-gradient and 50 feet up-gradient from building foundations for standard
	bioretention facilities with a 0.5 acre or smaller CDA
	25 feet down-gradient and 100 feet up-gradient from building foundations for standard
	bioretention facilities with a CDA of between 0.5 to 2.5 acres.
	If an in-ground basement or other special conditions exist, the design should be
	reviewed by a licensed engineer. NOTE: A special footing or drainage design may be
	used to justify a reduction of the setbacks noted above.
	In cold climate areas, 25 feet from roadways to prevent potential frost heaving of the
	pavement
	100 feet from any water supply well (50 feet if the biofilter is lined)
	Design Urban Bioretention, in particular, to minimize interference with pedestrian traffic and
	allow for frequent landscape and facility maintenance
	Geometry:
	Level 1: Length of the shortest flow path/overall length = 0.3 <i>OR</i> other design methods
	are used to prevent short-circuiting; a one-cell design (not including the pre-treatment
	cell.
	Level 2: Length of the shortest flow path/overall length = 0.8 <i>OR</i> other design methods
	are used to prevent short-circuiting; a two-cell design (not including the pre-treatment
	cell.
	Show the location of all conveyance system outfalls (inlets) into the facility with pre-treatment
	and outlet protection designed in accordance with the VE&SCH
	Ensure the proper geometry and orientation of the facility and inlets to the facility to avoid short-
	circuiting
	Show the top-of-bank and basin bottom elevations
	Show the treatment volume and maximum water surface elevations for all appropriate design
	storms and safety storms
	Show the location of the underdrain, if applicable
	Ensure and show adequate maintenance access to the facility
	Show the location of the observation well
В.	BMP Section Views & Related Details
4	Micro-Bioretention Facility (Rain Garden)
1.	Pre-treatment:
	Fre-treatment Level 1: External (leaf screens, grass filter strip, energy dissipators, etc.)
	Level 1. External (lear screens, grass filter strip, energy dissipators, etc.) Level 2: External <i>plus</i> a grass filter strip
	Inflow: From sheet flow or a roof leader
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	Facility may be a single-cell design (can be divided into smaller cells at downspout locations) Maximum ponding depth: 6 inches.
	waxiinum ponuing deptin o inches.

	Show the elevations of treatment volume and maximum design water surface elevations for all appropriate design storms and safety storms
	Show the facility rim elevations: constructed height and settled height (allowing for 10% settlement).
	Ensure adequate freeboard
	Provide a typical grading section through the facility
	Filter media:
	Depth: minimum 18 inches for Level 1; minimum 24 inches for Level 2; recommended maximum depth is 36 inches for both.
	Media mixed on site or supplied by vendor for Level 1, but <i>must</i> be supplied by vendor for Level 2
	P-index: Between 20 and 30 for a media mix, <i>OR</i> between 7 and 21 mg/kg of P in the soil media (see Section 6.6 of Stormwater Design Specification No. 9) Cation Exchange Capacity (CEC): Soils with a CEC exceeding 10 are preferred for pollutant removal.
	Infiltration Rate: Between 1 to 2 inches per hour
	Media mix: Equivalent to loamy sand, with the following composition: 85% to 88% sand
	8% to 12% soil fines
	3% to 5% organic matter
	Mulch cover: 2 to 3-inch layer composed of shredded, aged hardwood bark mulch Underdrain:
	Level 1: Corrugated HDPE or equivalent
	Level 2: Corrugated HDPE or equivalent, with a minimum 6-inch stone sump below the invert; <i>OR</i> none, if soil infiltration requirements are met
	A minimum of 3 inches of VDOT #57 clean washed stone (less than 1% passing a #200
	sieve) must be laid and packed above and below the pipe. Cleanouts are <i>not</i> needed
	In cold climates (winter or otherwise) it is advisable to extend the filter bed and underdrain pipe
	below the frost line and/or oversize the underdrain by on pipe size to reduce the potential for freezing.
	Vegetation:
	Level 1: Turf or herbaceous cover (alternative to mulch), or shrubs (minimum 1 of these 3 choices)
	Level 2: Turf or herbaceous cover (alternative to mulch), shrubs, or trees (minimum 2 of these 4 choices)
2. Star	ndard Bioretention Filter or Bioretention Basin
	Pre-treatment: Level 1: A pre-treatment cell, grass filter strip, gravel diaphragm, gravel flow spreader,
	or another approved (manufactured) pre-treatment device.
	Level 2: A pre-treatment cell <i>plus</i> one of the following: a grass filter strip, gravel diaphragm, gravel flow spreader, or another approved (manufactured) pre-treatment
	device. Inflow: From sheet flow, curb cuts, trench drains, concentrated flow, or the equivalent
	Maximum ponding depth: 6 inches (preferred) to 12 inches. NOTE: Ponding depths greater than
	6 inches will require a specific planting plan to ensure appropriate plant selection.
	Show the elevations of treatment volume and maximum design water surface elevations for all
	appropriate design storms and safety storms Show the facility rim elevations: constructed height and settled height (allowing for 10%)
	settlement).
	Ensure adequate freeboard
-	Provide a typical grading section through the facility
	Filter media: Depth: minimum 24 inches for Level 1; minimum 36 inches for Level 2; recommended
	maximum depth is 6 feet for both.

	Media mixed on site or supplied by vendor for Level 1, but <i>must</i> be supplied by vendor for Level 2
	P-index: Between 20 and 30 for a media mix, <i>OR</i> between 7 and 21 mg/kg of P in the soil media (see Section 6.6 of Stormwater Design Specification No. 9) Cation Exchange Capacity (CEC): Soils with a CEC exceeding 10 are preferred for
	pollutant removal.
	Infiltration Rate: Between 1 to 2 inches per hour Media mix: Equivalent to loamy sand, with the following composition:
	85% to 88% sand
	8% to 12% soil fines
	3% to 5% organic matter
	Mulch cover: 2 to 3-inch layer composed of shredded, aged hardwood bark mulch Underdrain:
	Level 1: Schedule 40 PVC with clean-outs
	Level 2: Schedule 40 PVC with clean-outs and with a minimum 12-inch stone sump
	below the invert; OR none, if soil infiltration requirements are met
	A minimum of 3 inches of VDOT #57 clean washed stone (less than 1% passing a #200 sieve) must be laid and packed above and below the pipe.
	In cold climates (winter or otherwise) it is advisable to extend the filter bed and underdrain pipe
	below the frost line and/or oversize the underdrain by on pipe size to reduce the potential for freezing.
	Conveyance and Overflow:
	For on-line bioretention: Incorporate an overflow structure to safely convey larger storms
	through the bioretention area. The following criteria apply to overflow structures:
	The overflow associated with the 2-year and 10-year design storms should be
	controlled so that velocities are non-erosive at the outlet point (to prevent downstream erosion)
	Common overflow systems within bioretention practices consist of an inlet structure, where the top of the structure is placed at the maximum water surface
	elevation of the bioretention area, which is typically 6 to 12 inches above the surface of the filter bed (6 inches is preferred).
	The overflow capture device (typically a yard inlet) should be scaled to the
	application; this may be a landscape grate inlet or a commercial-type structure. The filter bed surface should generally be flat so the bioretention area fills up
	like a bathtub.
	For off-line bioretention (preferred): Create an alternate flow path at the inflow point into the structure so that when the maximum ponding depth is reached, the incoming flow is
	diverted past the facility (so that the excess flows do not pass over the filter bed and
	through the facility, but additional flow is able to enter as the ponding water filters
	through the soil media).
	_ Vegetation:
	Level 1: A planting template to include turf or herbaceous cover (alternative to mulch), shrubs, and/or trees to achieve surface area coverage of at least 75% within 2 years.
	Level 2: A planting template to include turf or herbaceous cover (alternative to mulch),
	shrubs, and/or trees to achieve surface area coverage of at least 90% within 2 years. If
	using turf, it must be combined with other vegetation.
0 11	on Dispetantian (plantage etc.)
3. Urb	an Bioretention (planters, etc.) Pre-treatment (keep in mind the aesthetic qualities of the visible materials):
	A pre-treatment cell, grass filter strip, gravel diaphragm, gravel flow spreader, or another
	approved (manufactured) pre-treatment device.
	A trash rack between the pre-treatment cell and the main filter bed, allowing trash to be
	collected from a single location.
	Trash racks across curb cuts, keeping trash in the gutter, accessible to street-sweeping equipment.

	A pre-treatment area above the ground or a manhole or removable grate directly over
	the pre-treatment area. Inflow: From sheet flow, curb cuts, trench drains, roof drains, concentrated flow, or the
	equivalent
	Inlets should be stabilized with VDOT #3 stone, a splash block, river stone, or another
	acceptable energy dissipation measure.
	Surface slope: 1% toward the outlet, unless a stormwater planter is used.
	Maximum ponding depth: 6 inches (preferred) to 12 inches. NOTE: Ponding depths greater than
	6 inches will require a specific planting plan to ensure appropriate plant selection.
	Filter media:
	Depth: minimum 30 inches; recommended maximum depth is 4 feet. NOTE: If large
	trees and shrubs are planted, the <i>minimum</i> depth should be 4 feet.
	Media mixed on site or supplied by vendor for Level 1, but <i>must</i> be supplied by vendor
	for Level 2
	P-index: Between 20 and 30 for a media mix, OR between 7 and 21 mg/kg of P in the
	soil media (see Section 6.6 of Stormwater Design Specification No. 9)
	Cation Exchange Capacity (CEC): Soils with a CEC exceeding 10 are preferred for
	pollutant removal.
	Infiltration Rate: Between 1 to 2 inches per hour Media mix: Equivalent to loamy sand, with the following composition:
	Niedla filix. Equivalent to loarry sand, with the following composition.
	8% to 12% soil fines
	3% to 5% organic matter
	Filter media in a box should be extended from one wall to within 6 inches of the opposite
	wall, and it may be centered in the box or offset to one side.
	Filter media must be separated from the soil by non-woven geotextile fabric or a 2 to 3
	inch layer of either washed VDOT #8 stone or 1/8 to 3/8-inch pea gravel.
	Mulch cover: 2 to 3-inch layer composed of shredded, aged hardwood bark mulch.
	Waterproof stormwater planters near building foundations by using a watertight concrete shell or
	an impermeable liner, to prevent seepage.
-	Expanded tree pits:
	The bottom of the soil/media layer must be a minimum of 4 inches below the root ball of
	trees and shrubs being planted. Where portions of extended tree pits are covered with permeable pavers or cantilevered
	sidewalks, ensure the filter media is connected beneath these surfaces so roots can
	share the space.
	Installing a removable tree pit grate (capable of supporting H-20 axel loads) over the
	filter bed media can prevent pedestrian traffic and trash accumulation.
	Low, wrought iron fences can help restrict pedestrian traffic across the tree pit bed and
	protect pedestrians where there is a drop-off from the sidewalk to the bioretention cell.
	Each tree needs a minimum of 400 cubic feet of shared root space.
	Stormwater Curb Extensions: It may be necessary to provide a barrier to keep water from
	saturating the adjacent road or street's sub-base and ensure it continues to be capable of
	supporting H-20 axel loads.
	Underdrain:
	Slotted Schedule 40 PVC pipe greater than 4 inches in diameter, with clean-outs.
	A minimum of 2 inches of VDOT #57 clean washed stone (less than 1% passing a #200
	sieve) must be laid and packed above and below the pipe. Minimum underdrain pipe slope is 0.5%.
	Overflows can either be diverted from entering the bioretention cell or dealt with via an overflow
	inlet. Optional methods include:
	Curb openings sized to capture only the treatment volume and bypass higher flows
	through the existing gutter.
	Landscaping-type inlets or standpipes with trash guards.
	A pre-treatment chamber with a weir design that limits flow to the filter bed area.

	Any grates used above Urban Bioretention areas must be removable to allow maintenance
	access.
	Stencil or otherwise permanently mark each Urban Bioretention unit as a "stormwater management facility," indicating that (1) it has a water quality protection purpose, (2) it may pond briefly after a storm, and (3) it is not to be disturbed except for required maintenance. Vegetation:
	Urban Bioretention cells can vary from formal gardens or naturalized landscapes, depending on the degree of landscape maintenance that can be provided Where less frequent maintenance may be available and trash accumulation is a concern, use a "turf and trees" landscape model, perhaps including some herbaceous flowering plants. Choose native trees and shrubs known to be hearty in the polluted air and compacted soils of urban settings, although some ornamental species can be used. Selected vegetation must be tolerant of road salts, drought, and inundation.
C. La	andscape Plan
	Consider the importance of aesthetics and visual characteristics (foliage form, texture, color, etc.)
	 Consider visibility, traffic considerations and other safety issues Provide a planting schedule and specifications (transport / storage / installation / maintenance) Plant selection should be appropriate for the site's vegetation climatic zone (4-8 in Virginia), emphasizing native species
	Check whether future tree canopy heights associated with Urban Bioretention practices will interfere with existing overhead utility lines.
	 Specify preservation measures for existing vegetation The construction contract should include a Care and Replacement Warranty that specifies a minimum survival for species planted of 75% after the first growing season, and a minimum effective ground cover of 75% for flat roofs and 90% for pitched roofs.
D. E	cological Considerations
	Consider sun and wind exposure
	 Consider the effects upon bioretention area from adjacent plant communities Wildlife benefits appropriate for the location may be included in plant material layout Consider any insect and disease infestation at or near the facility site
F C	onstruction Notes
	 Planned bioretention areas should be clearly marked off and remain <i>outside</i> the limits of land disturbance during construction to prevent soil compaction by heavy equipment. Bioretention areas <i>may</i> be used during construction as sites for temporary sediment traps or basins, provided the construction plans include notes and graphical details specifying the
	following: The maximum excavation depth at the construction stage must be at least 1 foot above the post-construction installation.
	 The facility must contain an underdrain. Showing the proper procedures for converting the temporary sediment controls to a permanent bioretention facility, including dewatering, cleanout and stabilization. Provide traffic control to avoid tracking mud and fine sediment into the facility and compacting
	the soil. Store materials in a protected area to keep them free from mud, dirt and other foreign materials.
	Obtain filter media from an approved vendor and store it on an adjacent impervious area or on plastic sheeting. Where any Urban Bioretention facilities are constructed in the road or right-of-way, the
	construction sequence may need to be adjusted to account for traffic control, pedestrian access and utility notification.

Construction sequence:
Construction inspections should occur before, during and after installation to ensure the
bioretention facility is constructed according to specifications.
Use detailed inspection checklists that require sign-offs by qualified individuals
at critical states of construction, to ensure the contractor's interpretation of the
plan is consistent with the designer's intent.
Check the proposed site for existing utilities prior to any excavation.
The designer and the installer/contractor should have a pre-construction meeting,
checking the boundaries of the CDA and the actual inlet elevations to ensure they
conform to the original design.
The designer should clearly communicate, in writing, any project changes
determined during the pre-construction meeting to the installer and the plan
review/inspection authority.
Construction of the bioretention facility should begin only after site work is completed
and the entire contributing drainage area has been stabilized with dense and healthy
vegetation.
It may be necessary to block certain curb or other inlets while the bioretention area is
being constructed.
Temporary E&S control measures (typically silt fence, diversion berms, EC fabric, etc.)
to prevent sediment from moving into the filter media or stone base material during
construction), to avoid clogging (particularly if the practice relies on infiltration), and to
protect the facility's vulnerable side slopes from erosion during construction.
Ensure that pre-treatment structures are properly installed and working effectively.
Excavators or backhoes (with arms with adequate extension) should work from the
sides to excavate the reservoir layer to its appropriate design depth and dimensions.
Contractors should use a cell construction approach in larger bioretention
basins, with the basin split into 500 to 1,000 sq. ft. temporary cells with a 10 to
15 foot earth bridge in between each cell, so that cells can be excavated from
the side.
The floor of the facility should be completely level, but equipment should be
kept off the floor to prevent soil compaction.
It may be necessary to rip the bottom soils to a depth of 6 to 12 inches to
promote greater infiltration.
Correctly install geotextile fabric on the excavation sides.
Trim large tree roots flush with the sides of the excavation to prevent puncturing
or tearing of the filter fabric.
When laying out the geotextile, the width should include sufficient material to
compensate for perimeter irregularities in the trench and for a 6-inch minimum
overlap at the top of the excavation.
Place stones or other anchoring objects on the fabric at the trench sides to keep
the trench open during windy periods.
Place natural soils in any voids that occur between the fabric and the excavated
sides of the trench, to ensure the fabric conforms smoothly to the sides of the
excavation.
Install and anchor the observation well(s) and, if used, install the underdrains.
Check aggregate material prior to installation to confirm that it is clean and
washed and meets specifications and is installed to the correct depth
Check elevations (underdrain inverts, inflow and outflow point inverts, depth of
aggregate installations, etc.) and the surface slope.
Provide the correct depth and type of aggregate above and below the
underdrains.
Underdrains should slope down towards the outlet at a grade of 0.5% or
steeper.
Up-gradient ends of underdrains in the reservoir layer should be capped, but
not the downstream ends.

		Where an underdrain pipe is connected to a structure, there must be no
		perforations within 1 foot of the structure. Ensure there are no perforations in clean-outs and observation wells within 1
		foot of the surface.
		Place approximately 3 inches of choker stone/pea gravel on the stone above the
	 -	underdrain(s) as a filter between the underdrain stone layer and the soil filter media.
		Place the filter media by hand (to avoid compaction and maintain porosity) in 12-inch
		lifts, with no machinery allowed directly on the media surface during or after
		construction, until the design top elevation is achieved.
		Overfill the media above the proposed finished surface elevation to allow for natural settling. Lifts may be lightly watered to encourage settling.
		After the final lift is placed, rake the media to level it, saturate it, and allow it to
		settle for at least one week prior to installing plant materials. Check for
		settlement and add additional media, if needed, to achieve the design elevation.
		Prepare planting holes for any trees and shrubs, install the vegetation, and water
		accordingly.
		Install any temporary irrigation equipment.
		Place the surface cover in the bioretention cells (mulch, river stone or turf), depending on the design.
		If coir or jute matting will be used instead of mulch, the matting will need to be
		installed prior to planting, and holes or slits will have to be cut in the matting to
		install the plants.
		Install the plant materials as shown in the landscaping plan, and water them during
		weeks of no rain for the first two months following installation.
		The construction contract should include a Care and Replacement Warranty to
		ensure that vegetation is properly established and survives during the first growing season following construction.
		Implement any remaining permanent stabilization measures.
		Log the GPS coordinates for each facility and submit them for entry into the local BMP
		maintenance tracking database.
_	Maintanana	a Hama (ass include DND Operation 9 Maintenance Inspection Charlista from
⊏.		e Items (can include BMP Operation & Maintenance Inspection Checklists from Appendix 9-C of this Handbook)
		e a Maintenance Agreement, indicating the person or organization responsible for
		nance, authorizing access for inspections and maintenance, and including a maintenance
		tion checklist.
		Include a Maintenance Narrative which describes the long-term maintenance
		requirements of the facility and all components, including removal and disposal of trash,
		debris and sediment accumulations, periodic replacement of soil media, care of the
	Record	vegetation, and mowing. I a deed restriction, drainage easement, and/or other enforceable mechanism, including
		pordinates of the area, to ensure the bioretention areas are not disturbed or converted to
	other u	·
		e sufficient facility access from the public ROW or roadway to both the bioretention facility
	and an	y pre-treatment practices.
IV	COMMENTS	
IV.	COMMENT	

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By: Date	::

8-A.11.0. DRY SWALES: DESIGN CHECKLIST

(NOTE: Think of this practice as linear bioretention)

Plan Submission Date	
Proiect Name	
Site Plan/Permit Number	
Practice No./Location on Site	
Owner	Phone Number
BMP Designer	Phone Number
General Contractor	Phone Number
Signature and stamp of licensed p certification	rofessional design consultant and owner
Plan Status	
Approved Legend:	Complete - Complete
Not Approved	Inc Incomplete/IncorrectN/A - Not Applicable
Facility Type: Level 1	Level 2
Type of Dry Swale: Dry Conveyance Swale Dry Treatment Swale Hydraulic Configuration: On-line (typical) Off-line (more rare, for Level 2 designs only)	Type of Pre-Treatment Facility: Sediment Forebay Check Dam Tree Check Dam Grass Filter Strip Gravel Diaphragm Pea Gravel Flow Spreader Other:
this practice fits into the overall plan, and statin Show the location of the BMP on the site map, Swale area Contributing drainage area (CDA) bour Delineation of FEMA 100-year floodpla	including: ndaries and acreage nin
but preferably not exceeding 2%. Check dams can be used to reduce the contact time to enhance filtering and/or In areas of steep terrain, Dry Swales gradient, as long as a terraced multiple filtering.	that the slope of the CDA is between 1% and 4%, ne effective slopes of the swale and lengthen the r infiltration. s can be implemented on slopes of up to 20% le-cell design is used to dissipate energy prior to
constructed. Provide a soil map for the site and area of the I Provide soil boring locations and soil boring descriptions (at least one boring must be take	ne or a suitable equivalent. dissipators must be carefully designed and

	groundwater table/bedrock or karst is identified). HSG-C or D soils typically require an underdrain, whereas HSG-A and B soils generally do not. Provide the results of soil infiltration rate testing to confirm a minimum subsoil infiltration rate of > 0.5 inch/hour to avoid the use of an underdrain. Use the infiltration test procedures provided in Appendix 8-A in Stormwater Design Specification No. 8 (Infiltration). Confirm the depth to the seasonal high groundwater table (minimum 2 ft. below the design bottom of the facility, or 1 ft. if in a coastal area and an underdrain is used that has a minimum slope of 0.5% and is connected to the drainage system). NOTE: Wet Swales are preferred in coastal plain settings. Confirm the depth to bedrock (minimum 2 ft. below the design bottom of the facility) If karst is present, a detailed geotechnical investigation is recommended to ensure the installation does not aggravate potential karst impacts (e.g., sinkholes, etc.) and an impermeable liner (recommend a min. 30 mil PVC Geo-membrane liner covered by 8 to 12 oz./sq. yd. non-woven geotextile) and underdrain must be place beneath the Dry Swale (Level 1 design only). Identify potential conflicts with other (existing?) structural components (pipes, underground utilities, etc.). Consult local utility design criteria for the horizontal and vertical clearance between
	Utilities and swales. Utilities can cross linear swales if they are specially protected (e.g., double casing). Water and sewer lines generally need to be placed under road pavements to enable the use of adjacent Dry Swales. The bottom elevation of a swale should be a minimum 1 foot below the invert elevation of any adjacent road bed. Dry Swales should be located so as to avoid inputs of springs, irrigation water, chlorinated wash water, or other dry weather flows.
II. C	COMPUTATIONS
A. H	Determine the runoff curve number (pre- and post-developed conditions), providing the worksheets. Determine the time of concentration (pre- and post-developed conditions), providing the worksheets. Generate hydrograph (pre- and post-developed conditions) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method) Confirm that there is adequate drainage area and/or base flow
B. H	The treatment volume must be completely filtered within a maximum of 6 hours following a storm. Typically require 3 to 5 feet of hydraulic head (between the inflow point and the downstream storm drain invert). The swale must be designed with enough capacity to: Convey runoff from the 2-year and 10-year design storms at non-erosive velocities with at least 3 inches of freeboard. Contain the 10-year flow within the banks of the swale (tends to drive the surface dimensions). The bottom width and slope must be designed so that the velocity from a 1-inch rainfall will not exceed 3 ft./sec. (check dams can be incorporated to reduce flow volume and velocity)
	 Specify assumptions and coefficients used. Provide a stage-storage table and curve Provide storm drainage and hydraulic grade line calculations (evaluate the flow profile through the channel at normal depth, as well as flow depth over the top of check dams). Account for any check dams placed within the swale

C. —	Water Quality Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet) Determine specific sizing/dimensions from criteria in Stormwater Design Specification No. 10.
III.	PLAN REQUIREMENTS
A.	BMP Plan View Information
	Show limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier. Show the locations and dimensions of pre-treatment practices: A grass filter strip for a Dry Conveyance Swale For a Dry Treatment Swale, may use a variety of pre-treatment practices, depending on they type of flow entering the swale, with one at each inflow point to the swale (to trap coarse sediment to prevent clogging of the filter media). Layout and dimensions of Dry Swale. NOTE: The maximum contributing drainage area for a Dry Swale is 5 acres (preferably less); a Dry Swale should be approximately 3% to 10% of the size of the CDA, depending on the amount of impervious cover. Dry Swales are not subject to normal building setbacks, given their position in the landscape. Runoff originating from hotspot sources should not be treated by Level 2 (infiltrating) Dry Swales; an impermeable liner should be used. Proper geometry and orientation to avoid short-circuiting: A parabolic cross-sectional shape is preferred for hydraulic, maintenance and aesthetic purposes; a trapezoidal shape may be used as long as the soil filter bed boundaries lay in the flat bottom of the swale Side slopes should be no steeper than 3H:1V to facilitate ease of mowing; flatter slopes are encouraged, where space is available, to enhance pre-treatment of sheet flows entering the swale. Dry Swales should have a bottom width of from 4 to 8 feet to provide adequate filtering area; if the swale will be wider than 8 feet, the designer should incorporate berms, check dams, level spreaders or multi-level cross-sections to prevent braiding and erosion of the swale bottom. The longitudinal slope should be relatively flat (2% or less for a Level 1 design, and 1% or less for a Level 2 design), to allow for temporary ponding of the treatment volume within the channel. The minimum recommended slope is 0.5% (unless the swale is off-line, similar to a bioretention facility), but slope
	Adequate maintenance access to the facility

B. BMP Section Views & Related Details

	Sections through pre-treatment practices.
	Elevations of treatment volume and maximum design water surface elevations for all appropriate
	design storms and safety storms; the maximum ponding depth is a Dry Swale should not
	exceed 12 inches at the most downstream point.
	Adequate freeboard
	Swale bank elevations: constructed height and settled height (allowing for 10% settlement).
	Typical grading section through the facility, showing basin bottom slope
	Underdrain, if applicable:
	Underdrains are provided to ensure Dry Swales drain properly after storms.
	Underdrains must be 6-inch Schedule 40 PVC with 3/8-inch perforations and clean-outs;
	use non-perforated pipe to connect to the storm drain system.
	Install the underdrain with two layers of stone:
	A 12-inch deep underdrain stone layer must be composed of 1-inch clean,
	double-washed stone (VDOT #57 aggregate) free of all soil and fines, with the
	underdrain set 4 inches above the bottom of this layer of stone. NOTE: The
	depth of this storage layer (9 to 18 inches) will depend on the target treatment
	and storage volumes needed to meet water quality, channel protection, and/or
	flood protection criteria.
	In cold climates, extend the underdrain pipe below the frost line and oversize
	the pipe by one pipe size, to reduce the risk of freezing.
	Choker layer: A 2 to 4-inch layer of sand laid over a 2 inch layer of VDOT #8 or #89 choker
	stone (washed gravel) laid above the underdrain encasement stone layer and immediately
	below the filter layer.
	Observation well(s):
	Installed along the length of the swale, if the contributing drainage area exceeds 1 acre.
	Wells should be tied into any T's or Y's in the underdrain system.
	Each well should be flush with the ground surface, with a vented cap.
	Filter media:
	Depth: minimum 18 inches above choker stone layer.
	Media mixed on-site (for smaller applications) or supplied by an approved vendor.
	P-index: Between 20 and 30 for a media mix, OR between 7 and 21 mg/kg of P in the
	soil media (see Section 6.6 of Stormwater Design Specification No. 9)
	Cation Exchange Capacity (CEC): Soils with a CEC exceeding 10 are preferred for
	pollutant removal.
	Infiltration Rate: Between 1 to 2 inches per hour
	Media mix: Equivalent to loamy sand, with the following consistent, homogenous
	composition:
	85% to 88% sand
	8% to 12% soil fines
	3% to 5% organic matter
	Alternative: Use 100% sand for the first 18 inches of the filter, and add a
	combination of topsoil and leaf compost for the top 4 inches, where turf cover
	will be maintained.
	The volume of the media mix should be 110% of the product of the surface area
	and the media depth, to account for settling.
	Filter fabric (side slopes):
	Non-woven polyprene geotextile with a flow rate of > 110 gal./min./sq. ft. (e.g., Geotex
	351 or equivalent).
	Apply immediately above the underdrain only.
-	Topsoil should be a 4-inch layer of loamy sand or sandy loam texture, with less than 5% clay
	content, a corrected pH of 6 to 7, and at least 2% organic content.
	Surface cover should be turf (as specified in the landscaping plan) or river stone.

Made of non-erosive material such as pressure-treated logs or timbers, wood from water-resistant tree species such as cedar, hemlock, swamp oak or locust, gabions, riprap, or concrete. Check dams must be firmly anchored into the side slopes to prevent outflanking and be stable during the 10-year design storm. The height of the check dam relative to the normal channel elevation should not exceed 12 inches. For greater than 12-inch high check dams or swale slopes greater than 4%, special features such as drop structures are required to ensure non-erosive flows. Each check dam should have a minimum of one weep hole or a similar drainage feature so it can dewater after storms (for slopes less than 2%, at least 3 weep holes in each check dam). Soil plugs, appropriate for Dry Swales of 4% or steeper slopes or with 12-inch high check dams, but hydrostatic pressure from the upstream ponding. Erosion control fabric for side slopes: where flow velocities dictate, use woven biodegradable erosion control fabric for side slopes: where flow velocities dictate, use woven biodegradable erosion control fabric for side slopes: where flow velocities dictate, use woven biodegradable erosion control fabric for side slopes: where flow velocities dictate, use woven biodegradable erosion control fabric for side slopes: where flow velocities dictate, use woven biodegradable erosion control fabric for side slopes: where flow velocities dictate, use woven biodegradable erosion control fabric for mats (EC2) that are durable enough to last at least two growing seasons. C. Landscape Plan Provide a planting schedule and specifications (transport / storage / installation / maintenance) Plant selection must be appropriate for the site's vegetation climatic zone (4-8 in Virginia) Where Dry Swales receive runoff from road surfaces in areas of cold climate, they should be planted with sall-tolerant grass species. The construction contract should include a Care and Replacement Warranty that specifies a minimum survival for species planted		Check dam details:
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Store materials in a protected area to keep them free from mud, dirt and other foreign materials. Obtain filter media from an approved vendor and store it on an adjacent impervious area or on plastic sheeting. Where Dry Swales are constructed in the road or right-of-way, the construction sequence may need to be adjusted to account for traffic control, pedestrian access and utility notification. Construction sequence: Construction inspections should occur before, during and after installation to ensure the bioretention facility is constructed according to specifications. Use detailed inspection checklists that require sign-offs by qualified individuals		Showing the proper procedures for converting the temporary sediment controls to a permanent Dry Swale, including dewatering, cleanout and stabilization.
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Construction inspections should occur before, during and after installation to ensure the bioretention facility is constructed according to specifications. Use detailed inspection checklists that require sign-offs by qualified individuals		Where Dry Swales are constructed in the road or right-of-way, the construction sequence may need to be adjusted to account for traffic control, pedestrian access and utility notification.
		Construction inspections should occur before, during and after installation to ensure the bioretention facility is constructed according to specifications.
plan is consistent with the designer's intent. Check the proposed site for existing utilities prior to any excavation.		at critical states of construction, to ensure the contractor's interpretation of the plan is consistent with the designer's intent.

After the first big storm, verify whether the sheet flow, shallow concentrated flow or fully concentrated flow assumed in the plan actually occurred in the field and verify that the swale drains completely within 6 hours. Adjust the plan as
necessary.
 The designer and the installer/contractor should have a pre-construction meeting,
checking the boundaries of the CDA and the actual inlet elevations to ensure they conform to the original design.
The designer should clearly communicate, in writing, any project changes
determined during the pre-construction meeting to the installer and the plan
review/inspection authority.
Construction of the bioretention facility should begin only <i>after</i> site work is completed
 and the entire contributing drainage area has been stabilized with dense and healthy
vegetation.
 It will be necessary to divert flow while the Dry Swale is being constructed, until the filter
bed and side slopes are fully stabilized.
 Temporary E&S control measures (typically silt fence, diversion berms, EC fabric, etc.)
to prevent sediment from moving into the filter media or stone base material during
construction), to avoid clogging (particularly if the practice relies on infiltration), and to protect the facility's vulnerable side slopes from erosion during construction.
Ensure that pre-treatment structures are properly installed and working effectively.
 Excavators or backhoes (with arms with adequate extension) should work from the
 sides to excavate the reservoir layer to its appropriate design depth and dimensions.
Rip, roto-till or otherwise scarify the swale's bottom soils to promote greater infiltration.
Correctly install geotextile fabric on the side slopes.
When laying out the geotextile, the width should include sufficient material to
compensate for perimeter irregularities in the trench and for a 6-inch minimum
overlap at the top of the excavation.
Place stones or other anchoring objects on the fabric at the trench sides to keep
the trench open during windy periods.
 Install and anchor the observation well(s) and, if used, install the underdrains. Check elevations (underdrain inverts, inflow and outflow point inverts, depth of
aggregate installations, etc.) and the surface slope.
Check aggregate material prior to installation to confim that it is clean and
washed and meets specifications.
Provide the correct depth and type of aggregate layers above and below the
underdrains.
Up-gradient ends of underdrains in the reservoir layer should be capped, but
not the downstream ends.
Ensure there are no perforations in clean-outs and observation wells within 1
foot of the surface.
 Place the filter media by hand (to avoid compaction and maintain porosity) in 12-inch lifts, with no machinery allowed directly on the media surface during or after
construction, until the design top elevation is achieved.
Overfill the media above the proposed finished surface elevation to allow for
natural settling. Lifts may be lightly watered to encourage settling.
After the final lift is placed, rake the media to level it, saturate it, and allow it to
settle for at least a few days prior to installing plant materials. Check for
settlement and add additional media, if needed, to achieve the design elevation.
 Install check dams, driveway culverts and internal pre-treatment features, as specified in
the plan.
 Install erosion control fabric, prepare planting holes for any trees and shrubs, install the
vegetation, and water accordingly. Install any temporary irrigation equipment.
 Install the plant materials as shown in the landscaping plan, and water them during
 weeks of no rain for the first two months following installation.

	The construction contract should include a Care and Replacement Warranty to ensure that vegetation is properly established and survives during the firs growing season following construction. Implement any remaining permanent stabilization measures. Log the GPS coordinates for each facility and submit them for entry into the local BMF maintenance tracking database.
E. 	aintenance Items (can include BMP Operation & Maintenance Inspection Checklists from hapter 9, Appendix 9-C of this Handbook) Provide a Maintenance Agreement, indicating the person or organization responsible for maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist. Include a Maintenance Narrative which describes the long-term maintenance requirements of the facility and all components, including removal and disposal of trash debris and sediment accumulations, periodic replacement of soil media, care of the vegetation, and mowing. Record a deed restriction, drainage easement, and/or other enforceable mechanism, including GPS coordinates of the area, to ensure the dry swale areas are not disturbed or converted to other uses. Provide sufficient facility access from the public ROW or roadway to both the bioretention facility and any pre-treatment practices.
IV.	OMMENTS
	By: Date:

8-A.12.0. WET SWALES: DESIGN CHECKLIST

(NOTE: Think of this practice as a linear constructed wetland)

Plan Submission Date	
Project Name	
Site Plan/Permit Number	
Practice No./Location on Site	
Owner_	Phone Number
BMP Designer Constructor	Phone Number
General Contractor	Priorie Number
Signature and stamp of licensed certification	professional design consultant and owner
Plan Status	
	end: _ 🗓 - Complete
Not Approved	Inc Incomplete/Incorrect
	N/A - Not Applicable
Facility Type: Level 1	Level 2
Hydraulic Configuration:	Type of pretreatment facility:
☐ On-line facility☐ Off-line facility	☐ Check Dams (channel flow)
☐ Oil-line facility	☐ Tree Check Dams (channel flow)
	☐ Grass Filter Strip (sheet flow)
	☐ Gravel or Stone Diaphragm (sheet flow)
	☐ Gravel or Stone Flow Spreaders
	(concentrated flow)
	☐ Other:
	□ None
	- None
I. SUPPORTING INFORMATION	
I. SUFFORTING INFORMATION	
Provide a concise narrative describing the	e stormwater management strategy, describing how
this practice fits into the overall plan, and st	
Show the location of this BMP on the site m	nap, including the following:
Swale area	
Contributing drainage area (CDA) to	boundaries and acreage (should not exceed 5 acres).
Delineation of FEMA 100-year floor Areas of site compensated for in war	
	ng that the slope of the CDA is between 1% and 2%.
	the effective slopes of the swale and lengthen the
contact time to enhance treatment.	
	the Regenerative Conveyance System (RCS), which
	nrough a series of step pools that provide treatment
(see Stormwater Design Specificat	
Provide a soil map for site and area of facili	
	boring logs with Unified Soils Classifications and
. ,	taken to confirm the underlying soil properties). Wet
Swales work best when constructed over the	
Confirm the depth to the seasonal high group	
nollutant removal and increase exc	wales to intersect the water table; this may reduce

		Identify potential conflicts with other (existing?) structural components (pipes, underground utilities, etc.). Wet Swales are not recommended for the following situations: To treat runoff from stormwater hotspots, due to the potential interaction with the water table and the risk that hydrocarbons, trace metals and other pollutants could migrate into the groundwater. Karst areas. Residential areas, due to the risk of mosquito breeding.
II.	CON	IPUTATIONS
A.	Hydı	rology
		Determine the runoff curve number (pre- and post-developed conditions), providing the worksheets.
		Generate hydrographs (pre- and post-developed conditions) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method) Determine the time of concentration (pre- and post-developed conditions), providing the worksheets. Confirm that there is adequate drainage area and/or base flow.
_		
В.	Нуа	raulics If designed as an on-line practice (Level 1 design), the swale must be designed with enough capacity to:
		Convey runoff from the 2-year and 10-year design storms at non-erosive velocities with
		adequate freeboard. Contain the 10-year flow within the banks of the swale with adequate freeboard. (tends to drive the surface dimensions).
		If designed as an off-line practice (Level 2 design), a bypass or diversion structure must be designed to divert the large storm (e.g., when the flow rate and/or volume exceeds the treatment volume) to an adequate channel or conveyance system. The Wet Swale is then designed to meet the volume, velocity and residence time criteria
		for Wet Swales are designed based on peak flow rate – the maximum flow velocity of the channel
		must be less than 1 foot per second during a 1-inch water quality storm event. The longitudinal slope of the channel should, ideally, be between 1% and 2% in order to avoid scour and short-circuiting within the channel; longitudinal slopes up to 4% are acceptable, but check dams will be necessary to reduce the effective slope in order to meet the limiting velocity requirements)
		Verify hydraulic capacity using Manning's Equation or an accepted equivalent method, such as
		erodibility factors and vegetal retardance The flow depth for the peak treatment volume (1-inch rainfall) should be maintained at 3 inches or less
		Manning's "n" value for grass channels should be 0.2 for flow depths up to 4 inches, decreasing to 0.03 at a depth of 12 inches (which applies to the 2-year and 10-year storms if an on-line application
		Peak flow rates for the 2-year and 10-year frequency storms must be non-erosive or subject to site-specific analysis of the channel lining material and vegetation The 10-year peak flow rate must be contained within the channel banks, with a minimum of 6 inches of freeboard
		Specify assumptions and coefficients used.
		Provide a stage-discharge table and curve (provide equations). Route post-development hydrographs for appropriate design storms (2-yr., 10-yr., or as required by watershed conditions) and safety storms (100-yr. or as required)
		Provide storm drainage and hydraulic grade line calculations. Calculations for peak flow depth and velocity should reflect any increase in flow along the length of the channel, as appropriate. If a single flow is used, the flow at the outlet should be used.

		The hydraulic residence time should be minimum of 9 minutes for the treatment volume (1-inch rainfall) design storm. If flow enters the channel at multiple locations, a 9-minute minimum hydraulic residence time should be demonstrated for each entry point, using equations in Stormwater Design Specification No. 3 (Grass Channels).
C	Wate	er Quality
		Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet) Indicate the treatment volume for extended detention (if added) with draw-down calculation Determine specific sizing/dimensions from criteria in Stormwater Design Specification No. 11.
III.	PLA	N REQUIREMENTS
Α.	ВМР	Plan View Information
		Show the limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier. Show the locations and dimensions of pre-treatment practices and all conveyance system outfalls into the swale
		Wet Swales are not subject to normal building setbacks, given their position in the landscape. Show the layout and dimensions of the Wet Swale.
		A Wet Swale should be approximately 5% to 15% of the size of the CDA, depending on the amount of impervious cover (NOTE: The maximum contributing drainage area for a Wet Swale is 5 acres).
		Surface dimensions are largely determined by the need to pass the 10-year design storm.
		The minimum length may be achieved with multiple swale cells connected by culverts with energy dissipators.
		Ensure the proper geometry and orientation, to avoid short-circuiting: A parabolic cross-sectional shape is preferred for hydraulic, maintenance and aesthetic purposes; a trapezoidal shape may be used as long as the soil filter bed boundaries lay in the flat bottom of the swale
		Side slopes should be no steeper than 4H:1V to enable wetland plant growth; flatter slopes are encouraged, where space is available, to enhance pre-treatment of sheet flows entering the swale. Under no circumstances are the side slopes to be steeper than 3H:1V.
		Wet Swales should have a bottom width of from 4 to 8 feet to provide adequate filtering area; if the swale will be wider than 8 feet, the designer should incorporate berms, check dams, level spreaders or multi-level cross-sections to prevent braiding and erosion of the swale bottom.
		Indicate the top-of-bank and swale bottom elevations
		Indicate the elevations of treatment volume and maximum design water surface elevations for all
		appropriate design storms and safety storms. The average normal pool depth (dry weather) throughout the swale should be 6 inches
		or less. The maximum temporary ponding depth in any single wet Swale cell should not exceed 18 inches at the most downstream point (e.g., at a check dam or driveway culvert).
		Show the location of check dams, if applicable: Stone energy dissipators are required at the downstream toe of check dams to prevent
		erosion. The check dam must be designed to spread runoff evenly over the Wet Swale's surface, through a depressed weir (in the center of the check dam) with a length equal to the bed width (sized to convey the depth of flow for the appropriate design storm).
		Check dams must be spaced correctly: Cells formed by check dams or driveways should be at least 25 to 40 feet in length.

	Check dams should also be spaced as needed to maintain the effective longitudinal slope of 2% for Level 1 Wet Swales or 1% for Level 2 Wet Swales. Show adequate maintenance access to the facility
В.	BMP Section Views & Related Details
	Show cross-sections through the swale, showing: Various water surface elevations (treatment volume and maximum design water surface elevations for all appropriate design storms and safety storms) and adequate freeboard. Side slopes, top width, swale bank elevations: constructed height and settled height (allowing for 10% settlement). Wetland planting areas.
	Ensure the proper geometry: Wet Swales should be designed with a trapezoidal or parabolic cross-section. A parabolic shape is preferred for aesthetic, maintenance and hydraulic reasons. Side slopes should be no steeper than 4H:1V to enable wetland plant growth; flatter slopes are encouraged, where space is available, to enhance pre-treatment of sheet flows entering the swale. Under no circumstances are the side slopes to be steeper than 3H:1V.
	The longitudinal slope should be relatively flat (2% or less for a Level 1 design, and 1% or less for a Level 2 design), to allow for temporary ponding of the treatment volume within the channel. The minimum recommended slope is 0.5% (unless the swale is off-line), but slopes up to 4% are acceptable if check dams are used.
C	Check Dams Check dams should be composed of wood, concrete, stone, or other non-erodible material, or should be configured with elevated driveway culverts. Check dams should be underlain with filter fabric conforming to the following standards: Needled, non-woven, polypropylene geotextile. Grab Tensile Strength (ASTM D4632): ∃ 120 lbs. Mullen Burst Strength (ASTM D3786): ∃ 225 lbs./sq. in. Flow Rate (ASTM D4491): ∃ 125 gpm/sq. ft.
	 Apparent Opening Size (ASTM D4751): ∃ US #70 or #80 sieve Wood used for check dams should consist of pressure-treated logs or timbers, or water-resistant tree species such as cedar, hemlock, swamp oak or locust. It is necessary to compute check dam materials, based on the surface area and depth used in the design computations. Check dams should be spaced based on the channel slope, as needed to increase residence time and provide adequate storage for the treatment volume (1-inch rainfall) or any additional volume attenuation requirements. The ponded water at a downhill check dam should not touch the toe of the upstream check dam.
	The maximum desired check dam height is 12 inches (for maintenance purposes). However, for challenging sites, a maximum of 18 inches can be allowed, with additional design elements to ensure the stability of the check dam and the adjacent and underlying soils The average ponding depth throughout the channel should be 12 inches. Armoring may be needed at the downstream toe of the check dam to prevent erosion. Check dams must be firmly anchored into the side-slopes to prevent outflanking; check dams must also be anchored into the channel bottom so as to prevent hydrostatic head from pushing out the underlying soils. Check dams must be designed with a center weir sized to pass the channel design storm peak
	flow (10-year storm event for man-made channels). Each check dam should have a weep hole or similar drainage feature so it can dewater after storms.

	Individual channel segments formed by check dams or driveways should generally be at least 25 to 40 feet in length.
D.	Diaphragms Pea gravel used to construct pre-treatment diaphragms should consist of washed, open-graded, course aggregate between 3 and 10 mm in diameter and must conform to local design standards.
E.	Landscape Plan Provide a planting schedule and specifications (transport / storage / installation / maintenance) Select plant materials appropriate for the site's vegetation climatic zone (6-8 in Virginia), emphasizing native plant materials. Plant materials must be able to withstand both wet and dry periods as well as relatively high velocity flows within the swale. Wet Swales should be planted with wet-footed species, such as sedges or wet meadow vegetation. If the swale is adjacent to a roadway where winter conditions will require the use of road solve in the CDA, then solt telerant non weady plant species should be specified.
	salts in the CDA, then salt-tolerant non-woody plant species should be specified. It may be advisable to incorporate sand or compost into the surface soils to promote a better growing environment. Specify preservation measures for existing vegetation The construction contract should include a <i>Care and Replacement Warranty</i> that specifies a minimum survival for species planted of 75% after the first growing season, and a minimum effective ground cover of 75% for flat roofs and 90% for pitched roofs.
D.	Construction Notes Ideally, planned Wet Swale areas should be clearly marked off and remain <i>outside</i> the limits of land disturbance during construction to prevent soil compaction by heavy equipment. However, this is seldom practical, since swales are a key part of the natural drainage system at most sites. Therefore, temporary E&S controls such as dikes, silt fences, etc. should be integrated into the swale design throughout the construction sequence. Specifically, barriers should be installed at key check dam locations, and E&S control fabric should be used to protect the channel bottom. Wet Swale areas <i>may</i> be used during construction as sites for temporary sediment traps or basins, provided the construction plans include notes and graphical details specifying the
	following: The maximum excavation depth at the construction stage must be at least 1 foot above the post-construction installation. Show the proper procedures for converting the temporary sediment controls to a permanent Wet Swale, including dewatering, cleanout and stabilization. Wet Swale construction should begin only after the entire contributing drainage area has been stabilized with vegetation. Sediment accumulation must be removed during final grading to
	achieve the design cross-section. Ideally, Wet Swales should be constructed during months that are best for establishing vegetative cover without irrigation (February 15 – April 15; September 15 – November 15). It will be necessary to divert flow while the Wet Swale is being constructed, until the bed and side slopes are fully vegetated. Show applicable temporary E&S control measures.
	Construction sequence for BMP(s) and E&S controls: Construction inspections should occur before, during and after installation to ensure the stormwater wetland is constructed according to specifications. Use detailed inspection checklists that require sign-offs by qualified individuals at critical states of construction, to ensure the contractor's interpretation of the plan is consistent with the designer's intent.

	Check the proposed site for existing utilities prior to any excavation. Install applicable temporary E&S Controls prior to construction. Grade the channel to the final dimensions shown on the plan. Install check dams, driveway culverts and internal pre-treatment features as shown on the plan
	Fill material used to construct the check dams should be placed in 8- to 12-inch lifts and compacted to prevent settlement. The top of each check dam should be constructed level at the design elevation.
	 (Optional) Till the bottom of the channel to a depth of 1 foot and incorporate compost amendments according to Stormwater Design Specification No. 4. Planting soil should be loam or sandy loam with a high organic content, placed by mechanical methods, and spread by hand to a depth of at least 4 inches for shallow
	wetlands. ———— Planting soil should be tamped as directed in the design specifications, but it
	should not be overly compacted.
	After the planting soil is placed, it should be saturated and allowed to settle for at least one week prior to installation of plant materials. No machinery should be allowed to traverse over the planting soil during or after
	construction. Redirect previously diverted flows into the Wet Swale to allow it to fill up to normal pool
	elevation.
	Wetland planting areas should be at least partially inundated during planting to promote plant survivability.
	Surveyed planting zones should be marked on the as-built or design plan, and the locations should be identified in the field, using stakes or flags.
	Propagate the stormwater wetland between mid-April and mid-June, using three simultaneous techniques to propagate the emergent community over the wetland bed: Initial planting of container-grown wetland plant stock.
	Broadcast wetland seed mixes over the higher wetland elevations, to establish diverse emergent wetlands.
	Seeding of Switchgrass or wetland seed mixes as a ground cover is recommended for all zones above 3 inches below the normal pool elevation.
	Hand broadcasting or hydroseeding can be used to spread seed, depending on the size of the wetland cell.
	After initial planting, a biodegradable E&S control fabric may be used, conforming to Standard and Specification 3.36 of the VESCH.
	Prepare planting holes for any trees and shrubs, then plant materials as shown in the landscaping plan and water them weekly in the first two months.
	Install goose protection for newly planted or newly growing vegetation, especially emergents and herbacious plants.
	Place netting, webbing, or string installed in a criss-cross pattern over the surface area of the wetland above the level of the emergent plants.
	 Implement any remaining permanent stabilization measures. Conduct a final inspection, log the GPS coordinates for each facility and submit them for entry into the local BMP maintenance tracking database.
	stenance Items (can include BMP Operation & Maintenance Inspection Checklists from
Cha	oter 9, Appendix 9-C of this Handbook) Provide a Maintenance Agreement, indicating the person or organization responsible for
	maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist.
	Include a Maintenance Narrative which describes the long-term maintenance requirements of the facility and all components, including removal and disposal of trash, debris and sediment accumulations, and care of the vegetation.

	 Record a deed restriction, drainage easement, and/or other enforceable mechanism, including GPS coordinates of the area, to ensure the wet swale area is converted to other uses. Provide sufficient facility access from the public ROW or roadway to both the wet pond and any pre-treatment practices.
IV.	COMMENTS
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	By: Date:

8-A.13.0. FILTERING PRACTICES: DESIGN CHECKLIST

Plan Submission DateProject Name		
Site Plan/Permit Number		
Owner		
BMP Designer		Phone Number
General Contractor		
Signature and stamp of licens certification	sed professio	onal design consultant and owner
Plan Status		
Approved Not Approved	Legend:	Inc Complete Inc Incomplete/Incorrect N/A - Not Applicable
Facility Type: Level 1	Le	vel 2
Facility Type: G Non-Structural Sand Filter G Surface Sand Filter Organic Media Filter Underground Sand Filter Proprietary Filter Other:	G	eatment: Wet or Dry Sedimentation Chamber designed as level spreaders and sized to accommodate 25% of the treatment volume Forebay
Hydraulic Configuration:		Compost-amended grass filter
☐ On-line facility		path
☐ Off-line facility		Gravel Diaphragm
☐ FILTER TREATS HOSPOT RUNOFF		Check Dam Engineered Level Spreader Proprietary device Other:
this practice fits into the overall plan, a Show the location of this BMP on the s Filter facility area Contributing drainage area (C Delineation of FEMA 100-year Areas of site compensated for Provide topography of the site area. Provide a soil map for site and area of Provide the soil boring locations and soil descriptions (at least one boring m At least one soil boring must l filtering practice to establish t suitability Confirm that there is a minim high groundwater table and/or	and stating all as site map, including DA) boundaries, refloodplain rein water quality facility, including the soil boring lenust be taken to be taken at a low the depth to grow aum of 2 feet sembled be taken and the geotechnical investigation.	acreage and land cover calculations g the CDA logs with Unified Soils Classifications and confirm the underlying soil properties). V point within the footprint of the proposed undwater/bedrock and to evaluate the soil paration distance between the seasonally be bottom invert of the filtering practice. Vestigation is recommended to ensure the

		tify potential conflicts with other (existing?) structural components (pipes, underground
		ies, etc.). cial conditions:
	Spe	Filters work well in karst areas, assuming that they are water tight and that excavation
		does not extend into a karst layer.
		In coastal plain settings, the Perimeter Sand Filter and the Non-Structural Sand Filter
		work best, subject to the following criteria:
		The combined depth of the underdrain and sand filter bed can be reduced to
		from 24 to 30 inches
		Consider maximizing the length of the filter or provide treatment in multiple
		connected cells The minimum depth to seasonally high groundwater may be relaxed to 1 foot,
		as long as the filter is equipped with a large diameter underdrain (e.g., 6 inches)
		that is only partially efficient at dewatering the filter bed.
		Maintain an underdrain slope of at least 0.5% to ensure positive drainage and to
		tie it into the receiving ditch or conveyance system.
		In steep terrain:
		Slope gradient contributing runoff to sand filters can be increased to 15%, as long as a two-cell, terraced design is used to dissipate erosive energy prior to
		the filter.
		The drop in elevation between cells should be limited to 1 foot and the slope
		should be armored with river stone or a suitable equivalent.
		In cold climate of for winter performance (problem is ice forming over the filter bed):
		Place a weir between the pre-treatment chamber and filter bed to reduce ice
		formation.
		 Extend the filter bed below the frost line to prevent freezing within the filter bed. Oversize the underdrain to encourage more rapid drainage and to minimize
		freezing of the filter bed.
		Expand the sediment chamber to account for road sand. Pre-treatment
		chambers should be sized to accommodate up ot 40% of the treatment volume.
II.	COMPUT	ATIONS
Δ	Hydrolog	nv
Λ.		ermine the runoff curve number (pre- and post-developed conditions), providing the
		ksheets.
		ermine the time of concentration (pre- and post-developed conditions), providing the
		ksheets.
		erate hydrographs (pre- and post-developed conditions) for appropriate design and safety
	Stor	ms (USDA-NRCS methods or modified rational-critical storm duration method)
В.	Hydrauli	CS
		hydraulic head required for filters varies from 2 to 10 feet, depending on the design variant;
		cient hydraulic head is critical to the proper function of filtering systems.
		firm that the design will result in the facility dewatering within 40 hours after a storm event.
		cify the assumptions and coefficients used.
		ride a stage-storage table and curve ride for large storm overflow or bypass
		ride for large storm overflow or bypass ride storm drainage and hydraulic grade line calculations.
	1 10	nao storm aramago ana nyaraano grado imo odiodiationo.
C.	Water Qu	uality
	A m	aximum contributing drainage area (CDA) of 5 acres is recommended for surface sand
		s, and a maximum CDA of 2 acres is recommended for perimeter or underground filters, to
	min	mize clogging.

	Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA. For Level 1 designs, the contributing drainage area may contain some pervious area; for Level 2 designs, the CDA must be nearly 100% impervious (preferred condition). Determine the pollutant load, pollutant load removal, and treatment volume requirements, generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet). Keep in mind that Level 2 designs are sized for a treatment volume that is 25% greater than for Level 1 practices.
	Also, keep in mind that for Level 2 designs, the runoff reduction value (normally 0) may be increased if a second cell is used for infiltration or bioinfiltration (Bioretention Level 2). The RR credit should be proportional to the fraction of the treatment volume designed to be infiltrated. Determine specific sizing/dimensions from criteria in Stormwater Design Specification No. 12.
III.	PLAN REQUIREMENTS
A. 	Show the limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier. Show the layout and dimensions of the filtering facilities (one cell for Level 1 design; two cells for Level 2)
	Sand and organic surface filters typically consume approximately 2% to 3% of the CDA, while perimeter sand filters typically consume less than 1% of the CDA. Underground filters generally consume no surface area except for their manholes. NOTE: Surface area and storage volume of the filter media relates to the treatment volume (Equations 12.1 and 12.2 in Stormwater Design Specification No. 12) Ensure proper orientation to avoid short-circuiting Ensure adequate maintenance access to the facility Show the observation well location
B. —	BMP Section Views & Related Details Details will vary depending upon the type of filter employed:
	Non-Structural Sand Filter – applied to sites less than 2 acres in size and essentially the same as a retention Basin (Stormwater Design Specification No. 9), with the following exceptions: The bottom is lined with an impermeable filter fabric and always has an underdrain. The surface cover is sand, turf or pea gravel (not trees, shrubs, or herbaceous material). The filter media is 100% sand. The filter has two cells, with a dry or wet sedimentation chamber preceding the sand filter bed.
2.	Surface Sand Filter (more economical) Designed with both the filter bed and sediment chamber located at ground level Normally constructed of pre-cast or cast-in-place concrete Usually designed to be off-line facilities, so that only the treatment volume is directed to the filter. Can be installed in the bottom of a dry Extended Detention Basin (see Stormwater Design Specification No. 15).
3.	Organic Media Filter Essentially the same as surface sand filters, except the sand is replaced with an organic filtering medium (e.g., peat/sand filter, leaf compost filter, etc.) that is better at removing metals and hydrocarbons. However, organic media can actually leach soluble nitrate and phosphorus back into the discharge water.
4.	Underground Sand Filter (more expensive, but they consume very little surface area) Filtering components are installed underground

5.	Perimeter Sand Filter (more economical)	
Incorporates a sediment chamber and filter bed, but flow enters through grates, usually edge of a parking lot.		
	bypass by entering an overflow chamber	
	Requires only about 2 feet of hydraulic head, so can be used on sites with little topographic relief	
6.	Proprietary Filters	
٠.	Follow the design criteria provided by the manufacturer	
	Conveyance and Overflow:	
	For off-line filter systems, show the internal flow splitter or overflow device that	
	bypasses runoff from larger storm events around the filter.	
	For on-line filter systems, show how the device will safely pass the local design storm(s)	
	(1-year and/or 10-year storms) without re-suspending or flushing previously trapped material.	
	Ensure that the facility will dewater within 40 hours after a storm event.	
	Filtering practices typically have an impermeable liner meeting the following criteria: Needled, non-woven polypropylene geotextile (do <i>not</i> use heat-set or heat-	
	calendared fabrics)	
	Grab Tensile Strength (ASTM D4632) = \exists 120 lbs.	
	Mullen Burst Strength (ASTM D3786) = ∃ 225 lbs./sq. in.	
	Flow Rate (ASTM D4491) = \exists 125 gpm/sq. ft.	
	Apparent Opening Size (ASTM D4751) = US #70 or #80 sieve.	
	Underdrain:	
	Pipes comply with AASHTO M252 and ASTM F405	
	If the underdrain must meet ASTM F758, it must be perforated with slots that have a maximum width of 3/8-inch and provide a minimum inlet area of 1.76 sq. in. per linear	
	foot of pipe.	
	 If underdrain meets ASTM F949, it must be perforated with slots that have a maximum width of 3/8-inch and provide a minimum inlet area of 1.5 sq. in. per linear foot of pipe. Underdrain pipe with precision-machined slots is preferred to pipe with standard round. 	
	hole perforations.	
	The stone jacket for the underdrain must meet VDOT #57 stone specifications or the ASTM equivalent (1-inch maximum diameter).	
	Filter Media:	
	Normal filter media consists of clean, washed medium aggregate concrete sand with individual grains between 0.2 and 0.04 inches in diameter (AASHTO M-6/ASTM C-33)	
	Organic media can be used, such as a peat/sand mixture or a leaf compost mixture, but	
	this is not recommended unless metals and hydrocarbons are a particular issue in site runoff	
	Surface Cover:	
	For surface sand filters, surface cover should consist of a 3-inch layer of topsoil on top	
	of a non-woven filter fabric laid above the sand layer (pea gravel inlets in the topsoil layer where sheet flow enters, at margins around the filter bed, or at locations in the	
	middle of the bed, to promote infiltration).	
	 For underground sand filters, surface cover should have a pea gravel layer on top of a coarse non-woven filter fabric laid over the sand layer. Media depth can range from 12 to 18 inches. 	
	modic dopin our range from 12 to 10 monot.	

	Mainte	enance Reduction Design Features:	
		Observation wells and cleanouts (facilitates inspection and maintenance) Surface sand filters should include an observation well, consisting of a 6-inch diameter non-perforated PVC pipe fitted with a lockable cap. Install the observation well flush with the ground surface.	
		Typically, a cleanout pipe will be tied into the end of each underdrain pipe run. The portion of the cleanout pipe/observation well in the underdrain layer should be perforated.	
		Provide at least one cleanout pipe for every 2,000 sq. ft. of filter surface area. Good maintenance access must be provided, such that a vacuum truck or similar equipment can get close enough to the sedimentation chamber and filter to perform cleanouts.	
		Installing media depths deeper than 18 inches can facilitate the removal of 1 to 3 inches of sand during maintenance without have to necessarily replace it. Access to the headbox and clearwell of <i>underground</i> sand filters must be provided by	
		manholes at least 30 inches in diameter, along with steps to the areas where maintenance will occur. Install stormwater filters at the site so that inspection and maintenance personnel can easily see them. Provide adequate signs or markings at manhole access points for	
		underground filters. For underground filters, note that special OSHA rules and training apply to protect workers that must access them.	
C.	 Landscape Plan Consider the importance of aesthetics and visual characteristics (foliage form, texture, color etc.) 		
	Consider Con	der visibility, traffic considerations and other safety issues e a planting schedule and specifications (transport / storage / installation / maintenance) selection appropriate for the site's vegetation climatic zone (4-8 in Virginia), emphasizing species.	
	Specif	y preservation measures for existing vegetation applicable, ensure that topsoil / planting soil is included in final grading	
D.	Construction	on Notes	
	basin	ture location of filtering practices may be used as the site of a temporary sediment trap or during site construction, as long as the design elevations are set with final cleanout and rsion in mind.	
		The bottom elevation of the filtering practice should be lower than the bottom elevation of the temporary sediment basin.	
		Appropriate procedures must be implemented to prevent discharge of turbid waters when the temporary basin is converted to the filtering practice. Then the sediment basin must be dewatered, dredged and regraded to the design dimensions for the post-construction stormwater filter.	
		ruction sequence for filtering practices and E&S controls ze the drainage area.	
	Install	Construct filtering practices only <i>after</i> the CDA to the facility is completely stabilized. E&S controls for the filtering practice. It is extremely important that stormwater is diverted around the filtering practice as it is	
		being constructed, in order to prevent sediment from clogging the filter bed during construction.	
		 Install silt fence around the perimeter of the sand filter. Install erosion control fabric on exposed side-slopes with gradients exceeding 4H:1V. Rapidly stabilize exposed soils around the filter by hydro-seed, sod, mulch or other locally-approved method of soil stabilization. 	
		able construction materials, make sure they meet design specifications, and prepare g areas	

 Clear and strip the project area to the desired subgrade. Excavate/grade until the appropriate elevation and desired contours are achieved for the bottom and side slopes of the filtering practice.
_ Install the filter structure Check all design elevations (concrete vaults for surface, underground and perimeter sand filters).
Upon completion of the filter structure shell, plug inlets and outlets temporarily and fill the structure with water to the brim to check for water-tightness (maximum allowable leakage is 5% of the water volume in a 24-hour period). If the structure fails the test, perform repairs to make the structure watertight before any sand is place into it. Install the gravel, underdrains, and choker layer of the filter.
Place the filter media: Spread sand across the filter bed in 1 foot lifts up to the design elevation.
 Manually rake the sand. Add clean water until the sedimentation chamber and filter bed are completely full. Allow the facility to drain, hydraulically compacting the sand layers. After 48 hours of draining and drying, refill the structure to the final top elevation of the
 sand filter bed Filter fabric installation:
Install the permeable filter fabric over the sand Add a 3-inch topsoil layer and pea gravel inlets. Immediately stabilize with permanent grass species.
Water the grass as needed to develop a vigorous grass cover (do not activate the filter system until vigorous cover is present)
apter 9, Appendix 9-C of this Handbook) Provide a Maintenance Agreement, indicating the person or organization responsible for maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist. Include a Maintenance Narrative which describes the long-term maintenance requirements of the facility and all components, including removal and disposal of trash, debris and sediment accumulations, periodic replacement of soil media, care of the vegetation, and mowing. Record a deed restriction, drainage easement, and/or other enforceable mechanism, including GPS coordinates of the area, to ensure the bioretention areas are not disturbed or converted to other uses. Provide sufficient facility access from the public ROW or roadway to both the filtration facility and any pre-treatment practices. To prevent freezing in cold climates and winter weather, require or clearly recommend that filters be inspected before the onset of winter (prior to the first freeze) to dewater wet chambers and scarify the filter surface.

Ву:	Date:

Virginia Stormwater Management Handbook, Chapter 8

8-A.14.0. CONSTRUCTED WETLANDS: DESIGN CHECKLIST

Plan Submission Date	
Project Name	
Site Plan/Permit Number	
Practice No./Location on Site	
Owner	
BMP Designer	
General Contractor	Phone Number
Signature and stamp of licensed profesertification	essional design consultant and owner
Plan Status	
Approved Legend:	Complete
Not Approved	Inc Incomplete/Incorrect N/A - Not Applicable
Facility Type: Level 1	Level 2
Hydraulic Configuration:	Type of Pre-Treatment Facility:
☐ On-line facility	☐ Sediment forebay (above ground)
☐ Off-line facility	☐ Vegetated buffer area
Type of wetlends	☐ Grass filter strip
Type of wetland:	☐ Grass channel ☐ Other:
 Constructed Wetland Basin (Level 1 – emergent)) 	Li Ottier.
□ Constructed multi-cell wetland (Level 2	
emergent and forest)	
 Constructed multi-cell pond/emergent wetland combination (Level 2) 	
I. SUPPORTING INFORMATION	
Provide a concise narrative describing the store this practice fits into the overall plan, and stating Show the location of this BMP on the site map, in	all assumptions made in the design.
sustain a permanent water level within the	
Delineation of FEMA 100-year floodplain	
Areas of the site compensated for in wat	
Provide topography of the site area, including the Provide a geotechnical report with recomme	
description of any borrow area involved	nuations and earthwork specifications and a
Provide a soil map for site and area of facility, sh	owing CDA and facility boundaries
Provide soil boring locations and soil boring I	
descriptions.	proposed embankment, in the vicinity of the
proposed outlet area, and in at least two	o locations within the planned wetland treatment
area Determine the physical characteristics of	the soils regarding:
Suitability for use as structural fi	
Bearing capacity, buoyancy, etc	pertaining to outlet structure design
Compaction/composition needs	for the embankment.
	losses (and the consequent need for a liner).

Depth to bedrock.
Depth to seasonal high groundwater table (NOTE: It is permissible for wet swales to intersect the water table; this may reduce pollutant removal and
increase excavation costs).
 . If karst is present, a detailed geotechnical investigation is recommended to ensure the
constructed wetland does not aggravate potential karst impacts (e.g., sinkholes, etc.):
Must maintain at least 3 feet of vertical separation from the underlying karst layer.
Must employ an impermeable liner that meets the requirements of Stormwater Design
Specification No. 13.
Must use shallow, linear and multiple-cell wetland configurations rather than deep basin
configurations (e.g., a pond/wetland or ED wetland).
Constructed wetlands are ideal for coastal settings with flat terrain, low hydraulic head and high
water table conditions:
Choose shallow, linear and multiple-cell configurations
Acceptable to excavate below the water table, as follows:
6 inches below to provide the requisite hydrology for wetland planting zones.
Up to 3 feet below for micro-pools, forebays and other deep pool features.
The volume below the seasonably high groundwater table may count toward the
Treatment Volume, as long as the other primary geometric and design requirements for
the wetland are met (e.g., flow path, microtopography, etc.)
Plant selection should focus on species that are wet-footed and can tolerate some
salinity.
Consider creating forested wetlands, since a greater range of coastal plain tree species
(Atlantic White Cedar, Bald Cypress, Swamp Tupelo, etc.) can tolerate periodic
inundation.
Consider using the Regenerative Conveyance System (RCS) where there is
considerable drop in elevation from the channel to the outfall location (see Stormwater
Design Specification No. 13).
Constructed wetlands are not effective at sites with steep terrain.
 May be able to terrace wetland cells in a linear configuration, as with the Regenerative
Conveyance System.
Where cold winter climates are typical, make the following adjustments:
 Treat larger runoff volumes in the spring by adopting seasonal operation of the
permanent pool.
Plant salt-tolerant vegetation (to deal with higher chloride content of road salts).
Do not submerge inlet pipes and provide a minimum 1% pipe slope to discourage ice
formation.
Locate low-flow orifices so they withdraw at least 6 inches below the typical ice layer.
Angle trash racks to prevent ice formation.
Over-size the riser and weir structures to avoid ice formation and freezing pipes.
If road sanding is prevalent in the CDA, increase the forebay size to accommodate
additional sediment loading.
Constructed wetlands are generally <i>not</i> recommended in watersheds containing trout streams,
due to the potential for stream warming, unless:
All other upland runoff reduction opportunities have been exhausted.
The Channel Protection Volume has not been provided through other means.
A linear/mixed wetland design is applied to minimize stream warming.
 A constructed wetland should <i>not</i> be built within an existing perennial stream or natural wetland
nor should a constructed wetland discharge to jurisdictional waters without local/state/federal
approvals and the necessary permit(s).
Constructed wetlands built for stormwater management purposes are typically not
considered jurisdictional wetlands, but the designer should confirm this with applicable
wetland regulatory authorities.
Identify potential conflicts with other (existing?) structural components (pipes, underground
 utilities, etc.).

	The designer should check to see whether sediments removed from the forebay can be spoiled
	(deposited) on-site or must be hauled away.
II.	COMPUTATIONS
Α.	 Hydrology Determine the runoff curve number determinations (pre- and post-developed conditions), providing the worksheets.
	Determine the time of concentration (pre- and post-developed conditions), providing the worksheets.
	Generate hydrographs (pre- and post-developed conditions) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method) Ensure that there is adequate drainage area and/or water balance from groundwater, runoff or baseflow so the wetland will not go completely dry after a 30-day summer drought.
В.	Hydraulics
	 Specify assumptions and coefficients used. Typically, 2 to 4 feet of hydraulic head are need to drive flow through the wetland. Provide a stage-storage table and curve
	Weir/orifice control analysis for riser structure discharge openings and riser crest.
	Carefully design the low-flow orifice to minimize clogging, as follows: Recommend a minimum 3-inch diameter orifice to minimize clogging of an outlet or extended detention pipe when it is surface-fed (still susceptible to clogging from floating vegetation and debris).
	 Smaller openings (down to 1-inch in diameter) are permissible, using internal orifice plates within the pipe. All outlet pipes should be adequately protected by trash racks, half-round CMP, or reverse-sloped pipes extending to mid-depth of the micropool.
	Barrel: conduct an inlet/outlet control analysis Conduct a riser/outlet structure flotation analysis (factor of safety = 1.25 min.).
	Provisions for use as a temporary sediment basin riser with clean out schedule & instructions for conversion to a permanent facility.
	Conduct an emergency spillway adequacy/capacity analysis (100-year design storm) with required embankment freeboard.
	Provide for large storm overflow or bypass Provide a stage-discharge table and curve (provide equations).
	Route post-development hydrographs for appropriate design storms (1-yr., 10-yr., or as required by watershed conditions) and safety storms (100-yr. or as required) Provide storm drainage and hydraulic grade line calculations.
	Frovide storm drainage and riyuradiic grade line calculations.
C.	Downstream impacts
	Conduct a danger reach study. Evaluate 100-year floodplain impacts.
	Provide downstream hydrographs at critical study points.
	Demonstrate safe conveyance to an "adequate" receiving channel.
	If the receiving channel is natural and (1) has never been enhanced or "restored, OR (2) if stream channel erosion or localized flooding is an existing predevelopment condition, then conduct appropriate "energy balance" calculations to demonstrate safe conveyance from the facility to the receiving channel" (provide computations).

D.	Water Quality
	Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet) Calculate the treatment volume for extended detention (if added) with draw-down calculation Determine specific sizing/dimensions from criteria in Stormwater Design Specification No. 13.
III.	PLAN REQUIREMENTS
A.	BMP Plan View Information Show limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier. Setbacks (Note: local codes rule): Minimum 10 feet from property lines. Minimum 25 feet from building foundations. Minimum 50 feet from septic system drainfields. Minimum 100 feet from private wells. Pre-Treatment:
	Show all pre-treatment practices. A sediment forebay should be considered an integral pre-treatment practice for all constructed wetlands. A forebay should be located at every major inlet to trap sediment and preserve
	the capacity of the main wetland treatment cell. A major inlet is any individual storm drain inlet pipe or open channel conveying runoff from at least 10% of the wetland's CDA. The forebay is considered a separate cell in both Level 1 and Level 2 designs, formed by an acceptable barrier (e.g., earthen berm, concrete weir, gabion baskets, etc.) The forebay should be at least 4 feet deep and equipped with a variable width
	aquatic bench around the perimeter, for safety purposes. The aquatic bench should be 4 to 6 feet wide at a depth of 1 to 2 feet below the water surface, transitioning to zero width at grade. Show the location of the metered rod that monitors long-term sediment accumulation (in the center of the pool, as measured lengthwise along the low flow water travel path). The bottom of the forebay may be hardened (e.g., with concrete, asphalt, or grouted riprap) to make sediment removal easier.
	Show the locations of all conveyance system outfalls into basin Show the layout and dimensions of basin features: permanent pool, sediment forebay,
	embankment, emergency spillway. basin side slopes, basin bottom, etc. The footprint is typically <i>less</i> than 3% of the CDA for Level 1 designs and <i>more</i> than 3% of the CDA for Level 2 designs. Pool geometry
	Show the wet/dry weather flow paths Reflect the proper length-to-width ratio as specified in the BMP design specifications Reflect the proper orientation to avoid short-circuiting Reflect the side slopes (H:V) of basin storage area and embankment (upstream and downstream slopes) Provide an aquatic bench for safety
	Indicate the location of outlet protection per VE&SCH Std. & Spec. 3.18 Indicate the top-of-bank and basin bottom elevations Indicate the elevations of the permanent pool, the treatment volume and the maximum design water surface elevations for all appropriate design storms and safety storms Snow any shoreline protection measures Show the location and dimensions of the riser and barrel
	Identify the pool depth zones on the plan

	Identify the constructed wetland/shallow marsh areas on the plan
	Provide basin liner specifications Provide sufficient maintenance access to the forebay, safety benches, riser structure, embankment, emergency spillway, basin shoreline, extended drawdown device, principal spillway outlet, stilling basin, toe drains, and likely sediment accumulation areas. The access road must:
	Be constructed of load bearing materials able to withstand the expected frequency of use.
	Have a minimum width of 12 feet. Possess a maximum profile grade of 15%. Have sufficient turn-around area. A maintenance right-of-way or easement must extend to the stormwater pond from a public or private road.
B. BM	P Section Views & Related Details
1. Pre	e-Treatment
	_ The forebay should be sized to hold 0.25 inch of runoff per impervious acre of the CDA, but no
	less than 0.1 inch per impervious acre. For smaller stormwater facilities, a more appropriate sizing criterion of 10% of the total required pool or detention volume may be more practical.
	This volume should be a maximum of 4 feet deep (or a depth determined by the summer drought water balance) near the inlet to adequately dissipate turbulent inflow without re-suspending previously deposited sediment, and then transition to a depth of 1 foot at the entrance to the first wetland cell.
	The forebay should be equipped with a variable width aquatic bench around the perimeter of the 4-foot depth, for safety purposes. The aquatic bench should be4 to 6 feet wide at a depth of 1 to 2 feet below the water surface, transitioning to zero width at grade.
	The volume of the forebay is part of the treatment volume of the stormwater basin for which it provides pre-treatment.
	However, for dry facilities, the forebay does <i>not</i> represent available storage volume if it remains full of water.
	A dry forebay must be carefully designed to avoid the resuspension of previously deposited sediments.
	The total volume of all forebays should be at least 15% of the total Treatment Volume. The relative size of individual forebays should be proportional to the percentage of their total inflow to the wetland.
	Separation between the forebay and the main basin may be achieved through the use of an earthen berm, gabion baskets, concrete, or a riprap wall.
	A designed overflow section should be constructed on the top of the separation to allow flow to exit the forebay at non-erosive velocities during the 2-year and 10-year frequency design
	storms.
	The overflow section may be set at the permanent pool elevation or the extended detention volume elevation.
	The bottom of the forebay(s) may be hardened (e.g., with concrete, asphalt, or grouted rip-rap) to make sediment removal easier.
	 Providing a hardened access or staging pad adjacent to the forebay helps protect the forebay and basin from excessive erosion from heavy equipment operation used for maintenance. Provide a typical grading section through the forebay, including typical side slopes, aquatic bench, shoreline protection, etc.

2. Wetland Cells Since mos

Z.	wetiand Ce	IIS
	Since n	nost constructed wetlands are on-line facilities, they need to be designed to safely pass
	the ma	ximum design storm (e.g., the 10-year and 100-year design storms).
		Ponding depths for the more frequent Treatment Volume storm (1-inch rainfall) and
		Channel Protection storm (1-year event) are limited in order to avoid adverse impacts to
		plant materials.
		Overflow for the less frequent 10- and 100-year storms should likewise be carefully
		designed to minimize the depth of ponding (a maximum of 4 feet over the wetland pool
		is recommended).
		The use of flashboard risers is strongly recommended to control or adjust water
		elevations in wetlands constructed on relatively flat terrain.
		Alternatively, a weir can be designed to accommodate passage of larger storms flows at
		relatively low ponding depths.
		Level 1 designs may incorporate extended detention that meets a maximum of 50% of
		the treatment volume or up to 12 inches of detention storage above the wetland pool
		(for channel protection); Level 2 designs may <i>not</i> incorporate extended detention.
	Internal	I design geometry:
		Internal design geometry and depth zones are critical in maintaining the pollutant
		removal capability and plant diversity of constructed wetlands.
		When feasible, wetlands should be irregularly shaped with long, sinuous flow paths,
		multiple cells (Level 2), and a high ratio of surface area to volume (see Stormwater
		Design Specification No. 13).
		Flow Path:
		Overall flow path through the wetland (length-to-width ratio):
		Level 1 design: 2L:1W.
		Level 2 design: 3L:1W.
		Ratio of the shortest flow path (closest inlet to the outlet) to the overall length:
		Level 1 design: 0.5.
		Level 2 design: 0.8.
		If unable to meet these targets, then the drainage area served by these
		"closer" inlets should constitute no more than 20% of the total CDA.
		Side slopes should be from 4H:1V to 5H:1V to promote better establishment and growth
		of wetland vegetation, provide for easier maintenance, and create a more natural
		appearance.
		The slope profile within individual wetland cells should generally be flat from inlet to
		outlet (adjusting for microtopography). The recommended elevation drop between
		wetland cells should be no more than 1 foot.
	Proper	surface area/depth allocations for permanent pool/shallow marsh/constructed wetland.
	1 10001	Indicate the elevations of permanent pool, treatment volume and maximum design
		water surface elevations for all appropriate design storms and safety storms
		Pool depths:
		Level 1 wetlands have a uniform depth with the mean pool depth greater than 1
		foot.
		Level 2 wetlands have variable depths with the mean pool depth # 1 foot.
		At least 25% of the Treatment Volume must be provided in at least three (3) deeper
		pools of from 18 to 48 inches, located at the inlet (forebay), center, and outlet
		(micropool) of the wetland.
		High Marsh Zone: At least 70% of the wetland surface must exist in the high marsh
	<u> </u>	zone (-6 inches to +6 inches, relative to normal pool elevation)
		Transition Zone: The Low Marsh Zone (-6 inches to -18 inches below the normal pool
		elevation) is no longer an acceptable wetland zone , and is only allowed as a short
		transition zone from the deeper pools to the high marsh zone.
		This transition zone should have a maximum slope of 5H:1V, or preferably
		flatter, from the deep pool to the high marsh zone.
		It is advisable to install biodegradable erosion control fabrics or similar materials
		during construction to prevent erosion and slumping of this transition zone.

	 Micro-topographic features (mix of above-pool vegetation, shallow pools and deep pools) that promote dense and diverse vegetative cover (Level 2 designs require at least two of the following): Tree peninsulas, high marsh wedges or rock filter cells configured perpendicular to the flow path. Tree islands above the normal pool elevation and maximum extended detention zone, formed by coir fiber logs. Inverted root wads or large woody debris. Gravel diaphragm layers within high marsh zones. Cobble sand weirs. Additional deeper pools.
3. I	mbankment (or dam)
	Type of embankment:
	Homogenous embankment Zoned embankment
	The earthen embankment must be designed to be stable against any force condition or
	combination of force conditions that may develop during the life of the structure (including differential settlement within the embankment, seepage through the embankment and foundation, or sharing stresses within the embankment and foundation) and is dependent upon: Construction materials
	Foundation conditions
	Embankment height and cross-section geometry
	Normal and maximum pool levels
	Purpose of structure (i.e., retention, extended detention, etc.).
	Embankment geometry:
	Top of dam elevations: constructed height and settled height (allowing for 10%
	settlement). Height (based on the freeboard requirements): There must be at least 1 foot of freeboard between the maximum 100-year storm water surface elevation (WSE) to the lowest point on the top of the embankment (excluding the emergency spillway).
	An embankment without an emergency spillway must provide at least 2 feet of freeboard between the maximum 100-year storm water surface elevation (WSE) to the lowest point on the top of the embankment. NOTE: The spillway design storm WSE, if specified, may be substituted for the 100-year storm WSE in either of the above situations.
	Top width varies with embankment height and should be shaped to provide positive
	drainage.
	The top of the embankment must be level in order to avoid possible overtopping in one location in cases of extreme storms or spillway failure.
	Embankment slopes should be no steeper than 3H:1V, if feasible, with a maximum combined upstream and downstream slope of 5:1 (i.e., 3H:1V downstream face and
	2H:1V upstream face).
	For embankments exceeding 15 feet in height, a 6 to 10 foot wide bench should be provided at intervals of 10 to 15 feet of height, particularly if slopes are steeper than 3H:1V.
	The embankment cross-section must be designed to provide an adequate factor of safety to
	protect against sliding, sloughing, or rotation in the embankment or foundation. Slope stability depends upon:
	Physical characteristics of the fill materials
	Configuration of the site
	Foundation materials
	Shear strength
	Compressibility
	Permeability

	_ Internal drainage systems in embankments (e.g., drainage blankets, toe drains, etc.) should be
	designed so that the collection conduits discharge downstream of the embankment at a location
	where access for observation is possible by maintenance personnel.
	_ Adequate erosion protection is recommended along the contact point between the face of the
	embankment and the abutments, where runoff concentrates.
	Evaluate whether a gutter surface other than sod is necessary (riprap is generally
	preferred over a paved concrete gutter).
	_ Trees, shrubs or any other woody plants should not be planted or allowed on the embankment
	or adjacent areas extending at least 25 feet beyond the embankment toe and abutment
	contacts.
	_ Indicate the top of embankment elevations: constructed height and settled height (allowing for
	10% settlement).
	_ Indicate the elevation of the crest of the emergency spillway.
	_ Indicate the emergency spillway, with side slopes.
	_ Indicate the emergency spillway inlet, level, and outlet sections.
	_ Show the existing ground and proposed improvements profile along the center line of the
	embankment.
	_ Show the existing ground and proposed improvements profile along the center line of the
	principal spillway
	Provide a typical grading section through the pond, including typical side slopes with the aquatic
	bench, shoreline protection, etc.
-	_ Show the existing ground and proposed improvements along the center line of the emergency
	spillway
	Show the dimensions of zones for any zoned embankment
4 0-	anana Cantual
4. Sec	epage Control
	_ The contact point between the embankment soil, the foundation material, and the conduit is the
	most likely location for <i>piping</i> to occur, due to the discontinuity in materials and the difficulty in
	compacting the soil around the pipe.
	_ All utility conduits (except the principal spillway) should be installed away from the embankment.
	When utility conduits through the embankment cannot be avoided, they should meet the
	requirements for spillways:
	Watertight joints
	No gravel bedding
	Restrained to prevent joint separation due to settlement Phreatic line (4:1 slope measured from the principal spillway design high water elevation) is the
-	upper limit of the saturation zone
	At a minimum, this should be the 10-year design storm water surface elevation.
	If the phreatic line intersects the downstream slope of the embankment, a qualified soil
	scientist should be consulted to decide if additional controls, such as an internal drain,
	are needed.
	Seepage control should be included in the design if the following conditions exist:
	Pervious layers in the foundation are not intercepted by the cutoff.
	Possible seepage from the abutments may create a wet embankment.
	The phreatic line intersects the downstream slope.
	Special conditions exist that require drainage to ensure a stable embankment.
	Seepage may be controlled by:
-	A foundation, abutment or embankment drains.
	A downstream drainage blanket.
	A downstream toe drain (often desirable for homogeneous embankments).
	A combination of these measures.
	Seepage along pipe conduits that extend through an embankment should be controlled by use
	of the following to prevent piping failures along conduit surfaces:
	Anti-seep collar (provide detail).
	The Bureau of Reclamation, the U.S. Army Corps of Engineers, and the USDA
	no longer recommend the use of anti-seep collars, in deference to graded filters

or <i>filter diaphragms</i> and <i>drainage blankets</i> (more complex to design, but less complicated and more cost-effective to construct and allow for easier placement of fill material).
Size, based on the length of pipe in the saturation zone (aim is a minimum 15% increase in seepage length).
Spacing and location of collars on barrel:
Maximum collar spacing is 14 times the minimum projection above the pipe.
Minimum collar spacing is 5 times the minimum projection above the pipe.
Collar dimensions should extend a minimum of 2 feet in all directions around the pipe.
Anti-seep collars should be placed within the saturation zone. Where the spacing limit will not allow this, then at least one collar must be in the saturation zone.
All anti-seep collars and their connections to the conduit should be completely water-tight and made of material compatible with the conduit. NOTE: Dimple bands are <i>not</i> considered water-tight.
Metals must be shielded from dissimilar materials with rubber or plastic insulation at least 24 mils thick.
Anti-seep collars should be placed a minimum of 2 feet from pipe joints unless flanged joints are used.
Collars size should be calculated using the procedure specified in Chapter 13 of the Virginia Stormwater Management Handbook (2011).
_ The embankment filter and drainage diaphragm should be designed by a professional
geotechnical engineer.
These devices channel seepage flow through a filter of fine graded material,
such as sand, which traps any embankment material being transported. The flow is then conveyed out of the embankment through a perforated toe
drain or other acceptable technique.
The critical design element: the filter material grain size distribution is based on the grain size distribution of the embankment fill and foundation material.
The diaphragm should consist of sand, meeting fine concrete aggregate requirements (at least 15% passing the No. 40 sieve, but no more than
10% passing the No. 100 sieve).
The diaphragm should be a minimum of 3 feet thick and should extend vertically upward and horizontally at least 3 times the pipe diameter and vertically downward at least 24 inches beneath the barrel invert, or to
rock, whichever is encountered first.
The diaphragm should be placed immediately downstream of the cutoff trench, approximately parallel to the centerline of the dam.
The diaphragm should be discharged at the downstream toe of the embankment.
The opening sizes for slotted and perforated pipes in drains must be designed using the filter criteria.
A second filter layer may be required around the drain pipe in order to alleviate the need for many very small openings.
Fabric should <i>not</i> be used around the perforated pipe as it may clog, rendering the perforations impenetrable to water.

5.	Foundation and Cut Off Trench or Key Trench
	Label all materials
	The presence of rock in the embankment foundation area requires specific design and
	construction recommendations (provided by the geotechnical engineering analysis) to ensure a
	proper bond between the foundation and the embankment.
	Generally, no blasting should be permitted within 100 feet of the foundation and abutment area.
	If blasting is necessary, it should be carried out under controlled conditions to reduce
	adverse effects on the rock foundation (e.g., over-blasting, opening fractures, etc.),
	especially critical in karst topography.
	Show the cut-off trench bottom width (4 foot minimum or greater as specified in the geotechnical
	report).
	Show the cut-off trench depth (4 foot minimum or as specified in the geotechnical report)
	Show the cut-off trench side slopes (no steeper than 1H:1V).
	Chew the cut on trenen side diopse (no steeper than 111117).
6.	Multi Stage Riser and Barrel System
	Principal spillways should be sized according to calculation procedures in Chapter 13 of the
	Virginia Stormwater Management Handbook (2011).
	The principal spillway should be located within the embankment and accessible from dry land to
	ensure easy access for maintenance.
	Access to the riser should be provided by lockable manhole covers and manhole steps
	within easy reach of valves and other controls.
	Provide a schedule of materials and clearly label them in drawings.
	Drop inlet spillways (riser and barrel system) should be designed as follows:
	Full flow is established in the outlet conduit and riser at the lowest hydraulic head over
	the riser crest that is feasible. Indicate the crest elevation of riser structure.
	The facility must operate without excessive surging, noise, vibration, or vortex
	action at any stage.
	Therefore, the riser must have a larger cross-sectional area than the outlet
	conduit.
	Headwall or conduit spillways consist of a pipe extending through an embankment with a
	headwall at the upstream end. The headwall is typically oversized to provide an adequate
	surface against which to compact the embankment fill.
	Weir spillways should be designed as follows:
	When used as the principal spillway, it should be armored with concrete or other non-
	erosive material.
	At the spillway, armoring should extend from the upstream face of the embankment to a
	point downstream of the spillway toe.
	All principal spillways should be constructed of non-erosive material with an anticipated life
	expectancy similar to that of the stormwater management facility.
	Pre-cast riser structures may <i>not</i> be substituted if the plans call for a cast-in-place structure,
	unless approved by the design engineer and the plan approving authority.
	Sections of pre-cast structures must be anchored together to meet stability and flotation
	requirements.
	A separate principal spillway and emergency spillway is generally recommended, unless:
	Topography/abutments are too steep.
	Existing or proposed development conditions impose constraints.
	Other factors (e.g., a road embankment is used as the dam, the basin is excavated,
	etc.)
	In such instances, a combined principal/emergency spillway that passes both low flows
	and extreme flows may be considered for use, in the form of a drop inlet spillway, a
	headwall/conduit spillway, or some other design that achieves equivalent results.
	It is very important to protect such combined spillways from clogging.
	Conduits/structures through embankments:
	Limit the number of conduits that penetrate through the embankment.
	Indicate the barrel diameter, inverts, and slope (%).
	Show the inverts and dimensions of control release orifices/weirs

Show th	ne structure dimensions
Show th	he extended detention (if added) orifice protection
NOTE:	A cause of embankment failure is the separation of pipe joints due to differential
settlem	ent and pipe deflection.
	nections to pipes must be completely water-tight.
•	The drain pipe (or barrel) connection to the riser should be welded all around
	when both are metal.
	A rubber or neoprene gasket should be used when joining pipe sections.
	The end of each pipe should be re-rolled by enough corrugations to fit the band
	· · · · · · · · · · · · · · · · · · ·
	width.
	Helically corrugated pipe should have either continuous welded seams or lock
	seams with internal caulking or a neoprene bead.
	The following connection types are acceptable:
	For pipes less than 24 inches in diameter:
	Flanges with gaskets on both ends of the pipe
	A 12-inch wide standard lap type band with a 12-inch wide by
	½-inch thick closed cell circular neoprene gasket.
	A 12-inch wide hugger type band with O-ring gaskets having a
	minimum diameter of 3/8 inch greater than the corrugation
	depth.
	For pipes ∃ 24 inches in diameter:
	A 24-inch long annular corrugated band using rods and lugs.
	A 24-inch wide by 3/8 inch thick closed cell circular neoprene
	gasket.
Corruga	ated metal pipe (CMP) must meet or exceed the minimum required design
thickne	SS.
	Steel pipe and its appurtenances should be galvanized and fully bituminous-
	coated and should conform to the requirements of AASHTO Specification M-
	190 Type A with water-tight coupling bands.
	Any bituminous coating damaged or otherwise removed should be
	replaced with cold-applied bituminous coating compound.
	Steel pipes with polymeric coatings should have a minimum coating
	thickness of 0.01 inches (10 mils) on both sides of the pipe.
	Coated corrugated steel pipe should meet the requirements of
	AASHTO M-245 and M-246; the following coatings or an approved
	equivalent may be used: Nexon, Plasti-Cote, Blac-Clad, and Beth-Cu-
	Loy.
	Aluminum coated steel pipe and its appurtenances should conform to the
	requirements of AASHTO Specification M-274 with water-tight coupling bands
	or flanges.
	Any aluminum coating damaged or otherwise removed should be
	replaced with cold-applied bituminous coating compound.
	Aluminum pipe and its appurtenances should conform to the requirements of
	AASHTO Specification M-196 or M-211 with water-tight coupling bands or
	· · · · · · · · · · · · · · · · · · ·
	flanges.
	Aluminum surfaces that are to be in contact with concrete should be
	painted with one coat of zinc chromate primer, and hot-dipped
	galvanized bolts may be used for connections.
	The pH of the surrounding soils should be between 4 and 9.
	The contractor and project inspector should verify the metal thickness,
_	corrugation size, proper connecting bands, and gasket type.
	Maximum allowable deflection of CMP conduits is 5% of the pipe diameter.
	Water-tight joints are necessary to prevent infiltration of embankment soils into
	the conduit.
	All joints must be constructed as specified by the pipe manufacturer.
	, we write that be constituted as specified by the pipe manufacture.

		Field joints (the ends of the pipes are cut off in the field) should <i>not</i> be accepted. With larger pipe sizes, it may be difficult to get water-tight joints, even if the deflection is within design parameters.
	Bands:	In such cases, the designer may choose to specify a heavier gage pipe.
		All connectors must be composed of the same material as the pipe. Metals must be shielded from dissimilar materials with rubber or plastic insulation at least 24 mils thick.
		6-inch hugger bands and "dimple bands" should not be accepted for CMP conduits.
		For pipes \leq 24 inches in diameter, use 12-inch wide bands with 12-inch O-ring or flat neoprene gaskets.
		For larger pipes, use 24-inch wide bands with 24-inch wide flat gaskets and four "rod and lug" type connectors. Flanged pipe with gaskets may also be used.
		All pipe gaskets should be properly lubricated with the material provided by the manufacturer, and tensioned, to prevent deterioration of the gasket material.
		Flat gaskets must be factory welded or solvent-glued into a circular ring, with no overlaps or gaps
		e should be firmly and uniformly bedded throughout its length: Where rock or soft, spongy or other unstable soil is encountered, it should be removed and replaced with suitable soil that is subsequently compacted to provide adequate structural support.
		Under no conditions should gravel bedding be placed under a conduit through the embankment.
	the bar	tion of a concrete pipe cradle will help to reduce the risk of piping under rrel and the subsequent failure of the embankment, resulting from tial settlement.
		The concrete cradle may not be necessary along the entire length of the conduit to prevent piping, but it is recommended since gravel bedding under an embankment conduit is <i>never</i> appropriate unless it is designed as a filter or drainage diaphragm
		If the external load (e.g., from height of the embankment, anticipated construction traffic, the weight of compaction equipment, etc.) on the barrel is enough to warrant provision for its maximum supporting strength, then a concrete cradle should be installed along the conduit's entire length.
		crete pipe should have bell and singular spigot joints with rubber gaskets
and sho	Bell and	al or exceed ASTM Designation C-361. I spigot pipe should be placed with the bell end upstream. hould be made consistent with manufacturer recommendations.
	After th	ie joints are sealed for the entire run of pipe, the bedding should be so that all spaces under the pipe are filled.
		All reinforced concrete pipe conduits should be laid in a <i>concrete</i> bedding for their entire length.
		This bedding should consist of high slump concrete placed under the pipe and up the sides of the pipe at least 25% of its outside diameter, and preferably to the spring line, with a minimum thickness of 3 inches, or otherwise as shown on the drawings.
	Care sh of the p	nould be taken to prevent any deviation from the original line and grade ipe.
	yl Chlori or ASTI	de (PVC) pipe should be PVC-1120 or PVC-1220 conforming to ASTM D-2241.
	Joints a	and connections to anti-seep collars should be completely water-tight.

The pipe should be firmly and uniformly bedded throughout its length. Where rock or soft, spongy or other unstable soil is encountered, it should be removed and replaced with suitable soil that is subsequently compacted to provide adequate structural support. All conduits penetrating dam embankments should be designed using the following
criteria:
Conduits and structures penetrating an embankment should have a smooth surface without protrusions or indentations that will hinder compaction of embankment materials.
All conduits should be circular in cross-section except cast-in-place reinforced concrete box culverts. This is also true where multiple conduits are employed. Conduits should be designed to withstand the external loading from the
proposed embankment without yielding, buckling or cracking, all of which will result in joint separation.
Conduit strength should not be less than the values shown in the design specifications for corrugated steel, aluminum, and PVC pipes, and the applicable ASTM standards for other materials The designer or contractor should obtain a manufacturer's certification
that the pipe meets plan requirements for design load, pipe thickness, joint design, etc.
Inlet and outlet flared-end sections should be made from materials that are compatible with the pipe.
All pipe joints should be made water-tight by using flanges with gaskets, coupling bands with gaskets, bell and spigot ends with gaskets, or by welding. Where multiple conduits are employed, sifficient space should be provided
between the conduits and installed anti-seep collars to allow for backfill material to be placed between the conduits with earth-moving equipment and easy
access by hand-operated compaction equipment The distance between conduits should be ∃ 1/2 of the pipe diameter,
but not less than 2 feet.
Cathodic protection should be provided for coated welded steel and galvanized corrugated metal pipe when soil and resistivity studies indicate the need for a protective coating against acidic soils.
Outlet protection must be used for the downstream toe of a spillway structure to help dissipate the high-energy flow through the spillway and to prevent excessive erosion in the receiving
channel. The type of outlet protection depends on the flow velocities associated with the spillway.
Riprap is the preferred form of outlet protection, designed according to Chapter 13 of the Virginia Stormwater Management Handbook (2011) and the Virginia Erosion and Sediment Control Handbook (1992). Gabion baskets are also an acceptable outlet protection material.
The bottom of the riprap apron should be constructed at 0% slope along its length.
The end of the apron should match the grade and alignment of the receiving channel.
If the receiving channel is well-defined, the riprap should be place on the channel bottom and side slopes (no steeper than 2H:1V) for the entire length, as required in the design criteria in Chapter 13 of the <i>Virginia Stormwater</i>
Management Handbook (2011) and the Virginia Erosion and Sediment Control Handbook (1992).
 Riprap placement should not alter the channel's geometry. Excavation of the channel bed and banks may be required to construct the full thickness of the apron.
If the barrel discharges into the receiving channel at an angle, the opposite bank must be protected up the 10-year storm elevation. In no instance should the total length of outlet protection be shortened.

 If a permit requires that no work may be performed in the stream or channel, then the outlet structure must be moved back to allow for adequate protection. The horizontal alignment of the apron should have no bends within the design length.
length. Additional riprap should be placed if a significant change in grade occurs at the downstream end of the outfall apron.
Filter fabric should be placed between the riprap and the underlying soil to
prevent soil movement into and through the riprap. All control structures should have a trash rack or debris control device, designed as follows:
All trash rack and debris control components should be made of stainless steel or galvanized metal meeting VDOT specifications.
Trash racks attached to a concrete spillway structure should be secured with stainless
steel anchor bolts Openings for trash racks should be no larger than 1/2 of the minimum conduit
dimension and, to discourage child access, bar spacing should be no greater than 1 foot apart. The clear distance between the bars on large storm discharge openings generally should be no less than 6 inches.
Flat grates for trash racks are <i>not</i> acceptable. Inlet structures that have flow over the top should have a non-clogging trash rack (e.g.,
a hood-type inlet that allows passage of water from underneath the trash rack into the riser, or a vertical or sloped grate).
The designer should verify that the surface area of the vertical perimeter of a raised
grate equals the area of the horizontal top opening, to allow adequate flow passage should the top horizontal surface become clogged.
Metal trash racks and monitoring hardware should be constructed of galvanized or
stainless steel.
Methods to prevent clogging of extended detention orifices in dry extended detention bains should be carefully designed, since these orifices are usually very small and located at the invert or bottom of the basin.
All drop inlet spillways designed for pressure flow should have adequate anti-vortex devices (<i>not</i>
 required if weir control is maintained in the riser through all flow stages, including the maximum design storm or safety storm):
The device may be a baffle or plate installed on top of the riser, or a headwall set on
 one side of the riser. The design of a principal spillway riser structure should include a <i>flotation</i> or <i>buoyancy</i> calculation (see Chapter 13 of the <i>Virginia Stormwater Management Handbook, 2011</i>).
The downward force of the riser and footing (to which the riser must be firmly attached)
is the <i>structure weight</i> , which must be 1.25 times greater than the buoyant force acting on the riser.
 Stormwater management facilities having permanent impoundments may be designed so that
the permanent pool can be drained to simplify maintenance and sediment removal.
The draining mechanism will usually consist of a valve or gate attached to the spillway
structure and an inlet pipe projecting into the reservoir area, with a trash rack or debris control device.
The typical configuration of a drainpipe will place the valve inside the riser structure with
the pipe extending out to the pool area.
This configuration results in the drainpipe being pressurized by the hydraulic
head associated with the permanent pool. Procesurized pipes should have mechanical joints in order to avoid possible.
Pressurized pipes should have mechanical joints in order to avoid possible leaks and seepage resulting from the innate pressure.
In all cases, valves should be secured to prevent unauthorized draining of the
facility.
Basin drains should be designed with sufficient capacity to pass the 1-year frequency design storm with limited ponding in the reservoir area, so that sediment removal and other maintenance functions are not hampered.

	An uncontrolled or rapid drawdown of a stormwater basin could cause a slide in
	the saturated upstream slope of the dam embankment or shoreline area. Therefore, the design of the basin drain system should include specific
	operating instructions for the owner.
	Generally, the drawdown rate should not exceed 6 inches per day.
	For embankment or shoreline slopes of clay or silt, the drawdown rate
	may be as low as 1 inch per week to ensure slope stability.
7.	Emergency Spillway
	Vegetated emergency spillways must be built in existing, undisturbed earth/rock or "cut" in the
	abutments at one or both ends of an earthen embankment or over a topographic saddle anywhere on the periphery of the basin. They should <i>never</i> be located on any portion of the embankment fill material.
	Excavated emergency spillways consist of three elements:
	Excavated energency spillways consist of three elements An inlet channel, through which <i>subcritical</i> flow enters the spillway.
	An inject chainer, through which subchited now enters the spillway The inject channel should have a straight alignment and grade.
	The line chainer should have a straight angrithent and grade The cross-sectional area of flow in the inlet channel should be large in
	comparison to the flow area at the control section.
	Where the depth of the channel changes to provide for the increased flow area,
	the bottom width should be altered gradually to avoid abrupt changes in the shape of the sloping channel banks.
	A level section, which controls the depth of flow.
	The maximum design water surface elevation (normally for the 100-year storm)
	through the emergency spillway should be at least 1 foot lower than the settled
	top of the embankment and should be confined by undisturbed earth or rock.
	The bottom width of the spillway should not exceed 35 times the design depth
	of flow, to avoid damage by meandering flow and accumulated debris.
	Whenever the required bottom width is likely to be excessive, consideration
	should be given to incorporation of a spillway at each end of the dam.
	The two spillways do not need to be of equal width if their total capacity
	meets design requirements.
	An exit channel, through which either <i>critical</i> or <i>supercritical</i> flow discharges from the
	spillway
	The alignment of the exit channel must be straight to a point far enough below the embankment to ensure that any flow escaping the exit channel cannot damage the embankment.
	The exit channel should have the same cross-section as the control section.
	The slope of the exit channel must be:
	Adequate to discharge the peak flow within the channel.
	No greater than that which will produce maximum permissible velocities
	for the soil type or the planned grass cover.
	The slope range of the exit channel is selected to ensure <i>supercritical</i> flow in the channel.
	The control section is the point on the spillway where the flow passes through <i>critical</i>
	depth, usually installed close to the intersection of the earthen embankment and the
	emergency spillway centerlines.
	The type of soil and vegetative cover used in the emergency spillway will influence the spillway
	design dimensions and geometry.
	Vegetation provides a degree of retardance to the flow through the spillway, depending mostly on the height and density of the vegetative cover chosen.
	Hydraulic design for emergency spillways must be done in accordance with criteria provided in
	Appendix C: Vegetated Emergency Spillways of the Introduction to the New Virginia Stormwater
	Design Specifications (as posted on the Virginia Stormwater BMP Clearinghouse web site at
	http://www.vwrrc.vt.edu/swc/NonProprietaryBMPs.html) and in Chapter 13 of the Virginia
	Stormwater Management Handbook (2011).
	Spillway side slopes should be no steeper than 3H:1V unless the spillway is excavated into rock.

	Show the existing ground and proposed improvements along the center line of the emergency spillway
C.	ndscape Plan
	_ The landscaping plan should be jointly developed by the design engineer and a wetlands expert
	or experienced landscape architect
	It may be advisable to use a subcontractor who specializes in aquatic landscaping.
	The plan should outline a detailed schedule for the installation, care, maintenance and possible
	reinforcement or replacement of vegetation in the wetland and its buffer for up to 10 years after
	the original planting.
	_ The plan should indicate how appropriate wetland plants will be established within each
	inundation zone (e.g., wetland plants, seed mixes, volunteer colonization, tree and shrub stock, etc.) and whether soil amendments are needed to get plants started.
	_ Include a plan view with topography at a contour interval of no more than 1 foot and spot
	elevations throughout the cell showing the wetland configuration, different planting zones, microtopography, grades, site preparation, and construction sequence.
	_ Provide a planting schedule and specifications (transport / storage / installation / maintenance)
	for emergent, perennial, shrub and tree species, quantity of each species, stock size, type of
	root stock to be installed, and spacing.
	Plan early. As much as 6 to 9 months of lead time may be needed to fill orders for
	wetland plant stock from aquatic plant nurseries.
	Plant stock should be nursery grown (unless otherwise approved by the local regulatory
	authority) and should be healthy and vigorous native species free from defects, decay,
	disfiguring roots, sun-scald, injuries, abrasions, diseases, insects, pests, and all forms
	of infestations or objectionable disfigurements Plant selection must be appropriate for the site's vegetation climatic zone (6-8 in Virginia)
	Plant materials should be wet-footed species but must be able to withstand both wet
	and dry periods as well as relatively high velocity flows within the swale.
	If the swale is adjacent to a roadway where winter conditions will require the use of road
	salts in the CDA, then salt-tolerant non-woody plant species should be specified.
	To the degree feasible, the species list should contain native species found in similar
	local wetlands.
	Plant 5 to 7 species of emergent wetland plants, with at least four (4) of these
	designated as aggressive colonizers.
	No more than 25% of the high marsh surface area needs to be planted, with individual
	plants 18 inches on center within each single species cluster. If done properly, the entire
	wetland should be colonized within three years.
	Trees and shrubs should be integrated into the design in tree islands, peninsulas, and
	fringe buffer areas (Level 2 design). Trees may be planted in clusters to share rooting space on compacted wetland
	side slopes. Planting holes should be amended with compost (a 2:1 ratio of loose soil to
	compost) prior to planting.
	Vary the size and age of the plant stock to promote a diverse structure.
	Plants should be kept in containers of water or moist coverings to protect their root
	systems and keep them moist when transporting them to the planting location.
	Buffer areas should be over-planted with a small stock of fast-growing successional
	species to achieve quick canopy closure and shade out invasive plant species.
	_ The construction contract should include a Care and Replacement Warranty that specifies a
	minimum survival for species planted of 75% after the first growing season, and a minimum
	effective ground cover of 75% for flat roofs and 90% for pitched roofs.
	Specify preservation measures for existing vegetation

D.	Construction	on Notes
_	Ideally,	planned constructed wetland areas should be clearly marked off and remain <i>outside</i> the fland disturbance during construction to prevent soil compaction by heavy equipment. Constructed wetland areas <i>may</i> be used during construction as sites for temporary sediment traps or basins, provided the construction plans include notes and graphical details specifying the facility will be de-watered, dredged and re-graded to design dimensions after the original site construction is complete.
	vegeta	stormwater wetlands should be constructed during months that are best for establishing tive cover without irrigation (February 15 – April 15; September 15 – November 15). ne cases, it will be necessary to divert flow while the stormwater wetland is being
		ucted, so that no sediment flows into the wetland area until installation and stabilization
	are cor	Flow diversions may be required to meet additional requirements of and obtain permits
	Constr	from state and federal regulatory agencies. uction sequence (Phase 1: Wetland construction):
		Construction inspections should occur before, during and after installation to ensure the stormwater wetland is constructed according to specifications. Use detailed inspection checklists that require sign-offs by qualified individuals at critical states of construction, to ensure the contractor's interpretation of the plan is consistent with the designer's intent. The following are critical inspection points:
		During initial site preparation and installation of E&S Controls Excavation and grading (e.g., interim and final elevations) Embankment construction
		Wetland installation (e.g., microtopography, soil amendments, and staking of planting zones)Planting phase (with the wetland expert or landscape architect).
		Check the proposed site for existing utilities prior to any excavation. Assemble the construction materials on-site, making sure they meet design specifications, and prepare any staging areas.
		Clear, grub and strip the areas designated for borrow sites, embankment construction, and structural work to the desired subgrade, removing all trees, vegetation, roots and other objectional material.
		All cleared and grubbed material should be disposed of outside and below the limits of the embankment and reservoir.
		When specified, a sufficient quantity of topsoil should be stockpiled in a suitable location for use on the embankment and other designated areas.
		Install applicable temporary E&S control measures prior to construction. Areas surrounding the wetland area that are graded or denuded during construction of the wetland must be planted with turf grass, native plant materials or other approved methods of soil stabilization. Grass sod is preferred over grass seed, to prevent seed colonization of the wetland.
		Excavate the core trench for the embankment and install the spillway (outlet) pipe, including the downstream rip-rap apron (energy dissipation) protection
		The cutoff trench should be excavated into impervious material along or parallel to the centerline of the embankment.
		Trench side slopes should be laid back in steps at a 1H:1V slope or flatter. (from page 6; conflicts with 2:1 specified on page 10, Earthen Embankment Spec?).
		Backfill should be compacted with construction equipment, rollers, or hand tampers to assure maximum density and minimum permeability.
		Install the riser pipe or overflow structure, ensuring the top invert of the overflow weir is constructed level and at the proper design elevation (flashboard risers are strongly

recommended).

ct the er	mbankment and any internal berms in 8- to 12-inch lifts, compacted with
	n which fill is to be placed should be scarified before its placement.
 The mo	ost permeable borrow material should be placed in the downstream
	s of the embankment.
	ne principal spillway or overflow weir concurrently with fill placement and avated into the embankment. A vertical trench through the embankment
material	I (in order to place the spillway pipe) should not be allowed under any
circums	tances.
	Ensure that the top invert of the principal spillway or any overflow weir is constructed level and at the proper design elevation (at least 1 foot below the crest of the emergency spillway). Flashboard risers are strongly recommended for use in constructed wetlands.
 Filter an	nd Drainage Layers:
	In order to achieve maximum density of clean sands, filter layers should be flooded with clean water and vibrated just after the water drops
	below the sand surface.
	The filter material should be placed in lifts of no more than 12 inches in thickness.
	Up to 4 feet of embankment material may be laced over a filter material
	layer before excavating back down to expose the previous layer.
	After removing any unsuitable materials, the trench may be filled with
	additional 12-inch lifts of filter material, flooded, and vibrated as
	described above, until the top of adjacent fill is reached.
	The contractor should ensure that a qualified professional inspect filter
	and drainage diaphragms, ensuring that backfill material meets
	specifications for quality, lift thickness, placement, moisture content,
	and dry unit weight.
 Fill mat	erial should be taken from an approved, designated borrow area or
stockpile	
	Fill material should be free of roots, stumps, wood, rubbish, stones greater than 6 inches in diameter, and frozen or other objectionable
	materials.
	Fill material for the center of the embankment and the cutoff trench
	should conform to Unified Soil Classification GC, SC, or CL.
	Fill material that is beside pipes or structures should be of the same
	type and quality as specified for the adjoining fill material.
	The fill material should be placed in horizontal lifts not to
	exceed 4 inches in thickness and compacted by hand tampers
	or other manually directed compaction equipment.
	The material should completely fill all spaces under and beside
	the pipe.
	During backfilling, equipment should not be driven closer the 4
	feet horizontally to any part of a structure.
	Equipment should NEVER be driven over any part of a
	structure or pipe, unless compacted fill has been placed to a depth specified by the structural live load capacity of the
	structure or pipe, that adequately distributes the load.
	Consideration may be given to the use of other materials in the
	embankment based on the recommendation of a geotechnical engineer
	supervising the design and construction.
	The surface layer of compacted fill should be scarified prior to
	placement of at least 6 inches of topsoil, which must be properly stabilized.

	Fill material should be compacted with appropriate compaction equipment. The number of necessary passes by the compaction equipment over
	the fill material may vary with soil conditions. Fill material should contain sufficient moisture so that the required degree of compaction will be obtained with the equipment used. The minimum required density is 95% of maximum dry density with a
	moisture content within \pm 2% of the optimum, unless otherwise specified by the engineer.
	Each layer of fill should be compacted as necessary to obtain minimum density.
	Compaction tests should be performed regularly throughout the embankment construction.
	Typically, one test per 5,000 sq. ft. on each layer of fill or as directed by
	the geotechnical engineer. Use either a Standard Proctor Test (ASTM D698) or a Modified Proctor Test (ASTM D1557 – usually more appropriate for earthen dams). A new Proctor test is required if the material changes from that
	previously tested.
	The engineer should certify, at the time of construction, that each fil
	layer meets the minimum density. A geotechnical or construction inspector should be on site during embankment construction to do the following:
	Test fill compaction
	Observe foundation preparation.
	Observe pipe installation. Observe riser construction.
	Observe filter installation, etc.
Constru	uct the emergency spillway in cut or structurally stabilized soils.
	te/grade until the appropriate elevations and desired contours are achieved for
the bot	tom and side slopes of the wetland.
	Rough up the interim elevations with a skid loader or other similar equipment to achieve the desired topography across the wetland.
	Spot surveys should be made to ensure that the interim elevations for the
	wetland are 3 to 6 inches below the final elevations.
Install surviva	micro-topographic features and soil amendments (essential for wetland plant I).
content	g soil within the wetland should be loam or sandy loam with a high organic t, placed by mechanical methods, and spread by hand to a depth of at least 4
inches	for shallow wetlands. Planting soil should be tamped as directed in the design specifications, but it
	should not be overly compacted. After the planting soil is placed, it should be saturated and allowed to settle for
	at least one week prior to installation of plant materials.
	No machinery should be allowed to traverse over the planting soil during or after
	construction.
environ	te exposed soils with temporary seed mixtures appropriate for a wetland iment. All wetland features above the normal pool elevation should be arily stabilized by hydro-seeding or seeding over straw.
Construction se	equence (Phase 2: Establishing wetland vegetation):
wetland	e the wetland landscaping plan. Several weeks standing time is needed following d construction so that the designer can more precisely predict the following two
things:	Where the inundation zones are located in and around the wetland. Whether the final grade and wetland microtopography will persist over time.

	Selection of appropriate species and additional soil amendments, based on actual field confirmation of soil properties and the actual depths and inundation frequencies occurring within the wetland. Open up the wetland construction, to allow the wetland cell(s) to fill up to normal pool elevation.
	Inundation must occur in stages so the deep pool and high marsh plant materials can be placed effectively and safely. Wetland planting areas should be at least partially inundated during planting to
	promote plant survivability. Measure (to the nearest inch) and stake planting depths at the onset of the planting
	season. It may be necessary to modify the planting plan to reflect altered depths or a
	change in the availability of wetland plant stock.
	 Surveyed planting zones should be marked on the as-built or design plan, and the locations should be identified in the field, using stakes or flags. Propagate the stormwater wetland between mid-April and mid-June, using three simultaneous techniques to prapagate the emergent community over the wetland bed:
	Initial planting of container-grown wetland plant stock. Broadcast wetland seed mixes over the higher wetland elevations, to establish
	diverse emergent wetlands. Seeding of switchgrass or wetland seed mixes as a ground cover is recommended for all zones above 3 inches below the normal pool elevation.
	Hand broadcasting or hydroseeding can be used to spread seed, depending on the size of the wetland cell.
	Allow volunteer plants from upstream or the forest buffer to establish on their own (over the next 3 to 5 years).
	Install goose protection for newly planted or newly growing vegetation, especially emergents and herbacious plants.
	Place netting, webbing, or string installed in a criss-cross pattern over the surface area of the wetland above the level of the emergent plants. Plant the wetland fringe and buffer area in the zone generally extending from 1 to 3 feet above the normal pool elevation (from the shoreline fringe to about half of the maximum water surface elevation for the 2-year storm) with vegetation that can tolerate both wet
	 and dry periods. Implement any remaining permanent stabilization measures. Conduct a final inspection, log the GPS coordinates for each facility and submit them for
	entry into the local BMP maintenance tracking database.
Chap	tenance Items (can include BMP Operation & Maintenance Inspection Checklists from oter 9, Appendix 9-C of this Handbook) Provide a Maintenance Agreement, indicating the person or organization responsible for
	maintenance, authorizing access for inspections and maintenance, and including a maintenance inspection checklist.
	Include a Maintenance Narrative which describes the long-term maintenance requirements of the facility and all components, including installation/maintenance of safety signage; removal and disposal of trash, debris and sediment accumulations; and periodic harvesting and disposal of overgrown or old wetland plant materials. The narrative should also include a list of qualified contractors that can perform inspection and maintenance services plus contact information for local or state assistance to solve common nuisance problems.
	Record a deed restriction, drainage easement, and/or other enforceable mechanism, including GPS coordinates of the area, to ensure the constructed wetland area is not disturbed or converted to other uses. Provide sufficient facility access from the public ROW or roadway to both the constructed
	wetland and any pre-treatment practices.

IV. COMMENTS		
	Bv:	Date:

8-A.15.0. WET PONDS: DESIGN CHECKLIST

	ubmission Date			
	:Name			
Site Pla	an/Permit Number			
Practic	e No./Location on Site			
				Phone Number
				Phone Number
Genera	al Contractor			Phone Number
	Signature and stamp of li certification	icensed profes	sio	nal design consultant and owner
Plan S	tatus			
	_ Approved	Legend:		Complete
	Not Approved			Inc Incomplete/Incorrect N/A - Not Applicable
Facility	y Type: Level 1		Lev	rel 2
Hydrau	ılic Configuration:			
	On-line facility	Tvi	ne n	f wetlands incorporated:
	Off-line facility	ועי		Emergent
	On mic radiity			
Wet Po	ond Configuration:	Tva	_	f Pre-Treatment Facility:
	Wet Pond with 100% of	ועי		Sediment forebay (above ground)
_	permanent pool in a single cell			Vegetated buffer area
	Wet ED and/or multi-cell Wet			Grass filter strip
	Pond			Grass channel
	Pond/Wetland Combination			Other:
				Other.
I. SU	regulated under the Virginia Dam Provide a concise narrative des this practice fits into the overall p Show the location of this BMP or The basin pool area	n Safety Act and Recribing the storm plan, and stating along the site map, inc	Regu wate II ass Iudir	er management strategy, describing how sumptions made in the design.
	acres) and land cover constructed wetland. Delineation of FEMA 100	, sufficient to su D-year floodplain	ustai	ies, acreage (typically between 10 and 25 n a permanent water level within the
	Areas of the site comper		ater	quality calculations
	_ Provide topography for the site a		datio	ons and earthwork specifications and a
	description of any borrow area in		ualic	ons and earthwork specifications and a
	Provide a soil map for site and a		ıdina	the CDA
				ring logs with Unified Soils Classifications
	and soil descriptions.	na provido tile 301	. 50	mig 10go with orinion cons classifications
	Borings should be take			ed embankment, in the vicinity of the ations within the planned basin treatment
	Determine the physical of	characteristics of the as structural fill of		

Bearing capacity, buoyancy, etc. pertaining to outlet structure design. Compaction/composition needs for the embankment.
Depth to groundwater bedrock. Depth to seasonal high groundwater table: if the water table is close to the
surface, it may make excavation difficult and expensive, and groundwater inputs can also reduce the pollutant removal rates of wet ponds.
Evaluation of potential infiltration losses (and the consequent need for a liner). Wet ponds are generally not recommended to be used in karst areas and should be the option of last resort. If karst is present, a detailed geotechnical investigation is recommended to ensure
the wet pond does not aggravate potential karst impacts (e.g., sinkholes, groundwater contamination, etc.):
A minimum of 6 feet of unconsolidated soil material must exist between the bottom of the pond and the top of the underlying karst layer.
The maximum temporary or permanent water elevation with the basin must not exceed 6 feet.
Employ an impermeable liner that meets the requirements of Stormwater Design Specification No. 14.
Annual maintenance inspections must be conducted to detect sinkhole formation. Sinkholes that develop should be reported immediately after they have been observed and should be repaired, abandoned, adapted or observed over time following the guidance prescribed by the appropriate local or state groundwater protection authority.
The use of wet ponds is constrained in coastal plain sites due to flat terrain, low hydraulic head and high water table (constructed wetlands are preferred). Wet ponds may be considered
acceptable in coastal settings if the following design considerations apply: Slightly lower nutrient removal rates are assigned to coastal plain wet ponds.
If a "pocket pond" (one that has a small CDA and is supplied solely by groundwater and runoff) is constructed in a coastal setting, then it must meet the minimum design geometry requirements for all ponds, in order to avoid nuisance conditions.
The use of wet ponds is highly constrained at sites with steep terrain. May be able to terrace pond cells in a linear configuration where slopes do not exceed 10% by using a 1 to 2 foot armored elevation drop between individual cells.
 Where cold winter climates are typical, make the following adjustments: Treat larger runoff volumes in the spring by adopting seasonal operation of the
permanent pool. Plant salt-tolerant vegetation at pond benches (to deal with higher chloride content of
road salts). Do not submerge inlet pipes and provide a minimum 1% pipe slope to discourage ice
formation. Locate low-flow orifices so they withdraw at least 6 inches below the typical ice layer.
 Angle trash racks to prevent ice formation. Over-size the riser and weir structures to avoid ice formation and freezing pipes. If road sanding is prevalent in the CDA, increase the forebay size by 25% to
accommodate additional sediment loading. Wet ponds are poorly suited to treat runoff within open channels located in highway rights-of-
way, unless storage is available in a cloverleaf interchange or in an expanded right-of-way and special VDOT design criteria are used.
Wet ponds are generally <i>not</i> recommended in watersheds containing trout streams, due to the potential for stream warming.
A wet pond should <i>not</i> be built within an existing perennial stream or natural wetland nor should a wet pond discharge to jurisdictional waters without local/state/federal approvals and the
necessary permit(s). Identify potential conflicts with other (existing?) structural components (pipes, underground
utilities, etc.). The designer should check to see whether sediments removed from the forebay can be spoiled (deposited) on-site or must be hauled away.

II. COMPUTATIONS

A.	Hydrology
	Determine the runoff curve number (pre- and post-developed conditions), providing the
	worksheets.
	Determine the time of concentration (pre- and post-developed conditions), providing the
	worksheets.
	Generate hydrograph (pre- and post-developed conditions) for appropriate design and safety storms (USDA-NRCS methods or modified rational-critical storm duration method)
	Confirm that there is adequate drainage area and/or water balance from groundwater, runoff or
	baseflow so the wet pond will not experience unacceptable drawdown after a 30-day summer
	drought (minimum 24-inch deep reservoir recommended).
В.	Hydraulics
	Specify assumptions and coefficients used.
	Typically, 6 to 8 feet of hydraulic head are need to drive flow through the wetland.
	Provide a stage-storage table and curve Weir/orifice control analysis for riser structure discharge openings and riser crest.
	Well/offlice control analysis for riser structure discharge openings and riser crest Carefully design the low-flow orifice to minimize clogging, as follows:
	All outlet pipes should be adequately protected by an acceptable external trash
	racks or by internal orifice protection that may allow for smaller diameters.
	Recommend a minimum 3-inch diameter orifice to minimize clogging of an
	outlet or extended detention pipe when it is surface-fed (still susceptible to
	clogging from floating vegetation and debris).
	Smaller openings (down to 1-inch in diameter) are permissible, using internal
	orifice plates within the pipe.
	Another option is a submerged reverse-slope pipe that extends downward from
	the riser to an inflow point 1 foot below the normal pool elevation.
	Alternative methods must employ a broad-crested rectangular V-notch (or
	proportional) weir, protected by a half-round CMP that extends at least 12
	inches below the normal pool elevation Barrel: Conduct an inlet/outlet control analysis
	Conduct a riser/outlet structure flotation analysis (factor of safety = 1.25 min.).
	Conduct appropriate calculations for use as a temporary sediment basin riser with clean out
	schedule & instructions for conversion to a permanent facility.
	Provide for large storm overflow or bypass: emergency spillway adequacy/capacity analysis
	(100-year design storm) with required embankment freeboard.
	Provide a stage-discharge table and curve (provide equations).
	Route post-development hydrographs for appropriate design storms (1-yr., 10-yr., or as required
	by watershed conditions) and safety storms (100-yr. or as required)
	Provide storm drainage and hydraulic grade line calculations.
C	Downstream impacts
٠.	Conduct a danger reach study.
	Describe the 100 year floodplain impacts.
	Provide downstream hydrographs at critical study points.
	Demonstrate safe conveyance to an "adequate" receiving channel.
	If the receiving channel is natural and (1) has never been enhanced or "restored, OR (2)
	if tream channel erosion or localized flooding is an existing predevelopment condition,
	then conduct appropriate "energy balance" calculations to demonstrate safe
	conveyance from the facility to the receiving channel" (provide computations).

D.	Wate	er Quality
		Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in the
		CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generated
		by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet)
		Indicate the treatment volume for extended detention (if added) with draw-down calculation
		Determine specific sizing/dimensions from criteria in Stormwater Design Specification No. 14.
III.	PLA	N REQUIREMENTS
Α.	BMP	Plan View Information
		Show the limits of clearing and grading, noting that they should be identified and protected by acceptable signage, silt fence, snow fence, or other comparable barrier.
		Setbacks (local codes rule):
		Minimum 20 feet from property lines Minimum 25 feet from building foundations.
		Minimum 100 feet from septic system drainfields and private wells.
		Pre-Treatment:
		Show all pre-treatment practices.
		A sediment forebay should be considered an integral pre-treatment practice for all wet
		ponds.
		A forebay should be located at every major inlet to trap sediment and preserve the capacity of the main pond treatment cell.
		A major inlet is any individual storm drain inlet pipe or open channel conveying
		runoff from at least 10% of the wet pond's CDA.
		The forebay is considered a separate cell in both Level 1 and Level 2 designs, formed by an acceptable barrier (e.g., earthen berm, concrete weir, gabion baskets, etc.)
		Show the location of the metered rod that monitors long-term sediment
		accumulation (in the center of the pool, as measured lengthwise along the low flow water travel path).
		Show the locations of all conveyance system outfalls (inlets) into basin
		Show the layout and dimensions of basin features: permanent pool, sediment forebay,
		embankment, emergency spillway. basin side slopes, basin bottom, etc.
		The footprint is typically between 1% and 3% of the CDA, depending on the pond depth
		(deeper ponds need a smaller footprint).
		Pool geometry Show the wet/dry weather flow path
		Confirm the proper orientation to avoid short-circuiting
		Internal design geometry and depth zones are critical in maintaining the pollutant
		removal capability.
		Wet ponds should have an irregular shape and a long flow path from inlet to outlet, to
		increase water residence time and pond performance.
		Flow Path:
		Overall flow path through the wetland (length-to-width ratio):
		Level 1 design: 2L:1W. Level 2 design: 3L:1W.
		Ratio of the shortest flow path (closest inlet to the outlet) to the overall length:
		Level 1 design: 0.5.
		Level 2 design: 0.8.
		If unable to meet these targets, then the drainage area served by these
		"closer" inlets should constitute no more than 20% of the total CDA.
		Treatment volume storage may be provided by a combination of a permanent pool, a
		shallow marsh and/or extended detention storage.
		The permanent pool storage may be divided among multiple cells
		Performance is enhanced by multiple treatment cells, longer flow paths, high surface area-to-volume ratios, and/or redundant treatment methods.

A berm or simple weir should be used instead of pipes to separate multiple
pond cells.
Stormwater pond benches:
A safety bench is a flat bench located just outside of the perimeter of the
permanent pool to allow for maintenance access and reduce safety risks when
the pond side slopes exceed 5H:1V.
The safety bench generally extends 8 to 15 feet outward from the
normal water edge to the shoulder of the stormwater pond side slope.
An aquatic bench is a shallow area just inside the perimeter of the normal pool
that promotes growth of aquatic and wetland vegetation.
The bench also serves as a safety feature, reduces shoreline erosion,
and conceals floatable trash.
The bench should extend up to 10 feet inward from the normal
shoreline and have an irregular configuration.
 Safety features:
End walls above pipe outfalls greater than 48 inches in diameter must be fenced to
prevent a hazard.
The emergency spillway must be located so that downstream structures will not be
impacted by spillway discharges.
Warning signs prohibiting swimming must be posted.
 Show outlet protection per VE&SCH Std. & Spec. 3.18
Must be stable for the 10-year design storm.
The channel immediately below the pond outfall must be modified to prevent erosion
and conform to natural dimensions in the shortest possible distance.
This is done typically by placing appropriately-sized riprap over filter fabric,
which can reduce flow velocities from the principal spillway to non-erosive
levels (3.5 to 5 ft./sec.).
Flared pipe sections, which discharge at or near the stream invert or into a step/plunge
pool, should be used at the spillway outlet.
Indicate the top-of-bank and basin bottom elevations
 Indicate the elevations of the permanent pool, the treatment volume and the maximum design
 water surface elevations for all appropriate design storms and safety storms
Show any shoreline protection provided
NOTE: Fencing the perimeter of wet ponds is discouraged, except at or above the maximum
 water surface elevation in the rare instances when the pond slope is a vertical wall.
Show the location and dimensions of the riser and barrel.
 Identify the pool depth zones on the plan
 Identify any wetland/shallow marsh areas incorporated into the pond plan
 Show sufficient maintenance access to the forebay, safety benches, riser structure,
 embankment, emergency spillway, basin shoreline, extended drawdown device, principal
spillway outlet, stilling basin, toe drains, and likely sediment accumulation areas. Access roads
must:
Be constructed of load bearing materials Have a minimum width of 12 feet.
Possess a maximum profile grade of 15%.
Have sufficient turn-around area.
A maintenance right-of-way or easement must extend to the stormwater pond from a
public or private road.

B. BMP Section Views & Related Details

	reatment
	The forebay should be sized to hold 0.25 inch of runoff per impervious acre of the CDA, but no
	less than 0.1 inch per impervious acre.
	For smaller stormwater facilities, a more appropriate sizing criterion of 10% of the total
	required pool or detention volume may be more practical.
	This volume should be a maximum of 4 feet deep (or a depth determined by the
	summer drought water balance) near the inlet to adequately dissipate turbulent inflow
	without re-suspending previously deposited sediment, and then transition to a depth of 1 foot at the entrance to the first wet pond cell.
	The forebay should be equipped with a variable width aquatic bench around the perimeter of the
	4-foot depth, for safety purposes. The aquatic bench should be4 to 6 feet wide at a depth of 1 to
	2 feet below the water surface, transitioning to zero width at grade.
	The volume of the forebay is part of the treatment volume of the stormwater basin for which it
	provides pre-treatment.
	However, for dry facilities, the forebay does <i>not</i> represent available storage volume if it
	remains full of water.
	A dry forebay must be carefully designed to avoid the resuspension of previously
	deposited sediments.
	The total volume of all forebays should be at least 15% of the total Treatment Volume. The
	relative size of individual forebays should be proportional to the percentage of their total inflow
	to the wet pond.
	Separation between the forebay and the main basin may be achieved through the use of an
	earthen berm, gabion baskets, concrete, or a riprap wall.
	A designed overflow section should be constructed on the top of the separation to allow flow to
	exit the forebay at non-erosive velocities during the 2-year and 10-year frequency design
	storms.
	The overflow section may be set at the permanent pool elevation or the extended
	detention volume elevation.
	The bottom of the forebay(s) may be hardened (e.g., with concrete, asphalt, or grouted rip-rap)
	to make sediment removal easier.
	Providing a hardened access or staging pad adjacent to the forebay helps protect the forebay
	and basin from excessive erosion from heavy equipment operation used for maintenance.
	Provide a typical grading section through the forebay, including typical side slopes, aquatic
	bench, shoreline protection, etc.
2. Emba	ankment (or dam) and Ponding Areas
	Indicate the type of embankment:
	Homogenous embankment
	Zoned embankment
	The earthen embankment must be designed to be stable against any force condition or
	combination of force conditions that may develop during the life of the structure (including
	differential settlement within the embankment, seepage through the embankment and
	foundation, or sharing stresses within the embankment and foundation) and is dependent upon:
	Construction materials
	Foundation conditions
	Embankment height and cross-section geometry
	Normal and maximum pool levels
	Purpose of structure (i.e. retention, extended detention, etc.)

 Embankment geometry:
Top of dam elevations: constructed height and settled height (allowing for 10% settlement).
Height (based on the freeboard requirements):
There must be at least 1 foot of freeboard between the maximum 100-
year storm water surface elevation (WSE) to the lowest point on the top
of the embankment (excluding the emergency spillway).
An embankment without an emergency spillway must provide at least 2
feet of freeboard between the maximum 100-year storm water surface
elevation (WSE) to the lowest point on the top of the embankment.
NOTE: The spillway design storm WSE, if specified, may be substituted
for the 100-year storm WSE in either of the above situations.
The top width varies with embankment height and should be shaped to provide positive
drainage.
The top of the embankment must be level in order to avoid possible overtopping in one
location in cases of extreme storms or spillway failure.
Embankment slopes should be no steeper than 3H:1V, if feasible, with a maximum
combined upstream and downstream slope of 5:1 (i.e., 3H:1V downstream face and
2H:1V upstream face).
For embankments exceeding 15 feet in height, a 6 to 10 foot wide bench should be
provided at intervals of 10 to 15 feet of height, particularly if slopes are steeper than
3H:1V.
The slope profile within a wet pond should be at least 0.5% to 1% to promote positive
flow through the pond.
 Pond side slopes should be from 4H:1V to 5H:1V to promote better establishment and growth of wetland vegetation, provide for easier maintenance, and create a more natural appearance.
Stormwater pond benches:
 The maximum slope of the safety bench is 5%.
An aquatic bench should have a maximum depth of 18 inches below the normal pool
water surface elevation.
Liners: When a stormwater pond is located over highly permeable soils or fractured bedrock, a
liner may be needed to sustain a permanent pool of water. Acceptable liners include (1) a clay
liner consistent with the criteria in Stormwater Design Specification No. 14, (2) a 30-mil poly
liner, (3) bentonite, (4) use of chemical soil additives, or (5) an engineering design approved by
the local regulatory authority.
Inlet pipe inverts should generally be located at or slightly below the permanent pool elevation.
Inlet areas should be stabilized to ensure that non-erosive conditions exist during storm
events up to the overbank flood event (10-year design storm).
 Since most wet ponds are typically on-line facilities, they need to be designed to safely pass the
maximum design storm (e.g., the 10-year and 100-year design storms).
Level 1 designs may incorporate extended detention associated with the treatment
volume of up to 12 inches of detention storage above the permanent pool (at least 10%
of the Level 2 surface area) at its maximum water surface elevation. The maximum ED
and channel protection detention levels can be up to 5 feet above the wet pond
permanent pool elevation. Show the elevations of permanent pool treatment volume and maximum design water surface
 Show the elevations of permanent pool, treatment volume and maximum design water surface elevations for all appropriate design storms and safety storms
Proper surface area/depth allocations for permanent pool and any shallow marsh/constructed
 wetlands

	_ The embankment cross-section must be designed to provide an adequate factor of safety to
	protect against sliding, sloughing, or rotation in the embankment or foundation. Slope stability
	depends upon:
	Physical characteristics of the fill materials
	Configuration of the site
	Foundation materials
	Shear strength
	Compressibility
	Permeability Permeability
	Internal drainage systems in embankments (e.g., drainage blankets, toe drains, etc.) should be
	designed so that the collection conduits discharge downstream of the embankment at a location
	where access for observation is possible by maintenance personnel.
	Adequate erosion protection is recommended along the contact point between the face of the
	embankment and the abutments, where runoff concentrates.
	Evaluate whether a gutter surface other than sod is necessary (riprap is generally
	preferred over a paved concrete gutter).
	Pond drain: Except for flat areas of the coastal plain, each wet pond should have a drain pipe
	that can completely or partially drain the permanent pool.
	In cases where a low level drain is not feasible (such as in an excavated pond), a pump
	wet well should be provided to accommodate a temporary pump intake when needed to
	drain the pond.
	The drain pipe should have an up-turned elbow or protected intake within the pond, to
	prevent sediment deposition, and a pipe diameter capable of draining the pond within
	24 hours.
	The pond drain must be equipped with an adjustable valve located within the riser,
	where it will not be normally inundated and can be operated in a safe manner.
	Trees, shrubs or any other woody plants should not be planted or allowed on the embankment
	or adjacent areas extending at least 25 feet beyond the embankment toe and abutment
	contacts.
	Safety features:
-	The principal spillway opening must be designed and constructed to prevent access by
	small children.
	An emergency spillway and associated freeboard must be provided in accordance with
	Stormwater Design Specification No. 14 and applicable local or state dam safety
	requirements.
	Manage the contours of the stormwater pond to eliminate drop-offs or other safety
	hazards.
	Indicate the top of embankment elevations: constructed height and settled height (allowing for
	10% settlement).
	Show the existing ground and proposed improvements profile along the center line of the
	embankment.
	Show the existing ground and proposed improvements profile along the center line of the
	principal spillway Provide a typical grading section through the pond, including typical side slopes with the aquatic
-	
	bench, shoreline protection, etc.
	Show the dimensions of zones for any zoned embankment
2 5000	nama Cantral
s. seep	page Control
	All utility conduits (except the principal spillway) should be installed away from the embankment.
	When utility conduits through the embankment cannot be avoided, they should meet the
	requirements for spillways:
	Watertight joints
	No gravel bedding
	Restrained to prevent joint separation due to settlement

. The contact point between the embankment soil, the foundation material, and the conduit is the
most likely location for piping to occur, due to the discontinuity in materials and the difficulty in
compacting the soil around the pipe.
 Phreatic line (4:1 slope measured from the principal spillway design high water elevation
through the embankment) is the upper limit of the saturation zone
At a minimum, this should be the 10-year design storm water surface elevation.
If the phreatic line intersects the downstream slope of the embankment, a qualified soil
scientist should be consulted to decide if additional controls, such as an internal drain,
are needed.
Seepage control should be included in the design if the following conditions exist:
Pervious layers in the foundation are not intercepted by the cutoff.
Possible seepage from the abutments may create a wet embankment.
The phreatic line intersects the downstream slope.
Special conditions exist that require drainage to ensure a stable embankment.
Seepage may be controlled by:
Foundation, abutment or embankment drains.
A downstream drainage blanket.
A downstream toe drain (often desirable for homogeneous embankments).
A combination of these measures.
Seepage along pipe conduits that extend through an embankment should be controlled by use
 of the following to prevent piping failures along conduit surfaces:
Anti-seep collar (provide detail).
The Bureau of Reclamation, the U.S. Army Corps of Engineers, and the USDA
no longer recommend the use of anti-seep collars, in deference to graded filters
or filter diaphragms and drainage blankets (more complex to design, but less
complicated and more cost-effective to construct and allow for easier placement
of fill material).
Size, based on the length of pipe in the saturation zone (aim is a minimum 15%
increase in seepage length).
Spacing and location of collars on barrel:
Maximum collar spacing is 14 times the minimum projection above the
pipe.
Minimum collar spacing is 5 times the minimum projection above the
pipe.
Collar dimensions should extend a minimum of 2 feet in all directions
around the pipe.
Anti-seep collars should be placed within the saturation zone. Where the
spacing limit will not allow this, then at least one collar must be in the saturation
zone.
All anti-seep collars and their connections to the conduit should be completely
water-tight and made of material compatible with the conduit. NOTE: Dimple
bands are <i>not</i> considered water-tight.
Metals must be shielded from dissimilar materials with rubber or plastic
insulation at least 24 mils thick.
Anti-seep collars should be placed a minimum of 2 feet from pipe joints unless
flanged joints are used.
· ·
Collars size should be calculated using the procedure specified in Chapter 13 of
the Virginia Stormwater Management Handbook (2011).
The embankment filter and drainage diaphragm should be designed by a professional
geotechnical engineer.
These devices channel seepage flow through a filter of fine graded material,
such as sand, which traps any embankment material being transported.
The flow is then conveyed out of the embankment through a perforated toe
drain or other acceptable technique.
The critical design element: the filter material grain size distribution is based on
the grain size distribution of the embankment fill and foundation material.

		The diaphragm should consist of sand, meeting fince concrete aggregate requirements (at least 15% passing the No. 40 sieve, but no more than 10% passing the No. 100 sieve). The diaphragm should be a minimum of 3 feet thick and should extend vertically upward and horizontally at least 3 times the pipe diameter and vertically downward at least 24 inches beneath the barrel invert, or to rock, whichever is encountered first.
		The diaphragm should be placed immediately downstream of the cutoff trench, approximately parallel to the centerline of the dam. The diaphragm should be discharged at the downstream toe of the
		embankment. The opening sizes for slotted and perforated pipes in drains must be designed using the filter criteria.
		A second filter layer may be required around the drain pipe in order to alleviate the need for many very small openings. Fabric should <i>not</i> be used around the perforated pipe as it may clog, rendering the perforations impenetrable to water.
		rendening the perforations impenetrable to water.
4.		nd Cut Off Trench or Key Trench
	constructi	materials sence of rock in the embankment foundation area requires specific design and ion recommendations (provided by the geotechnical engineering analysis) to ensure a and between the foundation and the embankment.
	Generally If a	r, no blasting should be permitted within 100 feet of the foundation and abutment area. blasting is necessary, it should be carried out under controlled conditions to reduce dverse effects on the rock foundation (e.g., over-blasting, opening fractures, etc.), specially critical in karst topography.
		the cut-off trench bottom width (4 foot minimum or greater as specified in the
	Indicate tl	ical report). he cut-off trench depth (4 foot minimum or as specified in the geotechnical report) he cut-off trench side slopes (no steeper than 1H:1V).
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5. —	Principal Virginia S The princ	ser and Barrel System spillways should be sized according to calculation procedures in Chapter 13 of the Stormwater Management Handbook (2011). ipal spillway should be located within the embankment and accessible from dry land to asy access for maintenance.
	A	ccess to the riser should be provided by lockable manhole covers and manhole steps rithin easy reach of valves and other controls.
	Drop inlet F	schedule of materials and clearly label them in drawings. spillways (riser and barrel system) should be designed as follows: ull flow is established in the outlet conduit and riser at the lowest hydraulic head over ne riser crest that is feasible. Indicate the crest elevation of riser structure. The facility must operate without excessive surging, noise, vibration, or vortex action at any stage.
	_	Therefore, the riser must have a larger cross-sectional area than the outlet conduit.
	headwall surface a	or conduit spillways consist of a pipe extending through an embankment with a at the upstream end. The headwall is typically oversized to provide an adequate gainst which to compact the embankment fill.
	W	ways should be designed as follows: /hen used as the principal spillway, it should be armored with concrete or other non-rosive material.
	A	t the spillway, armoring should extend from the upstream face of the embankment to a oint downstream of the spillway toe.

All principal spillways should be constructed of non-erosive material with an anticipated life
expectancy similar to that of the stormwater management facility.
Pre-cast riser structures may not be substituted if the plans call for a cast-in-place structure,
unless approved by the design engineer and the plan approving authority.
Sections of pre-cast structures must be anchored together to meet stability and flotation
requirements.
_ A separate principal spillway and emergency spillway is generally recommended, unless:
Topography/abutments too steep.
Existing or proposed development conditions impose constraints.
Other factors (e.g., a road embankment is used as the dam, the basin is excavated,
etc.) In such instances, a combined principal/emergency spillway that passes both low flows
and extreme flows may be considered for use, in the form of a drop inlet spillway, a
headwall/conduit spillway, or some other design that achieves equivalent results.
It is very important to protect such combined spillways from clogging.
Conduits/structures through embankments:
Limit the number of conduits that penetrate through the embankment.
Indicate the barrel diameter, inverts, and slope (%).
Show the inverts and dimensions of control release orifices/weirs
Show the structure dimensions
Show the extended detention (if added) orifice protection
A cause of embankment failure is the separation of pipe joints due to differential
settlement and pipe deflection.
All connections to pipes must be completely water-tight.
The drain pipe (or barrel) connection to the riser should be welded all around
when both are metal.
A rubber or neoprene gasket should be used when joining pipe sections. The end of each pipe should be re-rolled by enough corrugations to fit the band
width.
Helically corrugated pipe should have either continuous welded seams or lock
seams with internal caulking or a neoprene bead.
The following connection types are acceptable:
For pipes less than 24 inches in diameter:
Flanges with gaskets on both ends of the pipe
A 12-inch wide standard lap type band with a 12-inch wide by
½-inch thick closed cell circular neoprene gasket.
A 12-inch wide hugger type band with O-ring gaskets having a
minimum diameter of 3/8 inch greater than the corrugation
depth.
For pipes ∃ 24 inches in diameter:
A 24-inch long annular corrugated band using rods and lugs.
A 24-inch wide by 3/8 inch thick closed cell circular neoprene
gasket.
Corrugated metal pipe (CMP) must meet or exceed the minimum required design thickness.
Steel pipe and its appurtenances should be galvanized and fully bituminous-
coated and should conform to the requirements of AASHTO Specification M-
190 Type A with water-tight coupling bands.
Any bituminous coating damaged or otherwise removed should be
replaced with cold-applied bituminous coating compound.
Steel pipes with polymeric coatings should have a minimum coating
thickness of 0.01 inches (10 mils) on both sides of the pipe.
Coated corrugated steel pipe should meet the requirements of
AASHTO M-245 and M-246; the following coatings or an approved
equivalent may be used: Nexon, Plasti-Cote, Blac-Clad, and Beth-Cu-
Lov

 Aluminum coated steel pipe and its appurtenances should conform to the requirements of AASHTO Specification M-274 with water-tight coupling bands
or flanges.
Any aluminum coating damaged or otherwise removed should be replaced with cold-applied bituminous coating compound.
 Aluminum pipe and its appurtenances should conform to the requirements of
AASHTO Specification M-196 or M-211 with water-tight coupling bands or
flanges. Aluminum surfaces that are to be in contact with concrete should be
painted with one coat of zinc chromate primer, and hot-dipped
galvanized bolts may be used for connections.
The pH of the surrounding soils should be between 4 and 9.
 The contractor and project inspector should verify the metal thickness,
corrugation size, proper connecting bands, and gasket type. Maximum allowable deflection of CMP conduits is 5% of the pipe diameter.
 Water-tight joints are necessary to prevent infiltration of embankment soils into
 the conduit.
All joints must be constructed as specified by the pipe manufacturer.
Field joints (the ends of the pipes are cut off in the field) should <i>not</i> be
accepted With larger pipe sizes, it may be difficult to get water-tight joints, even if
the deflection is within design parameters.
In such cases, the designer may choose to specify a heavier gage pipe.
 Bands:
All connectors must be composed of the same material as the pipe.
Metals must be shielded from dissimilar materials with rubber or plastic insulation at least 24 mils thick.
6-inch hugger bands and "dimple bands" should not be accepted for
CMP conduits.
For pipes ≤ 24 inches in diameter, use 12-inch wide bands with 12-inch
O-ring or flat neoprene gaskets.
For larger pipes, use 24-inch wide bands with 24-inch wide flat gaskets
and four "rod and lug" type connectors. Flanged pipe with gaskets may also be used.
All pipe gaskets should be properly lubricated with the material provided
by the manufacturer, and tensioned, to prevent deterioration of the
gasket material.
Flat gaskets must be factory welded or solvent-glued into a
circular ring, with no overlaps or gaps The pipe should be firmly and uniformly bedded throughout its length:
 Where rock or soft, spongy or other unstable soil is encountered, it
should be removed and replaced with suitable soil that is subsequently
compacted to provide adequate structural support.
Under no conditions should gravel bedding be placed under a conduit
through the embankment. Installation of a concrete pipe cradle will help to reduce the risk of piping under
 the barrel and the subsequent failure of the embankment, resulting from
differential settlement.
The concrete cradle may not be necessary along the entire length of
the conduit to prevent piping, but it is recommended since gravel
bedding under an embankment conduit is <i>never</i> appropriate unless it is designed as a filter or drainage diaphragm
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If the external load (e.g., from height of the embankment, anticipated construction traffic, the weight of compaction equipment, etc.) on the barrel is enough to warrant provision for its maximum supporting strength, then a concrete cradle should be installed along the conduit's entire length.
 Reinforced concrete pipe should have bell and singular spigot joints with rubber gaskets
and should equal or exceed ASTM Designation C-361. Bell and spigot pipe should be placed with the bell end upstream.
Joints should be made consistent with manufacturer recommendations.
After the joints are sealed for the entire run of pipe, the bedding should be
placed so that all spaces under the pipe are filled.
All reinforced concrete pipe conduits should be laid in a concrete
bedding for their entire length.
This bedding should consist of high slump concrete placed under the
pipe and up the sides of the pipe at least 25% of its outside diameter, and preferably to the spring line, with a minimum thickness of 3 inches,
or otherwise as shown on the drawings.
Care should be taken to prevent any deviation from the original line and grade
of the pipe.
Polyvinyl Chloride (PVC) pipe should be PVC-1120 or PVC-1220 conforming to ASTM
D-1785 or ASTM D-2241.
Joints and connections to anti-seep collars should be completely water-tight.
The pipe should be firmly and uniformly bedded throughout its length.
Where rock or soft, spongy or other unstable soil is encountered, it should be removed and replaced with suitable soil that is subsequently
compacted to provide adequate structural support.
All conduits penetrating dam embankments should be designed using the following
criteria:
Conduits and structures penetrating an embankment should have a smooth
surface without protrusions or indentations that will hinder compaction of
embankment materials.
All conduits should be circular in cross-section except cast-in-place reinforced concrete box culverts. This is also true where multiple conduits are employed.
Conduits should be designed to withstand the external loading from the
proposed embankment without yielding, buckling or cracking, all of which will
result in joint separation.
Conduit strength should not be less than the values shown in the design
specifications for corrugated steel, aluminum, and PVC pipes, and the
applicable ASTM standards for other materials.
The designer or contractor should obtain a manufacturer's certification
that the pipe meets plan requirements for design load, pipe thickness, joint design, etc.
Inlet and outlet flared-end sections should be made from materials that are
compatible with the pipe.
All pipe joints should be made water-tight by using flanges with gaskets,
coupling bands with gaskets, bell and spigot ends with gaskets, or by welding.
Where multiple conduits are employed, sufficient space should be provided
between the conduits and installed anti-seep collars to allow for backfill material
to be placed between the conduits with earth-moving equipment and easy access by hand-operated compaction equipment.
The distance between conduits should be ∃ 1/2 of the pipe diameter, but not less than 2 feet.
Cathodic protection should be provided for coated welded steel and galvanized
 corrugated metal pipe when soil and resistivity studies indicate the need for a protective
coating against acidic soils.

Outlet protection must be used for the downstream toe of a spillway structure to help dissipate
the high-energy flow through the spillway and to prevent excessive erosion in the receiving channel.
The type of outlet protection depends on the flow velocities associated with the spillway.
Riprap is the preferred form of outlet protection, designed according to Chapter 13 of
the Virginia Stormwater Management Handbook (2011) and the Virginia Erosion and
Sediment Control Handbook (1992). Gabion baskets are also an acceptable outlet
protection material.
The bottom of the riprap apron should be constructed at 0% slope along its
length.
The end of the apron should match the grade and alignment of the receiving channel.
If the receiving channel is well-defined, the riprap should be place on the
channel bottom and side slopes (no steeper than 2H:1V) for the entire length,
as required in the design criteria in Chapter 13 of the <i>Virginia Stormwater</i>
Management Handbook (2011) and the Virginia Erosion and Sediment Control
Handbook (1992).
Riprap placement should not alter the channel's geometry.
Excavation of the channel bed and banks may be required to construct the full
thickness of the apron.
If the barrel discharges into the receiving channel at an angle, the opposite
bank must be protected up the the 10-year storm elevation. In no instance
should the total length of outlet protection be shortened.
If a permit requires that no work may be performed in the stream or channel,
then the outlet structure must be moved back to allow for adequate protection. The horizontal alignment of the apron should have no bends within the design
length.
Additional riprap should be placed if a significant change in grade occurs at the
downstream end of the outfall apron.
Filter fabric should be placed between the riprap and the underlying soil to
prevent soil movement into and through the riprap.
All control structures should have a trash rack or debris control device, designed as follows:
All trash rack and debris control components should be made of stainless steel or
galvanized metal meeting VDOT specifications.
Trash racks attached to a concrete spillway structure should be secured with stainless
steel anchor bolts.
Openings for trash racks should be no larger than 1/2 of the minimum conduit dimension and, to discourage child access, bar spacing should be no greater than 1 foot
apart. The clear distance between the bars on large storm discharge openings generally
should be no less than 6 inches.
Flat grates for trash racks are <i>not</i> acceptable.
Inlet structures that have flow over the top should have a non-clogging trash rack (e.g.,
a hood-type inlet that allows passage of water from underneath the trash rack into the
riser, or a vertical or sloped grate).
The designer should verify that the surface area of the vertical perimeter of a raised
grate equals the area of the horizontal top opening, to allow adequate flow passage
should the top horizontal surface become clogged.
Metal trash racks and monitoring hardware should be constructed of galvanized or stainless steel.
Methods to prevent clogging of extended detention orifices in dry extended detention
basins should be carefully designed, since these orifices are usually very small and
located at the invert or bottom of the basin.
 All drop inlet spillways designed for pressure flow should have adequate anti-vortex devices (not
 required if weir control is maintained in the riser through all flow stages, including the maximum
design storm or safety storm):

	The device may be a baffle or plate installed on top of the riser, or a headwall set on
	one side of the riser. The design of a principal spillway riser structure should include a <i>flotation</i> or <i>buoyancy</i> calculation (see Chapter 13 of the <i>Virginia Stormwater Management Handbook, 2011</i>).
	The downward force of the riser and footing (to which the riser must be firmly attached) is the <i>structure weight</i> , which must be 1.25 times greater than the buoyant force acting on the riser.
	Stormwater management facilities having permanent impoundments may be designed so that the permanent pool can be drained to simplify maintenance and sediment removal.
	The draining mechanism will usually consist of a valve or gate attached to the spillway structure and an inlet pipe projecting into the reservoir area, with a trash rack or debris control device.
	The typical configuration of a drainpipe will place the valve inside the riser structure with the pipe extending out to the pool area.
	This configuration results in the drainpipe being pressurized by the hydraulic head associated with the permanent pool.
	Pressurized pipes should have mechanical joints in order to avoid possible leaks and seepage resulting from the innate pressure.
	In all cases, valves should be secured to prevent unauthorized draining of the facility.
	Basin drains should be designed with sufficient capacity to pass the 1-year frequency design storm with limited ponding in the reservoir area, so that sediment removal and other maintenance functions are not hampered.
	An uncontrolled or rapid drawdown of a stormwater basin could cause a slide in the saturated upstream slope of the dam embankment or shoreline area. Therefore, the design of the basin drain system should include specific
	operating instructions for the owner Generally, the drawdown rate should not exceed 6 inches per day.
	For embankment or shoreline slopes of clay or silt, the drawdown rate may be as low as 1 inch per week to ensure slope stability.
6 Em	nergency Spillway
	Vegetated emergency spillways must be built in existing, undisturbed earth/rock or "cut" in the abutments at one or both ends of an earthen embankment or ovr a topographic saddle anywhere on the periphery of the basin. They should <i>never</i> be located on any portion of the
	embankment fill material. Excavated emergency spillways consist of three elements:
	An inlet channel, through which subcritical flow enters the spillway.
	The inlet channel should have a straight alignment and grade.
	The cross-sectional area of flow in the inlet channel should be large in comparison to the flow area at the control section.
	Where the depth of the channel changes to provide for the increased flow area,
	the bottom width should be altered gradually to avoid abrupt changes in the
	shape of the sloping channel banks.
	A level section, which controls the depth of flow. The maximum design water surface elevation (normally for the 100-year storm)
	through the emergency spillway should be at least 1 foot lower than the settled top of the embankment and should be confined by undisturbed earth or rock.
	The bottom width of the spillway should not exceed 35 times the design depth of flow, to avoid damage by meandering flow and accumulated debris.
	Whenever the required bottom width is likely to be excessive, consideration should be given to incorporation of a spillway at each end of the dam.
	The two spillways do not need to be of equal width if their total capacity meets design requirements.

	An exit channel, through which either <i>critical</i> or <i>supercritical</i> flow discharges from the
	spillway The alignment of the exit channel must be straight to a point far enough below
	the embankment to ensure that any flow escaping the exit channel cannot
	damage the embankment.
	The exit channel should have the same cross-section as the control section.
	The slope of the exit channel must be:
	Adequate to discharge the peak flow within the channel.
	No greater than that which will produce maximum permissible velocities
	for the soil type or the planned grass cover The slope range of the exit channel is selected to ensure supercritical
	flow in the channel.
	The control section is the point on the spillway where the flow passes through <i>critical</i> depth, usually installed close to the intersection of the earthen embankment and the
	emergency spillway centerlines. The type of soil and vegetative cover used in the emergency spillway can be used to establish
	the spillway design dimensions and geometry.
	Vegetation provides a degree of retardance to the flow through the spillway, depending
	mostly on the height and density of the vegetative cover chosen.
	Hydraulic design for emergency spillways must be done in accordance with criteria provided in <i>Appendix C: Vegetated Emergency Spillways</i> of the <i>Introduction to the New Virginia Stormwater Design Specifications</i> (as posted on the Virginia Stormwater BMP Clearinghouse web site at
	http://www.vwrrc.vt.edu/swc/NonProprietaryBMPs.html) and in Chapter 13 of the Virginia
	Stormwater Management Handbook (2011).
	Spillway side slopes should be no steeper than 3H:1V unless the spillway is excavated into rock.
	Show the existing ground and proposed improvements along the center line of the emergency
	spillway
C. Ian	dscape Plan
O. Lan	The landscaping plan must indicate the methods to be used to establish and maintain vegetative
	cover in the Wet Pond and its buffer area, including the following:
	Delineation of pondscaping zones within both the pond and buffer.
	Delineation of pondscaping zones within both the pond and buffer Selection of corresponding plant species.
	Delineation of pondscaping zones within both the pond and buffer. Selection of corresponding plant species. The planting plan.
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	Delineation of pondscaping zones within both the pond and buffer. Selection of corresponding plant species. The planting plan. The sequence for preparing the wetland benches (including soil amendments, if needed). Sources of native plant material. Elements that promote diverse wildlife and waterfowl use within the wet pond and buffer. Woody vegetation may not be allowed to grow within 15 feet of the toe of the embankment nor within 25 feet from the principal spillway structure. A vegetated buffer should be provided that extends at least 25 feet outward from the maximum water surface elevation of the wet pond. Permanent structures (e.g., buildings) should not be constructed within the buffer area. Existing trees within the buffer area should be preserved during construction. Due to soil compaction, planting holes should be 3 times deeper and wider than the diameter of the root ball for ball-and-burlap stock, and 5 times deeper and wider for container-grown stock. Avoid species that require full shade, or are prone to wind damage. Extra mulching around the base of trees and shrubs is strongly recommended as a means of conserving moisture and suppressing weeds. Provide a planting schedule and specifications (transport / storage / installation / maintenance)
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D.	Construction Notes	
	Ideally, planned wet pond areas should be constructed after the contributing draina	ge area is
	completely stabilized.	
	Wet pond areas may be used during construction as sites for temporary sedimer	nt traps or
	basins (properly sized for E&S control purposes), provided the construction plans inc	lude notes
	and graphical details specifying the facility will be de-watered, dredged and re-graded	to design
	dimensions after the original site construction is complete.	
	Installation of the permanent riser should be initiated during the construction p	hase
	Design elevations should be set with final cleanout of the sediment	
	conversion to the post-construction wet pond in mind.	
	The bottom elevation of the permanent wet pond should be lower than t	he bottom
	elevation of the temporary sediment basin.	
	Appropriate procedures should be implemented to prevent discharge of tur	bid waters
	when the basin is being converted into a wet pond.	
	In some cases, it will be necessary to divert flow while the wet pond is being construct	ed, so that
	no sediment flows into the pond area until installation and stabilization are complete.	
	Flow diversions may be required to meet additional requirements of and obtain	ain permits
	from state and federal regulatory agencies.	
	Construction sequence:	
	Construction inspections should occur before, during and after installation to	ensure the
	stormwater wetland is constructed according to specifications.	
	Use detailed inspection checklists that require sign-offs by qualified	
	at critical states of construction, to ensure the contractor's interpreta	tion of the
	plan is consistent with the designer's intent.	
	The following are critical inspection points:	
	During initial site preparation and installation of E&S Controls.	,
	Excavation and grading (e.g., interim and final elevations).	
	Installation of the embankment, the riser/primary spillway, and	the outlet
	structure.	
	Pondscaping installation and final stabilization.	
	Check the proposed site for existing utilities prior to any excavation.	
	Assemble the construction materials on-site, making sure they me	et design
	specifications, and prepare any staging areas.	
	Clear, grub and strip the areas designated for borrow sites, embankment co	
	and structural work to the desired subgrade, removing all trees, vegetation,	roots and
	other objectional material.	1
	All cleared and grubbed material should be disposed of outside and	below the
	limits of the embankment and reservoir.	
	When specified, a sufficient quantity of topsoil should be stockpiled in	a suitable
	location for use on the embankment and other designated areas.	
	Install applicable temporary E&S control measures prior to construction.	ıtlat) nina
	Excavate the core trench for the embankment and install the spillway (or	iliet) pipe,
	including the downstream rip-rap apron (energy dissipation) protection The cutoff trench should be excavated into impervious material along	or parallal
	to the centerline of the embankment.	oi parallei
	Trench side slopes should be laid back in steps at a 1H:1V slope	or flattor
	(from page 6; conflicts with 2:1 specified on page 10, Earthen Em	
	Spec?).	ibankineni
	Backfill should be compacted with construction equipment, rollers	e or hand
	tampers to assure maximum density and minimum permeability.	, oi Hallu
	Install the riser pipe or overflow structure, ensuring the top invert of the overf	low wair ie
	constructed level and at the proper design elevation.	TOM MEII 19
	Constructed level and at the proper design elevation. ———— Construct the embankment and any internal berms in 8- to 12-inch lifts, comp	acted with
	appropriate equipment.	aciou Willi
	Areas on which fill is to be placed should be scarified before its placer	nent
	Aicas on which hir is to be placed should be scanned before its placer	HOHIL.

 The most permeable borrow material should be placed in the downstream portions of the embankment.
 Install the principal spillway or overflow weir concurrently with fill placement and not excavated into the embankment. A vertical trench through the embankment
material (in order to place the spillway pipe) should not be allowed under any
circumstances.
Ensure that the top invert of the principal spillway or any overflow weir is constructed level and at the proper design elevation (at least 1 foot
below the crest of the emergency spillway). Flashboard risers are strongly recommended for use in constructed wetlands.
Filter and Drainage Layers:
 In order to achieve maximum density of clean sands, filter layers should
be flooded with clean water and vibrated just after the water drops below the sand surface.
The filter material should be placed in lifts of no more than 12 inches in thickness.
Up to 4 feet of embankment material may be laced over a filter material layer before excavating back down to expose the previous layer.
After removing any unsuitable materials, the trench may be filled with
additional 12-inch lifts of filter material, flooded, and vibrated as
described above, until the top of adjacent fill is reached.
The contractor should ensure that a qualified professional inspect filter
and drainage diaphragms, ensuring that backfill material meets specifications for quality, lift thickness, placement, moisture content,
and dry unit weight.
 Fill material should be taken from an approved, designated borrow area or
stockpile.
Fill material should be free of roots, stumps, wood, rubbish, stones
greater than 6 inches in diameter, and frozen or other objectionable materials.
Fill material for the center of the embankment and the cutoff trench
should conform to Unified Soil Classification GC, SC, or CL.
Fill material that is beside pipes or structures should be of the same
type and quality as specified for the adjoining fill material. The fill material should be placed in horizontal lifts not to
exceed 4 inches in thickness and compacted by hand tampers or other manually directed compaction equipment.
The material should completely fill all spaces under and beside
the pipe.
During backfilling, equipment should not be driven closer the 4 feet horizontally to any part of a structure.
Equipment should <i>NEVER</i> be driven <i>over</i> any part of a
structure or pipe, unless compacted fill has been placed to a
depth specified by the structural live load capacity of the structure or pipe, that adequately distributes the load.
Consideration may be given to the use of other materials in the
embankment based on the recommendation of a geotechnical engineer
supervising the design and construction.
The surface layer of compacted fill should be scarified prior to
placement of at least 6 inches of topsoil, which must be properly
stabilized. Fill material should be compacted with appropriate compaction equipment.
 The number of necessary passes by the compaction equipment over
the fill material may vary with soil conditions.
Fill material should contain sufficient moisture so that the required
degree of compaction will be obtained with the equipment used.

	The minimum required density is 95% of maximum dry density with a moisture content within ± 2% of the optimum, unless otherwise specified by the engineer. Each layer of fill should be compacted as necessary to obtain minimum
	density. Compaction tests should be performed regularly throughout the embankment construction.
	Typically, one test per 5,000 sq. ft. on each layer of fill or as directed by the geotechnical engineer.
	Use either a Standard Proctor Test (ASTM D698) or a Modified Proctor Test (ASTM D1557 – usually more appropriate for earthen dams). A new Proctor test is required if the material changes from that previously tested.
	The engineer should certify, at the time of construction, that each fil layer meets the minimum density.
	A geotechnical or construction inspector should be on site during embankment
	construction to do the following:
	Test fill compaction
	Observe foundation preparation.
	Observe pipe installation. Observe riser construction.
	Observe fiser construction. Observe filter installation, etc.
Const	ruct the emergency spillway in cut or structurally stabilized soils.
	rate/grade until the appropriate elevations and desired contours are achieved for
	ottom and side slopes of the pond.
	outlet pipes, including the downstream rip-rap apron (energy dissipation)
protec	
areas	ize exposed soils with temporary seed mixtures appropriate for the pond buffer. All above the normal pool elevation should be temporarily stabilized by hydroseeding eding over straw.
	the pond buffer area and implement any remaining permanent stabilization
meas	· · · · · · · · · · · · · · · · · · ·
	uct a final inspection, log the GPS coordinates for each facility and submit them for into the local BMP maintenance tracking database.
Chapter 9, Append	s (can include BMP Operation & Maintenance Inspection Checklists from dix 9-C of this Handbook)
Provide a Ma	aintenance Agreement, indicating the person or organization responsible for
inspection che	
	le a Maintenance Narrative which describes the long-term maintenance
	rements of the facility and all components, including installation/maintenance of removal and disposal of trash, debris and sediment accumulations;
	ng; and periodic harvesting and disposal of overgrown or old aquatic plant
	ed restriction, drainage easement, and/or other enforceable mechanism, including
	ites of the area, to ensure the wet pond is not converted to other uses. ient facility access from the public ROW or roadway to both the wet pond and any practices.

IV. COMMENTS		
-		
	Ву:	Date:

8-A.16.0. EXTENDED DETENTION PONDS: DESIGN CHECKLIST

Plan Submission Date	
Project Name	
Site Plan/Permit Number	
Practice No./Location on Site	
Owner_	Phone Number
BMP Designer	Phone Number
General Contractor	Phone Number
Signature and stamp of licensed profe certification	essional design consultant and owner
Plan Status	
Approved Legend: Not Approved	Inc.N/ACompleteIncomplete/IncorrectNot Applicable
Facility Type: Level 1	Level 2
Design Configuration: ☐ Micropool ED Pond ☐ Wet ED Pond (see Stormwater Design Specification No. 14) ☐ Limited ED above Wetlands (see Stormwater Design Specification No. 13)	ype of Pre-Treatment Facility: Sediment forebay (above ground) Vegetated buffer area Grass filter strip Grass channel Other:
Hydraulic Configuration: ☐ On-line facility ☐ Off-line facility	
I. SUPPORTING INFORMATION	
ED ponds with high embankments or large drainal under the Virginia Dam Safety Act and Regulation Provide a concise narrative describing the store this practice fits into the overall plan, and stating Show the location of this BMP on the site map, in The basin pool area The contributing drainage area (CDA) be sustain a permanent water level within the Delineation of FEMA 100-year floodplain Areas of site compensated for in water quere Provide topography for the site area, including the practices. Provide the geotechnical report with recommendation description of any borrow area involved. Provide a soil map for site and area of facility, income Show the soil boring locations and provide the second control of the second control of the soil boring locations and provide the second control of the second co	ns, requiring a state permit. mwater management strategy, describing how all assumptions made in the design. cluding: oundaries, acreage and land cover, sufficient to e constructed wetland. uality calculations e ED pond area, its CDA and any pre-treatment endations and earthwork specifications and a
and soil descriptions. Borings should be taken below the p proposed outlet area, and in at least tw area.	proposed embankment, in the vicinity of the olocations within the planned basin treatment

Determine the physical characteristics of the soils regarding:
Infiltration rate: infiltration through the bottom of the pond is encouraged unless
it will impair the integrity of the embankment.
Suitability for use as structural fill or spoil.
Bearing capacity, buoyancy, etc. pertaining to outlet structure design.
Compaction/composition needs for the embankment.
Depth to groundwater and bedrock not less than 2 feet below the floor of the
pond.
Evaluation of potential infiltration losses (and the consequent need for a liner).
ED ponds are normally combined with other stormwater treatment options within those facilities
(e.g., wet pond, constructed wetland) to enhance their performance and appearance.
ED ponds are generally discouraged for use in karst areas and should be considered the
 practice of last resort. If karst is present, a detailed geotechnical investigation is recommended
to ensure the ED pond does not aggravate potential karst impacts (e.g., sinkholes, groundwater
contamination, etc.):
A minimum of 3 feet of unconsolidated soil material must exist between the bottom of
the pond and the top of the underlying karst layer.
Employ an impermeable liner that meets the requirements of Stormwater Design
Specification No. 13 (Constructed Wetlands).
Annual maintenance inspections must be conducted to detect sinkhole formation.
Sinkholes that develop should be reported immediately after they have been observed
and should be repaired, abandoned, adapted or observed over time following the
guidance prescribed by the appropriate local or state groundwater protection authority.
The use of ED ponds is constrained in coastal plain sites due to flat terrain, low
hydraulic head and high water table (constructed wetlands are preferred).
The use of ED ponds is highly constrained at sites with steep terrain.
 Where cold winter climates are typical, make the following adjustments:
 Plant salt-tolerant vegetation at pond benches (to deal with higher chloride content of
road salts).
Do not submerge inlet pipes and provide a minimum 1% pipe slope to discourage
standing water and ice formation.
Place all pipes below the frost line to prevent frost heave and pipe freezing.
Locate low-flow orifices in the micropool, so they withdraw at least 6 inches below the
typical ice layer.
Angle trash racks to prevent ice formation.
If road sanding is prevalent in the CDA, increase the forebay size by 25% to
accommodate additional sediment loading.
ED ponds are poorly suited to treat runoff within open channels located in highway rights-of-
 way, unless storage is available in a cloverleaf interchange or in an expanded right-of-way and
special VDOT design criteria are used.
ED ponds are generally not recommended in watersheds containing trout streams, due to the
 potential for stream warming.
However, where other upland runoff reduction practices cannot meet the full Channel
Protection Volume requirement, a micropool ED pond may be used if the following
criteria are met:
It must be designed with a maximum 12-hour detention time
It must have a minimum pool volume sufficient to prevent clogging
It must be planted with trees so it becomes fully shaded
It must be located outside of any required stream buffer areas.
An ED pond should <i>not</i> be built within an existing perennial stream or natural wetland nor should
 an ED pond discharge to jurisdictional waters without local/state/federal approvals and the
necessary permit(s).
Identify potential conflicts with other (existing?) structural components (pipes, underground
 utilities, etc.).
The designer should check to see whether sediments removed from the forebay can be spoiled
 (deposited) on-site or must be hauled away.

II. COMPUTATIONS

A.	Hydrology
	Determine runoff curve number (pre- and post-developed conditions), providing the worksheets.
	Determine the time of concentration (pre- and post-developed conditions), providing the
	worksheets.
	Generate hydrographs (pre- and post-developed conditions) for appropriate design and safety
	storms (USDA-NRCS methods or modified rational-critical storm duration method)
	Ensure that there is adequate drainage area and/or base flow
_	
В.	Hydraulics
	Specify assumptions and coefficients used.
	Typically, 6 to 10 feet of hydraulic head are need to drive flow through the wetland.
	Provide a stage-storage table and curve
	Average treatment volume extended detention drawdown time is 24 hours or less for
	Level 1 designs and 36 hours or less for Level 2 designs.
	Vertical treatment volume fluctuation may exceed 4 feet for Level 1 designs but may not
	exceed 4 feet for Level 2 designs.
	Weir/orifice control analysis for riser structure discharge openings and riser crest.
	Consider providing a micropool at the outlet structure.
	The micropool should be designed to that the depth will not draw down by more than 2 feet during a 30 day summer drought, but should be at least 4 feet deep.
	Use a submerged reverse-slope pipe that extends downward from the riser to
	an inflow point at mid-depth of the normal pool or micropool.
	Install a down-turned elbow or half-round CMP over a riser orifice (circular,
	rectangular, V-notch, etc.) to pull water from at least 12 inches below the
	micropool surface.
	Use a perforated pipe under a gravel blanket with an orifice control at the end in the
	riser structure to supplement the primary outlet.
	Carefully design the low-flow orifice to minimize clogging, as follows:
	All outlet pipes should be adequately protected by an acceptable external trash
	racks or by internal orifice protection that may allow for smaller diameters.
	Recommend a minimum 3-inch diameter orifice to minimize clogging of an
	outlet or extended detention pipe when it is surface-fed (still susceptible to
	clogging from floating vegetation and debris).
	Smaller openings (down to 1-inch in diameter) are permissible, using internal
	orifice plates within the pipe.
	Barrel: Conduct an inlet/outlet control analysis
	Conduct a riser/outlet structure flotation analysis (factor of safety = 1.25 min.).
	Conduct appropriate calculations for use as a temporary sediment basin riser with clean out
	schedule & instructions for conversion to a permanent facility.
	Provide for large storm overflow or bypass: emergency spillway adequacy/capacity analysis
	(100-year design storm) with required embankment freeboard.
	Provide a stage-discharge table and curve (provide equations).
	Route post-development hydrographs for appropriate design storms (1-yr., 10-yr., or as required
	by watershed conditions) and safety storms (100-yr. or as required)
	Provide storm drainage and hydraulic grade line calculations.
_	Downstroom imposts
U.	Downstream impacts Conduct a danger reach study
	Conduct a danger reach study.
	Describe the 100 year floodplain impacts. Provide downstream hydrographs at critical study points.
	i iovide devinsticani nydrograpno at entical study politic.

	Demonstrate safe conveyance to an "adequate" receiving channel. If the receiving channel is natural and (1) has never been enhanced or "restored, OR if stream channel erosion or localized flooding is an existing predevelopment condition then conduct appropriate "energy balance" calculations to demonstrate satisfications conveyance from the facility to the receiving channel" (provide computations).	
D.	 Water Quality Provide a tabulation of land cover areas (impervious cover, managed turf, forest cover) in t CDA, pollutant load, pollutant load removal, and treatment volume requirements, all generat by using the Virginia Runoff Reduction Method spreadsheet (provide spreadsheet) Determine specific sizing/dimensions from criteria in Stormwater Design Specification No. 15. 	
III.	PLAN REQUIREMENTS	
A. 	 Show the limits of clearing and grading, noting that they should be identified and protected acceptable signage, silt fence, snow fence, or other comparable barrier. Setbacks (local ordinances rule): Minimum 10 feet from property lines. Minimum 25 feet from building foundations. Minimum 50 feet from septic system drainfields Minimum 100 feet from private wells. Pre-Treatment: Show all pre-treatment practices. A sediment forebay should be considered an integral pre-treatment practice for all Exercises. 	
	ponds. Consider providing an over-sized forebay to trap sediment, trash and deb before it reaches the ED pond's low-flow orifice. The forebay is considered a separate cell in both Level 1 and Level 2 design formed by an acceptable barrier (e.g., earthen berm, concrete weir, gabi baskets, etc.). Any outlet protection associated with the end section or end w should be designed according to state and local standards. A forebay should be located at every major inlet to trap sediment and preser the capacity of the main pond treatment cell. A major inlet is any individual storm drain inlet pipe or open channel conveyi runoff from at least 10% of the ED pond's CDA. The relative size of individual forebays should be proportional to the percenta of the total inflow to the ED Pond. The total volume of all forebays should be at least 15% of the total Treatmed Volume (inclusively, thereby satisfying the Level 1 design permanent por volume requirement). However, a micropool is still encouraged for maintenant benefits. The outlet from each forebay should be designed in such a manner that it are as a level spreader to distribute runoff evenly across the entire bottom surfate area of the main basin treatment cell. Therefore, there should be no low-flepilot channel constructed in the basin bottom. Show the location of the metered rod that monitors long-term sedime accumulation (in the center of the pool, as measured lengthwise along the low water travel path).	ris ris, on rall ve ng ge ent cool cce cts cce cow ent cow
	 Inlets should be stabilized to ensure that non-erosive conditions exist during storevents up to the overbank flood event (the 10-year storm). Inlet pipe inverts should generally be located at or slightly below the forebay posterior. 	
	Show the layout and dimensions of basin features: permanent pool, sediment forebased embankment, emergency spillway, basin side slopes, basin bottom, etc.	ıy,

The footprint is typically between 1% and 3% of the CDA, depending on the pond depth (a deeper pond needs a smaller footprint).
Pool geometry – wet/dry weather flow path
Internal design geometry and depth zones are critical in maintaining the pollutant
removal capability.
Ensure proper orientation and inlet locations to avoid short-circuiting
Ensure that there is adequate surface area
Show the wet/dry weather flow path:
Overall flow path through the wetland (length-to-width ratio):
Level 1 design: 2L:1W.
Level 2 design: 3L:1W.
Internal berms, baffles or topography can be used to extend flow paths
and/or create multiple pond cells.
Ratio of the shortest flow path (closest inlet to the outlet) to the overall length:
Level 1 design: 0.4.
Level 2 design: 0.7.
If unable to meet these targets, then the drainage area served by these
"closer" inlets should constitute no more than 20% of the total CDA.
The permanent pool storage may be divided among multiple cells
A berm or simple weir should be used instead of pipes to separate multiple
pond cells.
ED pond benches:
A safety bench is a flat bench located just outside of the perimeter of the
permanent pool to allow for maintenance access and reduce safety risks when
the pond side slopes exceed 5H:1V.
The safety bench generally extends 8 to 15 feet outward from the
normal water edge to the shoulder of the stormwater pond side slope. An aquatic bench is a shallow area just inside the perimeter of the normal pool
that promotes growth of aquatic and wetland vegetation.
The bench also serves as a safety feature, reduces shoreline erosion,
and conceals floatable trash.
The bench should extend up to 10 feet inward from the normal
shoreline and have an irregular configuration.
Both the safety bench and the aquatic bench should be landscaped with
vegetation that hinders or prevents access to the pool.
Micropool ED ponds should <i>not</i> have a low flow pilot channel, but instead must
be constructed in a manner whereby flows are evenly distributed across the
pond bottom, to promote the maximum infiltration possible.
Other safety features:
End walls above pipe outfalls greater than 48 inches in diameter must be fenced to
prevent a hazard.
The emergency spillway must be located so that downstream structures will not be
impacted by spillway discharges.
Outlet protection per VE&SCH Std. & Spec. 3.18
Stable for the 10-year design storm.
The channel immediately below the pond outfall must be modified to prevent erosion
and conform to natural dimensions in the shortest possible distance.
This is done typically by placing appropriately-sized riprap over filter fabric,
which can reduce flow velocities from the principal spillway to non-erosive
levels (3.5 to 5 ft./sec.).
Flared pipe sections, which discharge at or near the stream invert or into a step/plunge
pool, should be used at the spillway outlet. Indicate the top-of-bank and basin bottom elevations
Indicate the top-of-bank and basin bottom elevations. Indicate the elevations of permanent pool, treatment volume and maximum design water surface
elevations for all appropriate design storms and safety storms

	 Fencing the perimeter of ED ponds is discouraged, except at or above the maximum water surface elevation in the rare instances when the pond slope is a vertical wall. Identify the riser and barrel materials and label their dimensions Identify the pool depth zones on the plan, ensuring adequate surface area for each depth zone Provide sufficient maintenance access to the forebay, micropool, safety benches, riser structure, embankment, emergency spillway, basin shoreline, extended drawdown device, principal spillway outlet, stilling basin, toe drains, and likely sediment accumulation areas. Access roads must:
	Be constructed of load bearing materials able to withstand the expected frequency of
	use.
	Have a minimum width of 12 feet.
	Possess a maximum profile grade of 15%.
	Have sufficient turn-around area.
	A maintenance right-of-way or easement must extend to the stormwater basin from a public or private road.
B. B	MP Section Views & Related Details
1 Pi	re-Treatment
	The forebay should be sized to hold 0.25 inch of runoff per impervious acre of the CDA, but no
	less than 0.1 inch per impervious acre.
	For smaller stormwater facilities, a more appropriate sizing criterion of 10% of the total
	required pool or detention volume may be more practical.
	This volume should be a maximum of 4 feet deep (or a depth determined by the
	summer drought water balance) near the inlet to adequately dissipate turbulent inflow without re-suspending previously deposited sediment, and then transition to a depth of 1 foot at the entrance to the first wetland cell.
	The forebay should be equipped with a variable width aquatic bench around the perimeter of the
	4-foot depth, for safety purposes. The aquatic bench should be 4 to 6 feet wide at a depth of 1 to 2 feet below the water surface, transitioning to zero width at grade.
	The volume of the forebay is part of the treatment volume of the stormwater basin for which it provides pre-treatment.
	However, for dry facilities, the forebay does <i>not</i> represent available storage volume if it remains full of water.
	A dry forebay must be carefully designed to avoid the resuspension of previously deposited sediments.
	The total volume of all forebays should be at least 15% of the total Treatment Volume. The
	relative size of individual forebays should be proportional to the percentage of their total inflow
	to the ED pond.
	Separation between the forebay and the main basin may be achieved through the use of an
	earthen berm, gabion baskets, concrete, or a riprap wall. A designed overflow section should be constructed on the top of the separation to allow flow to
	exit the forebay at non-erosive velocities during the 2-year and 10-year frequency design
	storms.
	The overflow section may be set at the extended detention volume elevation.
	The bottom of the forebay(s) may be hardened (e.g., with concrete, asphalt, or grouted rip-rap)
	to make sediment removal easier.
	Providing a hardened access or staging pad adjacent to the forebay helps protect the forebay
	and basin from excessive erosion from heavy equipment operation used for maintenance. Provide a typical grading section through the forebay, including typical side slopes, aquatic
	bench, shoreline protection, etc.

2.	Embankment (or dam) and Ponding Areas Type of embankment:
	Type of embankment. Homogenous embankment
	Zoned embankment
	The earthen embankment must be designed to be stable against any force condition or combination of force conditions that may develop during the life of the structure (including
	differential settlement within the embankment, seepage through the embankment and
	foundation, or sharing stresses within the embankment and foundation) and is dependent upon: Construction materials
	Construction materials Foundation conditions
	Embankment height and cross-section geometry Normal and maximum pool levels
	Purpose of structure (i.e., extended detention).
	Embankment geometry: Top of dam elevations: constructed height and settled height (allowing for 10%
	settlement).
	Height (based on the freeboard requirements): There must be at least 1 foot of freeboard between the maximum 100-year storm water surface elevation
	(WSE) to the lowest point on the top of the embankment (excluding the
	emergency spillway). An embankment <i>without</i> an emergency spillway must provide at least 2 feet of
	freeboard between the maximum 100-year storm water surface elevation
	(WSE) to the lowest point on the top of the embankment.
	NOTE: The spillway design storm WSE, if specified, may be substituted for the
	100-year storm WSE in either of the above situations.
	Top width varies with embankment height and should be shaped to provide positive
	drainage.
	The top of the embankment must be level in order to avoid possible overtopping in one
	location in cases of extreme storms or spillway failure.
	Embankment slopes should be no steeper than 3H:1V, if feasible, with a maximum
	combined upstream and downstream slope of 5:1 (i.e., 3H:1V downstream face and
	2H:1V upstream face).
	For embankments exceeding 15 feet in height, a 6 to 10 foot wide bench should be
	provided at intervals of 10 to 15 feet of height, particularly if slopes are steeper than
	3H:1V.
	The slope profile within an ED pond should be at least 0.5% to 1% to promote positive
	flow through the pond.
	Basin side slopes should be from 4H:1V to 5H:1V to promote better establishment and growth of
	vegetation, provide for easier maintenance, and create a more natural appearance.
	ED pond benches:
	The maximum slope of the safety bench is 5%.
	An aquatic bench should have a maximum depth of 18 inches below the normal pool
	water surface elevation.
	Inlet pipe inverts should generally be located at or slightly below the permanent pool elevation.
	Inlet areas should be stabilized to ensure that non-erosive conditions exist during storm
	events up to the overbank flood event (10-year design storm).
	Since most ED ponds are typically on-line facilities, they need to be designed to safely pass the
	maximum design storm (e.g., the 10-year and 100-year design storms) with adequate freeboard
	between the maximum design water surface elevation and the top of the embankment.
	Show the elevations of the permanent pool, treatment volume and maximum design water
	surface elevations for all appropriate design storms and safety storms
	The maximum Treatment Volume water surface elevation must not extend more than 5
	feet above the basin floor or normal pool elevation for a Level 1 design, or 4 feet for a
	Level 2 design.
	The maximum vertical elevation for ED and channel protection detention over shallow
	wetlands is 1 foot.

	Larger flood control storms (e.g., the 10-year design storm) may exceed the 5 foot
	vertical limit if they are managed by a multi-stage outlet structure.
	The embankment cross-section must be designed to provide an adequate factor of safety to
	protect against sliding, sloughing, or rotation in the embankment or foundation. Slope stability
	depends upon:
	Physical characteristics of the fill materials
	Configuration of the site
	Foundation materials
	Shear strength
	Compressibility
	Permeability
	_ Internal drainage systems in embankments (e.g., drainage blankets, toe drains, etc.) should be
	designed so that the collection conduits discharge downstream of the embankment at a location
	where access for observation is possible by maintenance personnel.
	_ Adequate erosion protection is recommended along the contact point between the face of the
	embankment and the abutments, where runoff concentrates.
	Evaluate whether a gutter surface other than sod is necessary (riprap is generally
	preferred over a paved concrete gutter).
	_ Pond drain: Except for flat areas of the coastal plain, each ED pond designed to have a
	permanent pool should have a drain pipe that can completely or partially drain the permanent
	pool.
	In cases where a low level drain is not feasible (such as in an excavated pond), a pump
	wet well should be provided to accommodate a temporary pump intake when needed to
	drain the pond.
	The drain pipe should have an up-turned elbow or protected intake within the pond, to
	prevent sediment deposition, and a pipe diameter capable of draining the pond within
	24 hours.
	The pond drain must be equipped with an adjustable valve located within the riser,
	where it will not be normally inundated and can be operated in a safe manner.
	_ Trees, shrubs or any other woody plants should not be planted or allowed on the embankment
	or adjacent areas extending at least 25 feet beyond the embankment toe and abutment
	contacts.
	_ Safety features:
	The principal spillway opening must be designed and constructed to prevent access by
	small children.
	An emergency spillway and associated freeboard must be provided in accordance with
	Stormwater Design Specification No. 15 and applicable local or state dam safety
	requirements.
	Manage the contours of the basin to eliminate drop-offs or other safety hazards.
	_ Indicate the top of embankment elevations: constructed height and settled height (allowing for
	10% settlement).
	_ Show the existing ground and proposed improvements profile along the center line of the
	embankment.
	_ Show the existing ground and proposed improvements profile along the center line of the
	principal spillway
	Provide a typical grading section through the pond, including typical side slopes with the aquatic
	bench, shoreline protection, etc.
	Show the dimensions of zones for any zoned embankment.
	_
3. Se	epage Control
	All utility conduits (except the principal spillway) should be installed away from the embankment.
	When utility conduits through the embankment cannot be avoided, they should meet the
	requirements for spillways:
	Watertight joints
	No gravel bedding
	Restrained to prevent joint separation due to settlement

_ The contact point between the embankment soil, the foundation material, and the conduit is the
most likely location for piping to occur, due to the discontinuity in materials and the difficulty in
compacting the soil around the pipe.
_ The phreatic line (4:1 slope measured from the principal spillway design high water elevation
through the embankment) is the upper limit of the saturation zone
At a minimum, this should be the 10-year design storm water surface elevation.
If the phreatic line intersects the downstream slope of the embankment, a qualified soil
scientist should be consulted to decide if additional controls, such as an internal drain,
are needed.
Seepage control should be included in the design if the following conditions exist:
Pervious layers in the foundation are not intercepted by the cutoff.
Possible seepage from the abutments may create a wet embankment.
The phreatic line intersects the downstream slope.
Special conditions exist that require drainage to ensure a stable embankment.
Seepage may be controlled by:
Foundation, abutment or embankment drains.
A downstream drainage blanket.
A downstream toe drain (often desirable for homogeneous embankments).
A combination of these measures.
Seepage along pipe conduits that extend through an embankment should be controlled by use
of the following to prevent piping failures along conduit surfaces:
Anti-seep collar (provide detail).
The Bureau of Reclamation, the U.S. Army Corps of Engineers, and the USDA
no longer recommend the use of anti-seep collars, in deference to graded filters
or filter diaphragms and drainage blankets (more complex to design, but less
complicated and more cost-effective to construct and allow for easier placement
of fill material).
Size, based on the length of pipe in the saturation zone (aim is a minimum 15%
increase in seepage length).
Spacing and location of collars on the barrel:
Maximum collar spacing is 14 times the minimum projection above the
pipe.
Minimum collar spacing is 5 times the minimum projection above the
pipe.
Collar dimensions should extend a minimum of 2 feet in all directions
around the pipe.
Anti-seep collars should be placed within the saturation zone. Where the
spacing limit will not allow this, then at least one collar must be in the saturation
zone.
All anti-seep collars and their connections to the conduit should be completely
water-tight and made of material compatible with the conduit. NOTE: Dimple
bands are <i>not</i> considered water-tight.
Metals must be shielded from dissimilar materials with rubber or plastic
insulation at least 24 mils thick.
Anti-seep collars should be placed a minimum of 2 feet from pipe joints unless
flanged joints are used.
Collar size should be calculated using the procedure specified in Chapter 13 of
the Virginia Stormwater Management Handbook (2011).
The embankment filter and drainage diaphragm should be designed by a professional
geotechnical engineer.
These devices channel seepage flow through a filter of fine graded material,
such as sand, which traps any embankment material being transported.
The flow is then conveyed out of the embankment through a perforated toe
drain or other acceptable technique.
The critical design element: the filter material grain size distribution is based on
the grain size distribution of the embankment fill and foundation material.
and gram size and and are an area of the a

		The diaphragm should consist of sand, meeting fine concrete aggregate requirements (at least 15% passing the No. 40 sieve, but no more than 10% passing the No. 100 sieve). The diaphragm should be a minimum of 3 feet thick and should extend vertically upward and horizontally at least 3 times the pipe diameter and vertically downward at least 24 inches beneath the barrel invert, or to rock, whichever is encountered first. The diaphragm should be placed immediately downstream of the cutoff trench, approximately parallel to the centerline of the dam. The diaphragm should be discharged at the downstream toe of the embankment. The opening sizes for slotted and perforated pipes in drains must be designed using the filter criteria. A second filter layer may be required around the drain pipe in order to alleviate the need for many very small openings. Fabric should <i>not</i> be used around the perforated pipe as it may clog, rendering the perforations impenetrable to water.
4.	Fou	ndation and Cut Off Trench or Key Trench
		Label all materials
		The presence of rock in the embankment foundation area requires specific design and construction recommendations (provided by the geotechnical engineering analysis) to ensure a
		proper bond between the foundation and the embankment.
		Generally, no blasting should be permitted within 100 feet of the foundation and abutment area.
		If blasting is necessary, it should be carried out under controlled conditions to reduce
		adverse effects on the rock foundation (e.g., over-blasting, opening fractures, etc.), especially critical in karst topography.
		Show the cut-off trench bottom width (4 foot minimum or as specified in the geotechnical report).
		Show the cut-off trench depth (4 foot minimum or as specified in the geotechnical report) Show the cut-off trench side slopes labeled (no steeper than 1H:1V).
5.	R/114	ti Stage Riser and Barrel System
J.	wui	Principal spillways should be sized according to calculation procedures in Chapter 13 of the
		Virginia Stormwater Management Handbook (2011).
		The principal spillway should be located within the embankment and accessible from dry land to
		ensure easy access for maintenance. Access to the riser should be provided by lockable manhole covers and manhole steps
		within easy reach of valves and other controls.
		Provide a schedule of materials and clearly label them in drawings.
		Drop inlet spillways (riser and barrel system) should be designed as follows: Full flow is established in the outlet conduit and riser at the lowest hydraulic head over
		the riser crest that is feasible. Indicate the crest elevation of riser structure.
		The facility must operate without excessive surging, noise, vibration, or vortex
		action at any stage.
		Therefore, the riser must have a larger cross-sectional area than the outlet conduit.
		Headwall or conduit spillways consist of a pipe extending through an embankment with a
		headwall at the upstream end. The headwall is typically oversized to provide an adequate
		surface against which to compact the embankment fill.
		Weir spillways should be designed as follows: When used as the principal spillway, it should be armored with concrete or other non-
		erosive material.
		At the spillway, armoring should extend from the upstream face of the embankment to a
		point downstream of the spillway toe.
		All principal spillways should be constructed of non-erosive material with an anticipated life expectancy similar to that of the stormwater management facility.

 Pre-cast riser structures may not be substituted if the plans call for a cast-in-place structure
unless approved by the design engineer and the plan approving authority. Sections of pre-cast structures must be anchored together to meet stability and flotation
requirements. A separate principal spillway and emergency spillway is generally recommended, unless:
Topography/abutments too steep.
Existing or proposed development conditions impose constraints.Other factors (e.g., a road embankment is used as the dam, the basin is excavated
etc.)
In such instances, a combined principal/emergency spillway that passes both low flows and extreme flows may be considered for use, in the form of a drop inlet spillway, a headwall/conduit spillway, or some other design that achieves equivalent results.
It is very important to protect such combined spillways from clogging.
Conduits/structures through embankments: Limit the number of conduits that penetrate through the embankment.
Indicate the barrel diameter, inverts, and slope (%).
Show the inverts and dimensions of controlled release orifices/weirs
Show the structure dimensions
Show the extended detention orifice protection
NOTE: A cause of embankment failure is the separation of pipe joints due to differentia
settlement and pipe deflection. All connections to pipes must be completely water-tight. The drain pipe (or barrel) connection to the riser should be welded all around when both are metal.
A rubber or neoprene gasket should be used when joining pipe sections.
The end of each pipe should be re-rolled by enough corrugations to fit the band
width.
Helically corrugated pipe should have either continuous welded seams or lock
seams with internal caulking or a neoprene bead. The following connection types are acceptable:
For pipes less than 24 inches in diameter:
Flanges with gaskets on both ends of the pipe
A 12-inch wide standard lap type band with a 12-inch wide by 1/2-inch thick closed cell circular neoprene gasket.
A 12-inch wide hugger type band with O-ring gaskets having a minimum diameter of 3/8 inch greater than the corrugation
depth. For pipes ∃ 24 inches in diameter:
Por pipes \(\) 24 inches in diameter. A 24-inch long annular corrugated band using rods and lugs.
A 24-inch wide by 3/8 inch thick closed cell circular neoprene gasket.
Corrugated metal pipe (CMP) must meet or exceed the minimum required design thickness.
Steel pipe and its appurtenances should be galvanized and fully bituminous
coated and should conform to the requirements of AASHTO Specification M 190 Type A with water-tight coupling bands.
Any bituminous coating damaged or otherwise removed should be replaced with cold-applied bituminous coating compound.
Steel pipes with polymeric coatings should have a minimum coating thickness of 0.01 inches (10 mils) on both sides of the pipe.
Coated corrugated steel pipe should meet the requirements of AASHTO M-245 and M-246; the following coatings or an approved equivalent may be used: Nexon, Plasti-Cote, Blac-Clad, and Beth-Cu Loy.

Aluminum coated steel pipe and its appurtenances should conform to the requirements of AASHTO Specification M-274 with water-tight coupling band or flanges.
Any aluminum coating damaged or otherwise removed should be
replaced with cold-applied bituminous coating compound. Aluminum pipe and its appurtenances should conform to the requirements of AASHTO Specification M-196 or M-211 with water-tight coupling bands of
flanges.
Aluminum surfaces that are to be in contact with concrete should be painted with one coat of zinc chromate primer, and hot-dipped galvanized bolts may be used for connections.
The pH of the surrounding soils should be between 4 and 9.
The contractor and project inspector should verify the metal thickness
corrugation size, proper connecting bands, and gasket type. Maximum allowable deflection of CMP conduits is 5% of the pipe diameter.
Water-tight joints are necessary to prevent infiltration of embankment soils into the conduit.
All joints must be constructed as specified by the pipe manufacturer.
Field joints (the ends of the pipes are cut off in the field) should <i>not</i> be accepted.
With larger pipe sizes, it may be difficult to get water-tight joints, even
the deflection is within design parameters.
In such cases, the designer may choose to specify a heavier gage pipe Bands:
All connectors must be composed of the same material as the pipe.
Metals must be shielded from dissimilar materials with rubber or plasti insulation at least 24 mils thick.
6-inch hugger bands and "dimple bands" should not be accepted for CMP conduits.
For pipes ≤ 24 inches in diameter, use 12-inch wide bands with 12-incl O-ring or flat neoprene gaskets.
For larger pipes, use 24-inch wide bands with 24-inch wide flat gasket and four "rod and lug" type connectors.
Flanged pipe with gaskets may also be used.
All pipe gaskets should be properly lubricated with the material provide
by the manufacturer, and tensioned, to prevent deterioration of the gasket material.
Flat gaskets must be factory welded or solvent-glued into a
circular ring, with no overlaps or gaps The pipe should be firmly and uniformly bedded throughout its length:
Where rock or soft, spongy or other unstable soil is encountered,
should be removed and replaced with suitable soil that is subsequently
compacted to provide adequate structural support.
Under no conditions should gravel bedding be placed under a condu
through the embankment. Installation of a concrete pipe cradle will help to reduce the risk of piping unde
the barrel and the subsequent failure of the embankment, resulting from
differential settlement.
The concrete cradle may not be necessary along the entire length of the conduit to prevent piping, but it is recommended since grave bedding under an embankment conduit is <i>never</i> appropriate unless it is designed as a filter or drainage diaphragm

If the external load (e.g., from the height of the embankment,
anticipated construction traffic, the weight of compaction equipment,
etc.) on the barrel is enough to warrant provision for its maximum
supporting strength, then a concrete cradle should be installed along
the conduit's entire length.
 Reinforced concrete pipe should have bell and singular spigot joints with rubber gaskets
and should equal or exceed ASTM Designation C-361.
Bell and spigot pipe should be placed with the bell end upstream.
Joints should be made consistent with manufacturer recommendations.
After the joints are sealed for the entire run of pipe, the bedding should be
placed so that all spaces under the pipe are filled.
All reinforced concrete pipe conduits should be laid in a concrete
bedding for their entire length.
This bedding should consist of high slump concrete placed under the
pipe and up the sides of the pipe at least 25% of its outside diameter,
and preferably to the spring line, with a minimum thickness of 3 inches,
or otherwise as shown on the drawings.
Care should be taken to prevent any deviation from the original line and grade
of the pipe.
 Polyvinyl Chloride (PVC) pipe should be PVC-1120 or PVC-1220 conforming to ASTM
D-1785 or ASTM D-2241.
Joints and connections to anti-seep collars should be completely water-tight.
The pipe should be firmly and uniformly bedded throughout its length.
Where rock or soft, spongy or other unstable soil is encountered, it
should be removed and replaced with suitable soil that is subsequently
compacted to provide adequate structural support.
 All conduits penetrating dam embankments should be designed using the following
criteria:
Conduits and structures penetrating an embankment should have a smooth
surface without protrusions or indentations that will hinder compaction of
embankment materials.
All conduits should be circular in cross-section except cast-in-place reinforced
concrete box culverts. This is also true where multiple conduits are employed.
Conduits should be designed to withstand the external loading from the
proposed embankment without yielding, buckling or cracking, all of which will
result in joint separation.
Conduit strength should not be less than the values shown in the design
specifications for corrugated steel, aluminum, and PVC pipes, and the
applicable ASTM standards for other materials.
The designer or contractor should obtain a manufacturer's certification
that the pipe meets plan requirements for design load, pipe thickness,
joint design, etc.
Inlet and outlet flared-end sections should be made from materials that are
compatible with the pipe.
All pipe joints should be made water-tight by using flanges with gaskets,
coupling bands with gaskets, bell and spigot ends with gaskets, or by welding.
Where multiple conduits are employed, sufficient space should be provided
between the conduits and installed anti-seep collars to allow for backfill material
to be placed between the conduits with earth-moving equipment and easy
access by hand-operated compaction equipment.
The distance between conduits should be ∃ 1/2 of the pipe diameter,
but not less than 2 feet.
 Cathodic protection should be provided for coated welded steel and galvanized
 corrugated metal pipe when soil and resistivity studies indicate the need for a protective
coating against acidic soils.

Outlet protection must be used for the downstream toe of a spillway structure to help dissipate
the high-energy flow through the spillway and to prevent excessive erosion in the receiving channel.
The type of outlet protection depends on the flow velocities associated with the spillway.
Riprap is the preferred form of outlet protection, designed according to Chapter 13 of
the Virginia Stormwater Management Handbook (2011) and the Virginia Erosion and
Sediment Control Handbook (1992). Gabion baskets are also an acceptable outlet
protection material.
The bottom of the riprap apron should be constructed at 0% slope along its
length.
The end of the apron should match the grade and alignment of the receiving channel.
If the receiving channel is well-defined, the riprap should be placed on the
channel bottom and side slopes (no steeper than 2H:1V) for the entire length,
as required in the design criteria in Chapter 13 of the <i>Virginia Stormwater</i>
Management Handbook (2011) and the Virginia Erosion and Sediment Control
Handbook (1992).
Riprap placement should not alter the channel's geometry.
Excavation of the channel bed and banks may be required to construct the full
thickness of the apron. If the barrel discharges into the receiving channel at an angle, the opposite
bank must be protected up the the 10-year storm elevation. In no instance
should the total length of outlet protection be shortened.
If a permit requires that no work may be performed in the stream or channel,
then the outlet structure must be moved back to allow for adequate protection.
The horizontal alignment of the apron should have no bends within the design
length.
Additional riprap should be placed if a significant change in grade occurs at the downstream end of the outfall apron.
Filter fabric should be placed between the riprap and the underlying soil to
prevent soil movement into and through the riprap.
All control structures should have a trash rack or debris control device, designed as follows:
All trash rack and debris control components should be made of stainless steel or
galvanized metal meeting VDOT specifications.
Trash racks attached to a concrete spillway structure should be secured with stainless steel anchor bolts.
Openings for trash racks should be no larger than 1/2 of the minimum conduit
dimension and, to discourage child access, bar spacing should be no greater than 1 foot
apart. The clear distance between the bars on large storm discharge openings generally
should be no less than 6 inches.
Flat grates for trash racks are <i>not</i> acceptable.
Inlet structures that have flow over the top should have a non-clogging trash rack (e.g.,
a hood-type inlet that allows passage of water from underneath the trash rack into the riser, or a vertical or sloped grate).
The designer should verify that the surface area of the vertical perimeter of a raised
grate equals the area of the horizontal top opening, to allow adequate flow passage
should the top horizontal surface become clogged.
Metal trash racks and monitoring hardware should be constructed of galvanized or
stainless steel.
Methods to prevent clogging of extended detention orifices in dry extended detention
basins should be carefully designed, since these orifices are usually very small and
located at the invert or bottom of the basin. All drop inlet spillways designed for pressure flow should have adequate anti-vortex devices (not
required if weir control is maintained in the riser through all flow stages, including the maximum
design storm or safety storm):
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The device may be a baffle or plate installed on top of the riser, or a headwall set on
one side of the riser. The design of a principal spillway riser structure should include a <i>flotation</i> or <i>buoyancy</i> calculation (see Chapter 13 of the <i>Virginia Stormwater Management Handbook, 2011</i>).
The downward force of the riser and footing (to which the riser must be firmly attached) is the <i>structure weight</i> , which must be 1.25 times greater than the buoyant force acting
on the riser. Stormwater management facilities having permanent impoundments may be designed so that
the permanent pool can be drained to simplify maintenance and sediment removal. The draining mechanism will usually consist of a valve or gate attached to the spillway structure and an inlet pipe projecting into the reservoir area, with a trash rack or debris
control device. The typical configuration of a drainpipe will place the valve inside the riser structure with
the pipe extending out to the pool area. This configuration results in the drainpipe being pressurized by the hydraulic
head associated with the permanent pool. Pressurized pipes should have mechanical joints in order to avoid possible
leaks and seepage resulting from the innate pressure. In all cases, valves should be secured to prevent unauthorized draining of the
facility. Basin drains should be designed with sufficient capacity to pass the 1-year frequency design storm with limited ponding in the reservoir area, so that
sediment removal and other maintenance functions are not hampered. An uncontrolled or rapid drawdown of a stormwater basin could cause a slide in
the saturated upstream slope of the dam embankment or shoreline area. Therefore, the design of the basin drain system should include specific
operating instructions for the owner. Generally, the drawdown rate should not exceed 6 inches per day. For embankment or shoreline slopes of clay or silt, the drawdown rate
may be as low as 1 inch per week to ensure slope stability.
gency Spillway
Vegetated emergency spillways must be built in existing, undisturbed earth/rock or "cut" in the abutments at one or both ends of an earthen embankment or ovr a topographic saddle anywhere on the periphery of the basin. They should <i>never</i> be located on any portion of the
embankment fill material. Excavated emergency spillways consist of three elements:
 An inlet channel, through which <i>subcritical</i> flow enters the spillway.
The inlet channel should have a straight alignment and grade.
The cross-sectional area of flow in the inlet channel should be large in comparison to the flow area at the control section.
Where the depth of the channel changes to provide for the increased flow area,
the bottom width should be altered gradually to avoid abrupt changes in the
shape of the sloping channel banks.
A level section, which controls the depth of flow.
The maximum design water surface elevation (normally for the 100-year storm) through the emergency spillway should be at least 1 foot lower than the settled top of the embankment and should be confined by undisturbed earth or rock.
The bottom width of the spillway should not exceed 35 times the design depth of flow, to avoid damage by meandering flow and accumulated debris.
Whenever the required bottom width is likely to be excessive, consideration should be given to incorporation of a spillway at each end of the dam.
The two spillways do not need to be of equal width if their total capacity meets design requirements.

	An exit channel, through which either <i>critical</i> or <i>supercritical</i> flow discharges from the
	spillway The alignment of the exit channel must be straight to a point far enough below
	the embankment to ensure that any flow escaping the exit channel cannot
	damage the embankment.
	The exit channel should have the same cross-section as the control section.
	The slope of the exit channel must be:
	Adequate to discharge the peak flow within the channel.
	No greater than that which will produce maximum permissible velocities
	for the soil type or the planned grass cover.
	The slope range of the exit channel is selected to ensure <i>supercritical</i> flow in the channel.
	The control section is the point on the spillway where the flow passes through <i>critical</i>
	depth, usually installed close to the intersection of the earthen embankment and the
	emergency spillway centerlines. The type of soil and vegetative cover used in the emergency spillway can be used to establish
	the spillway design dimensions and geometry.
	Vegetation provides a degree of retardance to the flow through the spillway, depending
	mostly on the height and density of the vegetative cover chosen.
	_ Hydraulic design for emergency spillways must be done in accordance with criteria provided in
	Appendix C: Vegetated Emergency Spillways of the Introduction to the New Virginia Stormwater
	Design Specifications (as posted on the Virginia Stormwater BMP Clearinghouse web site at
	http://www.vwrrc.vt.edu/swc/NonProprietaryBMPs.html) and in Chapter 13 of the Virginia
	Stormwater Management Handbook (2011). Spillway side slopes should be no steeper than 3H:1V unless the spillway is excavated into rock.
	Show the existing ground and proposed improvements along the center line of the emergency
	spillway
C. La	ndscape Plan
	The landscaping plan must indicate the methods to be used to establish and maintain vegetative
	cover in the ED Pond and its buffer area, including the following:
	Consider including design elements that promote diverse wildlife and waterfowl use within the ED pond and buffer.
	Show the delineation of pondscaping zones within both the pond and buffer.
	Provide a planting schedule and specifications (transport / storage / installation / maintenance)
	Ensure that plant selection is appropriate for the site's vegetation climatic zone (4-8 in
	Virginia), emphasizing native species if feasible.
	Identify the sources of native plant material.
	Avoid species that require full shade, or are prone to wind damage.
	The planting plan should allow the pond to mature into a native forest in the right places,
	but yet keep mowable turf along the embankment and all access areas.
	A wooded wetland approach may be a good option for many ED ponds. Specify the sequence for preparing the wetland bed, if one is included with the ED pond
	(including soil amendments, if needed).
	Woody vegetation may not be allowed to grow within 15 feet of the toe of the
	embankment nor within 25 feet from the principal spillway structure.
	A vegetated buffer should be provided that extends at least 25 feet outward from the
	77 vegetated burier should be provided that extends at least 20 feet outward from the
	maximum water surface elevation of the ED pond.
	maximum water surface elevation of the ED pond. Existing trees within the buffer area should be preserved during construction.
	maximum water surface elevation of the ED pond. Existing trees within the buffer area should be preserved during construction. Permanent structures (e.g., buildings) should <i>not</i> be constructed within the buffer area.
	maximum water surface elevation of the ED pond. Existing trees within the buffer area should be preserved during construction. Permanent structures (e.g., buildings) should <i>not</i> be constructed within the buffer area. Due to soil compaction, planting holes should be 3 times deeper and wider than the
	maximum water surface elevation of the ED pond. Existing trees within the buffer area should be preserved during construction. Permanent structures (e.g., buildings) should <i>not</i> be constructed within the buffer area. Due to soil compaction, planting holes should be 3 times deeper and wider than the diameter of the root ball for ball-and-burlap stock, and 5 times deeper and wider for
	maximum water surface elevation of the ED pond. Existing trees within the buffer area should be preserved during construction. Permanent structures (e.g., buildings) should <i>not</i> be constructed within the buffer area. Due to soil compaction, planting holes should be 3 times deeper and wider than the diameter of the root ball for ball-and-burlap stock, and 5 times deeper and wider for container-grown stock.
	maximum water surface elevation of the ED pond. Existing trees within the buffer area should be preserved during construction. Permanent structures (e.g., buildings) should <i>not</i> be constructed within the buffer area. Due to soil compaction, planting holes should be 3 times deeper and wider than the diameter of the root ball for ball-and-burlap stock, and 5 times deeper and wider for

	Er	sure that topsoil / planting soil is included in final grading plan.
D.	Ide	uction Notes eally, planned ED pond areas should be constructed after the contributing drainage area is
	CO	mpletely stabilized.
	(pi gr	O pond areas <i>may</i> be used during construction as sites for temporary sediment traps or basins roperly sized for E&S control purposes), provided the construction plans include notes and aphical details specifying the facility will be de-watered, dredged and re-graded to design mensions after the original site construction is complete.
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	_	 Installation of the permanent riser should be initiated during the construction phase Design elevations should be set with final cleanout of the sediment basin and conversion to the post-construction ED pond in mind.
		The bottom elevation of the permanent ED pond should be lower than the bottom elevation of the temporary sediment basin.
		Appropriate procedures should be implemented to prevent discharge of turbid waters when the basin is being converted into a ED pond.
		some cases, it will be necessary to divert flow while the ED pond is being constructed, so that sediment flows into the pond area until installation and stabilization are complete.
	_	Flow diversions may be required to meet additional requirements of and obtain permits from state and federal regulatory agencies.
	Co	onstruction sequence:
		Construction inspections should occur before, during and after installation to ensure the
		stormwater wetland is constructed according to specifications.
		Use detailed inspection checklists that require sign-offs by qualified individuals
		at critical states of construction, to ensure the contractor's interpretation of the plan is consistent with the designer's intent.
		The following are critical inspection points:
		During initial site preparation and installation of E&S Controls.
		Excavation and grading (e.g., interim and final elevations).
		Installation of the embankment, the riser/primary spillway, and the outlet structure.
		Pondscaping installation and final stabilization.
		Check the proposed site for existing utilities prior to any excavation.
		Assemble the construction materials on-site, making sure they meet design specifications, and prepare any staging areas.
		Clear, grub and strip the areas designated for borrow sites, embankment construction, and structural work to the desired subgrade, removing all trees, vegetation, roots and
		other objectional material. All cleared and grubbed material should be disposed of outside and below the
		limits of the embankment and reservoir.
		When specified, a sufficient quantity of topsoil should be stockpiled in a suitable
		location for use on the embankment and other designated areas. Install applicable temporary E&S control measures prior to construction.
		Excavate the core trench for the embankment and install the spillway (outlet) pipe,
		including the downstream rip-rap apron (energy dissipation) protection
		The cutoff trench should be excavated into impervious material along or parallel
		to the centerline of the embankment.
		Trench side slopes should be laid back in steps at a 1H:1V slope or flatter.
		(from page 6; conflicts with 2:1 specified on page 10, Earthen Embankment Spec?).
		Backfill should be compacted with construction equipment, rollers, or hand
		tampers to assure maximum density and minimum permeability.
		Install the riser pipe or overflow structure, ensuring the top invert of the overflow weir is
		constructed level and at the proper design elevation.
		Construct the embankment and any internal berms in 8- to 12-inch lifts, compacted with appropriate equipment.

The	s on which fill is to be placed should be scarified before its placement. most permeable borrow material should be placed in the downstreamons of the embankment.		
İnstal	I the principal spillway or overflow weir concurrently with fill placement and		
mate	xcavated into the embankment. A vertical trench through the embankment rial (in order to place the spillway pipe) should not be allowed under any		
circumstances.			
	Ensure that the top invert of the principal spillway or any overflow weir is constructed level and at the proper design elevation (at least 1 foot		
	below the crest of the emergency spillway). Flashboard risers are strongly recommended for use in constructed wetlands.		
Filter	and Drainage Layers:		
	In order to achieve maximum density of clean sands, filter layers should be flooded with clean water and vibrated just after the water drops		
	below the sand surface. The filter material should be placed in lifts of no more than 12 inches in		
	thickness.		
	_ Up to 4 feet of embankment material may be laced over a filter material		
	layer before excavating back down to expose the previous layer. After removing any unsuitable materials, the trench may be filled with		
	additional 12-inch lifts of filter material, flooded, and vibrated as described above, until the top of adjacent fill is reached.		
	The contractor should ensure that a qualified professional inspect filter		
	and drainage diaphragms, ensuring that backfill material meets		
	specifications for quality, lift thickness, placement, moisture content,		
	and dry unit weight.		
Fill material should be taken from an approved, designated borrow			
stockpile.			
	Fill material should be free of roots, stumps, wood, rubbish, stones		
	greater than 6 inches in diameter, and frozen or other objectionable		
	materials.		
	_ Fill material for the center of the embankment and the cutoff trench		
	should conform to Unified Soil Classification GC, SC, or CL.		
	Fill material that is beside pipes or structures should be of the same type and quality as specified for the adjoining fill material.		
	The fill material should be placed in horizontal lifts not to		
	exceed 4 inches in thickness and compacted by hand tampers or other manually directed compaction equipment.		
	The material should completely fill all spaces under and beside		
	the pipe.		
	During backfilling, equipment should not be driven closer the 4		
	feet horizontally to any part of a structure.		
	Equipment should NEVER be driven over any part of a		
	structure or pipe, unless compacted fill has been placed to a		
	depth specified by the structural live load capacity of the		
	structure or pipe, that adequately distributes the load.		
	_ Consideration may be given to the use of other materials in the		
	embankment based on the recommendation of a geotechnical engineer		
	supervising the design and construction.		
	_ The surface layer of compacted fill should be scarified prior to		
	placement of at least 6 inches of topsoil, which must be properly		
Eill ∽	stabilized.		
	aterial should be compacted with appropriate compaction equipment. _ The number of necessary passes by the compaction equipment over		
	the fill material may vary with soil conditions.		

Fill material should contain sufficient moisture so that the degree of compaction will be obtained with the equipment used. The minimum required density is 95% of maximum dry density.	d. ·		
moisture content within \pm 2% of the optimum, unless of	-		
specified by the engineer. Each layer of fill should be compacted as necessary to obtain density.	minimum		
Compaction tests should be performed regularly throughout the emb construction.	oankment		
Typically, one test per 5,000 sq. ft. on each layer of fill or as did the geotechnical engineer.	rected by		
Use either a Standard Proctor Test (ASTM D698) or a Modifier Test (ASTM D1557 – usually more appropriate for earthen dam	ns).		
A new Proctor test is required if the material changes f previously tested.	from that		
The engineer should certify, at the time of construction, that	t each fil		
layer meets the minimum density A geotechnical or construction inspector should be on site during emb	nankment		
construction to do the following:	Jankinent		
Test fill compaction			
Observe foundation preparation.			
Observe pipe installation.			
Observe riser construction Observe filter installation, etc.			
Construct the emergency spillway in cut or structurally stabilized soils.			
Excavate/grade until the appropriate elevations and desired contours are achieved fo			
the bottom and side slopes of the pond.			
Install outlet pipes, including the downstream rip-rap apron (energy dissipation protection.			
			Stabilize exposed soils with temporary seed mixtures appropriate for the pond buffer. A areas above the normal pool elevation should be temporarily stabilized by hydroseedin or seeding over straw.
Plant the pond buffer area and implement any remaining permanent sta	abilization		
If the ED pond has a permanent pool, the contractor should measure the			
constructed pond depth at three locations within the permanent pool (fore-to-pond, and at the riser), and these depths should be marked and geo-reference as-built drawing. This will facilitate long-term maintenance.			
Implement any remaining permanent stabilization measures.			
Conduct a final inspection, log the GPS coordinates for each facility and submit entry into the local BMP maintenance tracking database.	t them for		
E. Maintenance Items (can include BMP Operation & Maintenance Inspection Checklis Chapter 9, Appendix 9-C of this Handbook)	sts from		
Provide a Maintenance Agreement, indicating the person or organization respon	nsible for		
maintenance, authorizing access for inspections and maintenance, and including a maintenance			
inspection checklist.			
Include a Maintenance Narrative which describes the long-term mai requirements of the facility and all components, including installation/mainte safety signage; removal and disposal of trash, debris and sediment accumulat	enance of		
mowing. Record a deed restriction, drainage easement, and/or other enforceable mechanism, CDS coordinates of the area to ensure the ED pend is not converted to other uses.	including		
Provide sufficient facility access from the public ROW or roadway to both the ED pond	d and any		
GPS coordinates of the area, to ensure the ED pond is not converted to other uses.			

IV.	COMMENTS		
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		Rv.	Date:

8-A.17.0. REFERENCES

Center for Watershed protection (CWP). July, 2008b. *Post-Construction Guidance Manual: Tool 6 – Plan Review, BMP Construction, and Maintenance Checklists.* Ellicott City, MD.

City of Gresham, Oregon. 2003. Inspection Checklist for Infiltration Systems. Gresham, OR.

City of Gresham, Oregon. 2003. Inspection Checklist for Ponds. Gresham, OR.

Interlocking Concrete Pavement Institute. 2008. *PICP Permeable Design Pro Software*. Herndon, VA. www.icpi.org.

Minnesota Pollution Control Agency. September, 2006. *Minnesota Stormwater Manual, Ver. 1.1, Appendix D: Operations and Maintenance Checklists.* St. Paul, MN.

Virginia Department of Conservation and Recreation (DCR). 1999. *Virginia Stormwater Management Handbook*. Richmond, VA.

Virginia Department of Environmental Quality (DEQ). 2013. Virginia Stormwater Management Handbook. Richmond, VA.

Virginia Department of Environmental Quality (DEQ). 2013. Various stormwater management BMP specifications. *Virginia Stormwater BMP Clearinghouse* web site: http://www.vwrrc.vt.edu/swc/. Richmond, VA.